

# NASA Contractor Report 159180

## OPTIMIZED AERODYNAMIC DESIGN PROCESS FOR SUBSONIC TRANSPORT WING FITTED WITH WINGLETS

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DESIGN PROCESS FOR SUBSONIC TRANSPORT WING  
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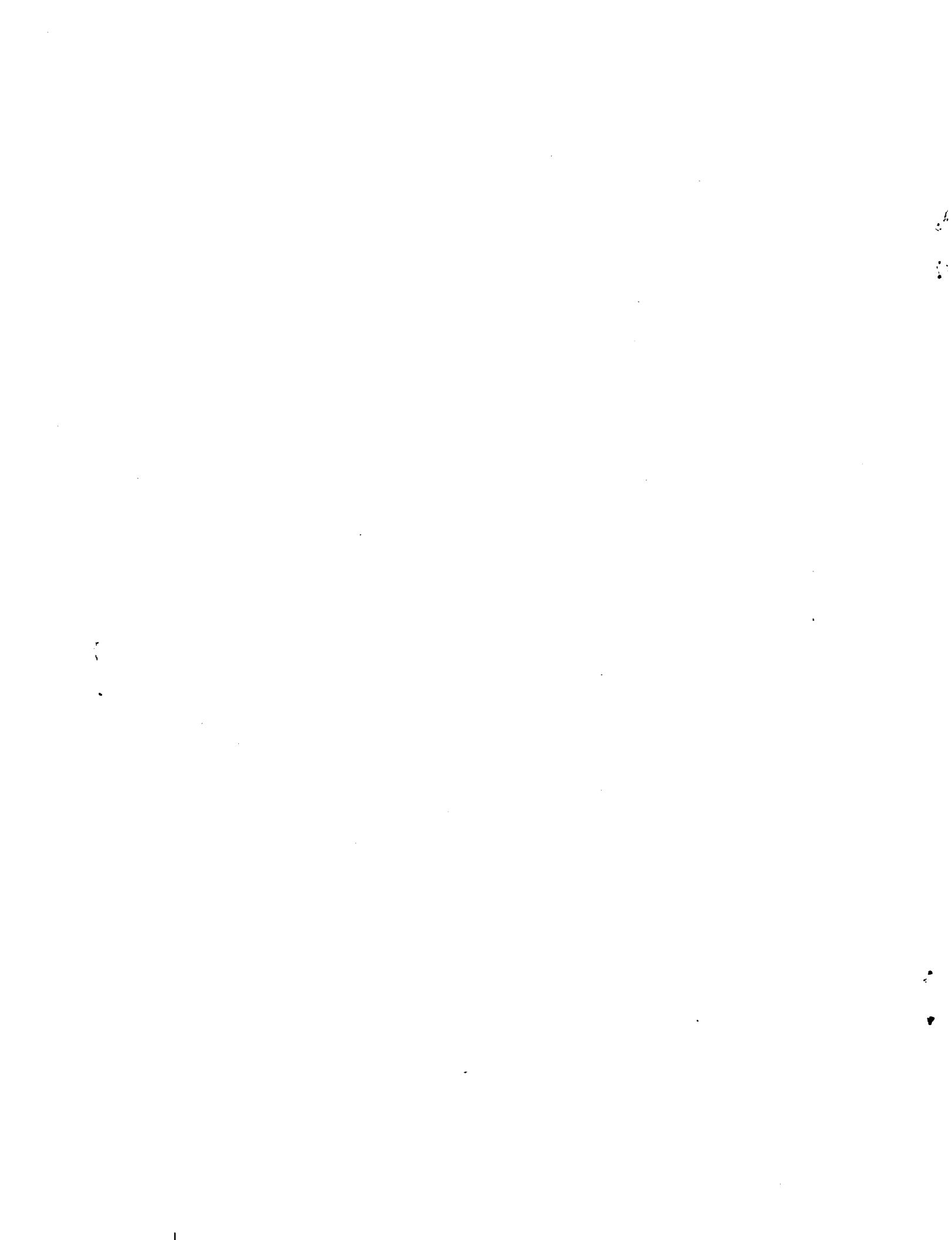
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## SUMMARY

The aerodynamic design of a wind-tunnel model of a wing representative of that of a subsonic jet transport aircraft, fitted with winglets, has been performed using two recently developed optimal wing-design computer programs. Both potential flow codes use a vortex lattice representation of the near-field of the aerodynamic surfaces for determination of the required mean camber surfaces for minimum induced drag, and both codes use far-field induced drag minimization procedures to obtain the required spanloads. One code uses a discrete vortex wake model for this far-field drag computation, while the second uses a 2-D advanced panel wake model. Wing camber shapes for the two codes are very similar, but the resulting winglet camber shapes differ widely. Design techniques and considerations for these two wind-tunnel models are detailed herein, including a description of the necessary modifications of the design geometry to format it for use by a numerically controlled (NC) machine for the actual model construction.

## INTRODUCTION

The current emphasis on improving the fuel efficiency at cruise of existing transport aircraft, and designing future generations of aircraft with even further increases in fuel efficiency, has resulted in the consideration of several new, novel aircraft configurations. Examples are the so-called box plane studied in references 1 and 2, the joined wing concept of reference 3, and winglets as discussed in reference 4. Further model studies of improved transport performance may be found in references 5-7. These concepts generally use nonplanar lifting surfaces to reduce the induced drag.

Recently a vortex lattice wing-design computer program has been developed, described in reference 8, which computes for subcritical flow, using thin wing potential flow theory, the wing camber surfaces for one or two interacting planforms for minimum induced drag. The user specifies the configuration geometry in planview, dihedral angles, the reference wing area and span, the subsonic design Mach number and design lift coefficient. The desired

chordwise loading function must also be specified on each planform. The camber shape is computed directly which will achieve the desired lift, have zero pitching moment (for two planforms) and will have minimum induced drag. This program may be used as a preliminary design tool for constructing wind-tunnel models to investigate the above-mentioned new aircraft configurations, so long as the design is subcritical. Further, for configurations which are subcritical, this program is relatively inexpensive to run compared to more sophisticated transonic codes which use iterative techniques to achieve optimal solutions.

However, there is concern that the vortex lattice theory could lead to errors in design shape in the vicinity of a change in wing dihedral angle (refs. 9 and 10). This has lead to the development of an advanced panel far-field wake model (ref. 11) where the wing wakes are broken into flat panels, and where the wake vortex strength is assumed to vary linearly on each wake panel. This theory has been shown to be more accurate than a discrete vortex wake model (ref. 11). This wake model has been extended to obtain the bound circulation and spanload distributions for minimum induced drag for use in the vortex lattice wing-design code of reference 8. Extensions of this theory, as well as sample results from the modified design code, have been given in reference 12. Design results to date (refs. 12 and 13) have shown that the original code (ref. 8) and the modified code (ref. 12) give identical results except where there is a change in wing dihedral.

In an attempt to determine the capabilities of both of these subcritical design codes, two wind-tunnel models are currently being designed for a single transport type wing fitted with winglets. The design point is  $M = 0.8$ ,  $C_L = 0.5$ , and it is expected that there will be only a very limited region of slightly supercritical flow. The wing planform for both models is the same as that used in one of the sample results given in reference 8. The winglet planforms for both models are identical; this planform has been chosen using the recommendations of reference 4. The two computer programs give essentially identical camber shapes on the wing, but yield widely different shapes on the winglet. Hence, a single wing model is to be built, using the results of the modified code, while both winglet models are to be constructed and tested for comparison. This report details the considerations used to design these two models. In particular, the data required for using a numerically controlled machine to cut the model surfaces is discussed.

## SYMBOLS

A	wing aspect ratio, defined as $b^2/S$
a	chordwise pressure loading parameter
b	wing span, cm (in.), equal to 71.491 cm (28.146 in.)
c	local chord, m (ft)
$\bar{c}$	mean chord, m (ft), equal to 0.2136 m (0.7008 ft)
$C_p$	pressure coefficient
$\Delta C_p$	pressure difference coefficient
$c_t$	wing tip chord, cm (in.), equal to 8.113 cm (3.194 in.)
$C_B$	wing root bending moment coefficient
$C_D$	induced drag coefficient
$C_L$	lift coefficient
$C_m$	pitching moment coefficient about origin of body axis coordinate system shown in figure 1
M	Mach number
q	dynamic pressure, Pa ( $1b/ft^2$ )
S	projected wing area, $m^2$ ( $ft^2$ ), equal to 0.30595 $m^2$ (3.293 $ft^2$ )
t	local semithickness, cm (in.)
X	streamwise body axis coordinate, cm (in.)
x	streamwise coordinate measured from local wing leading edge, cm (in.)
Y	spanwise coordinate, cm (in.)
Z	vertical coordinate, cm (in.)
z	coordinate normal to local wing chordplane, cm (in.)
$\alpha$	angle of attack, radians (degrees)
$\epsilon$	nondimensional chordwise coordinate
$\eta$	nondimensional spanwise coordinate
$\phi$	dihedral angle, radians (degrees)

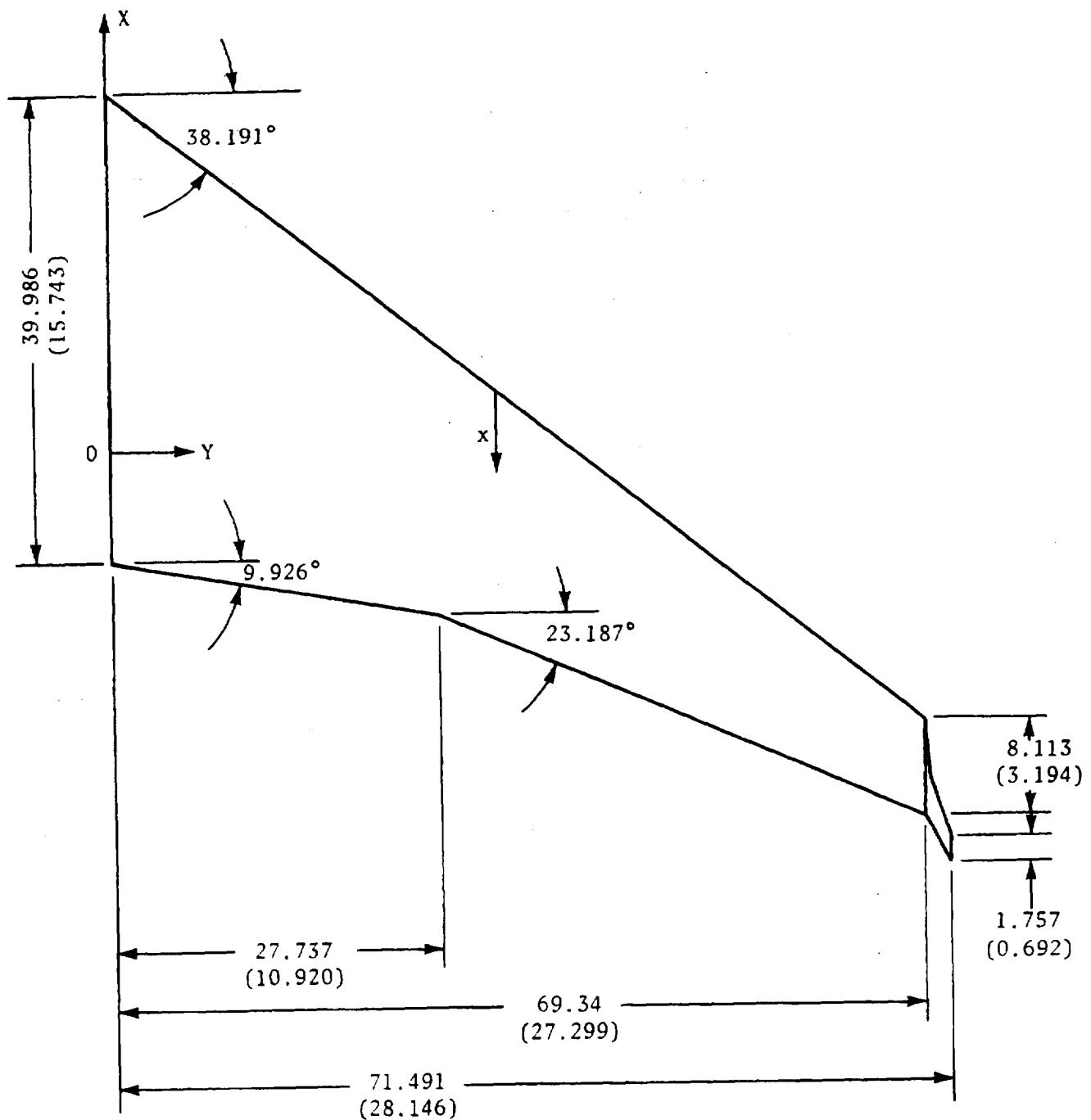


Figure 1. Planview of wing-winglet model. Dimensions are given in cm (in.); wing has  $6^\circ$  dihedral and winglet has  $77.5^\circ$  dihedral.

## MODEL WING-WINGLET DESCRIPTION

The current wind-tunnel wing-winglet models have been designed for use on an existing fuselage model, which has been used in a series of tests of previous wing-winglet models (ref. 5) and high-aspect ratio wing tests (ref. 7). The wing planform (fig. 1) was the same as that used in the single planform example of reference 8; however, the winglet plan view (fig. 2) has been altered to conform to recommended winglet-design criteria given in reference 4. The wing has been scaled so its projected span equals the span of the configurations tested in reference 5, using the same fuselage model. This wing planform is representative of current subsonic jet transport wings. Model wing projected area was  $0.30595 \text{ m}^2$  ( $3.293 \text{ ft}^2$ ), and mean chord equaled  $0.2136 \text{ m}$  ( $0.7008 \text{ ft}$ ). The design point chosen was a Mach number of 0.8 and a lift coefficient of 0.5. These were chosen as being representative of current jet transports. Also it was felt desirable to attempt a model design at the highest values of Mach number and lift coefficient which seemed advisable. It is likely that for the model size chosen ( $b = 1.430 \text{ m}$ ), the maximum Mach number achievable in the NASA-Langley  $7 \times 10$  foot high-speed tunnel where the model is to be tested will be no greater than  $M = 0.8$  (ref. 14). This design point was chosen such that once the wing thickness distribution was superimposed on the designed camber shape, the flow over the wing and winglet would be everywhere subcritical. Wing and winglet leading edge sweeps were 38.19 and 35.28 degrees, respectively. The wing had a trailing edge break at 0.388 times the total configuration projected semispan and a constant 6 degrees of dihedral. The winglet length was 0.143 times the projected span of the wing alone. The winglet trailing edge was straight, with a leading edge break at 0.25 times the winglet height. The lower 25 percent of the winglet was swept 61.6 degrees. The upper 75 percent of the winglet had a leading edge sweep of 35.28 degrees which, when projected down to the wing tip, intersected the tip at 0.65 times the wing tip chord. The winglet dihedral was 77.5 degrees (see fig. 2). These values, as well as the eight percent maximum thickness type NACA 64A008 thickness distribution (ref. 15), all followed the recommendations of reference 4. A design using a constant chordwise

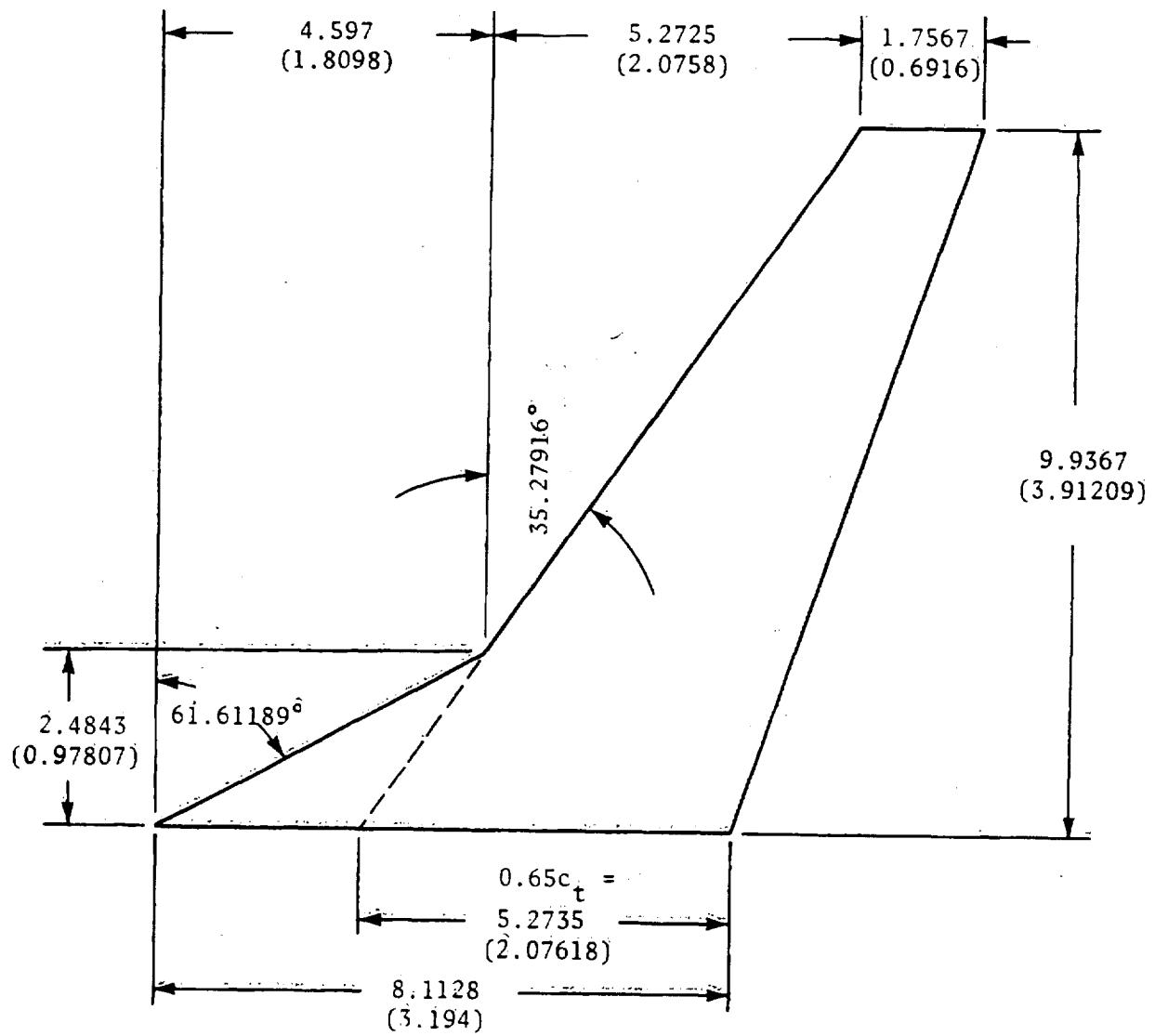


Figure 2. Winglet plan view. Dimensions are given in cm (in.).

loading function ( $a = 1.0$ ) like that used in reference 8 has been chosen.

#### CAMBER SURFACE DESIGN

Once the model planform, scale, and design point had been chosen, the two inviscid design codes of references 8 and 12 were used to obtain the camber shapes predicted by each which would lead to minimum induced drag. In both codes, a vortex lattice near-field representation of 18 chordwise vortices by 21 spanwise was chosen. This was close to the maximum number of near-field singularities allowable in either code. The design camber shape was insensitive to these values over the limited range of  $18 \times 21$  to  $16 \times 25$ . The adopted lattice layout led to three camber lines on the winglet: one below the leading edge break and two above the break. The original design code was modified to use 96 discrete vortex unknowns, rather than the usual 100, in the Trefftz plane to determine the optimum span load. This was done to duplicate as nearly as possible the true wake shape for the wing-winglet model, given the restriction of equally spaced wake vortices (ref. 8). The modified code (ref. 12) used 50 wake panels having a cosine spacing. Thirty-five panels were used on the wing and 15 on the winglet. It is believed that the calculations for the modified code were more accurate, based upon results shown in references 11 and 12. The computed induced drag for the original code was 0.009034, while for the modified code using the advanced panel wake model  $C_D = 0.008141$ . This is inconsistent with results of reference 11, where the discrete vortex model was seen to underpredict the induced drag, but is believed to be due to inaccuracies in the discrete vortex wake shape. Further study as to the reason for these  $C_D$  values is required.

The necessary input data cards for both computer programs, as well as the resultant outputs are shown in Appendix A. The different optimum spanloads from these two programs are plotted in figure 3. They differ most significantly on the winglet and near the wing tip. Examples of the computed optimum camber shapes are shown in figure 4. Again, the differences in the two methods are confined to the region near the winglet on the wing and on the winglet itself. Similar results have been

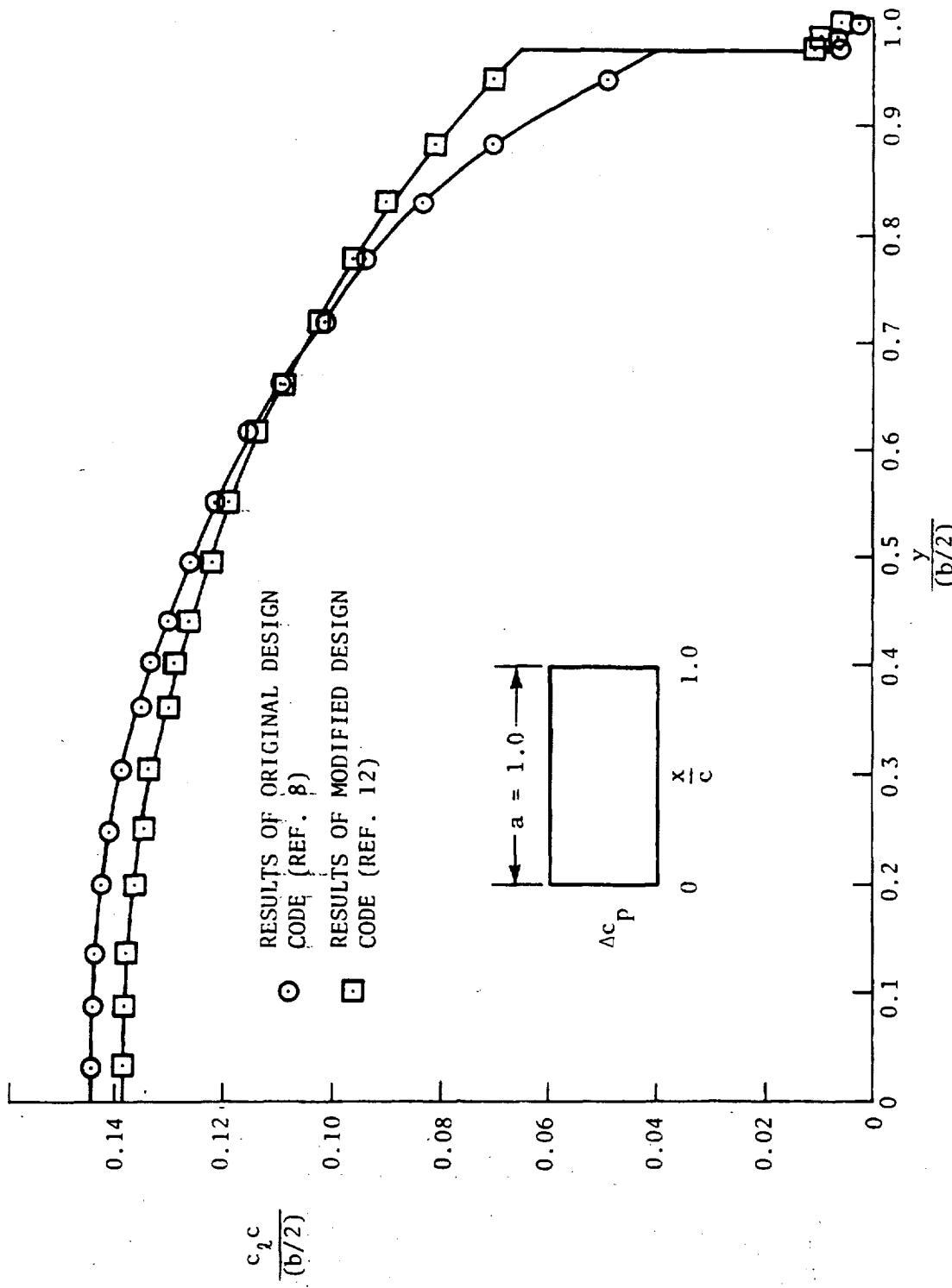


Figure 3. Spanload distribution for wing-winglet model designed for minimum induced drag  
at  $M = 0.8$ ,  $C_L = 0.5$ ,  $a = 1.0$ .

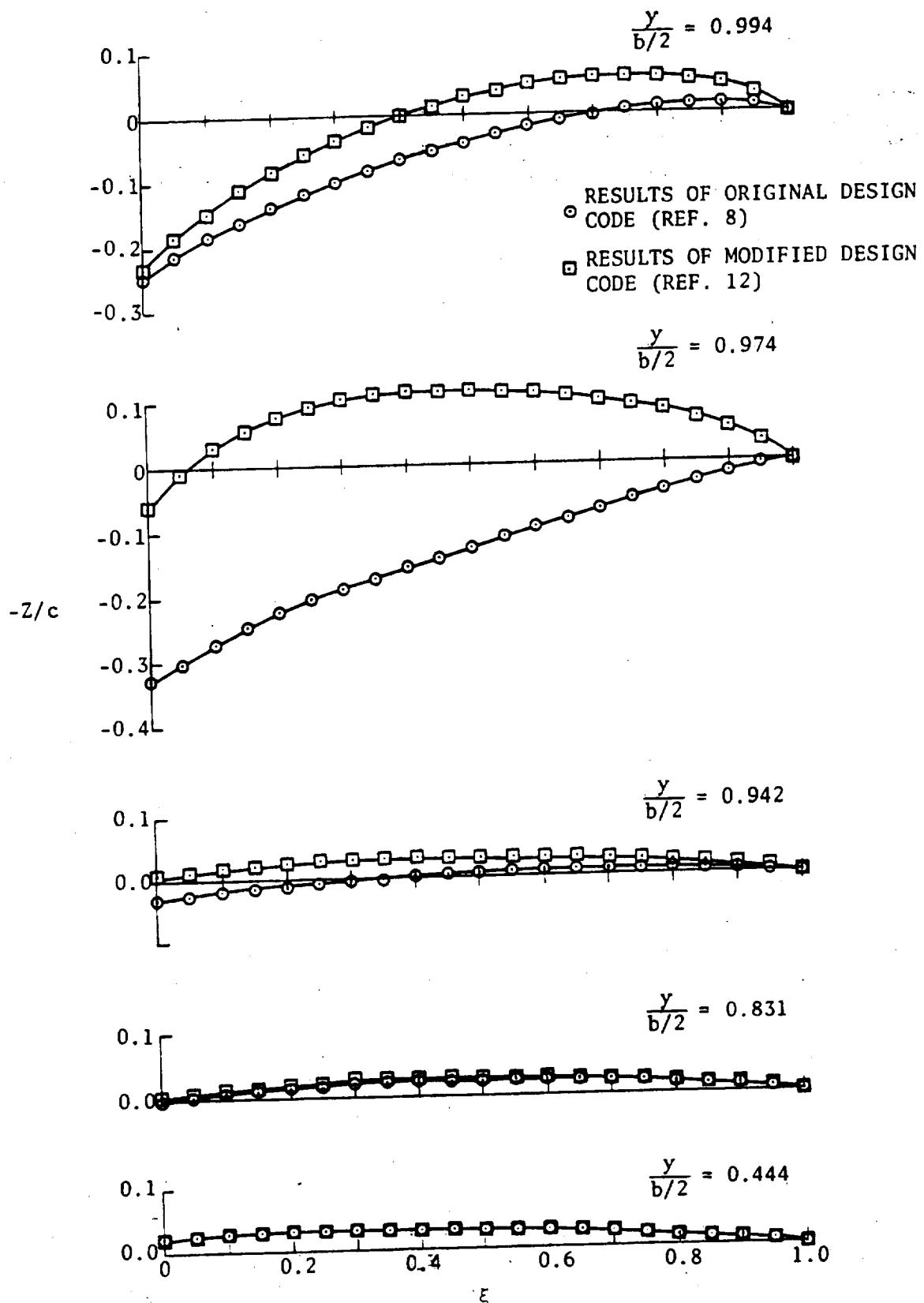


Figure 4. Camber shapes for wing-winglet model designed for minimum induced drag at  $M = 0.8$ ,  $C_L = 0.5$ ,  $a = 1.0$ .

presented previously in reference 12 for a similar wing-winglet configuration, having a different winglet planform.

Once these design results had been obtained, and the NACA 64A008 thickness distribution chosen, the three-dimensional potential flow code of reference 16 was utilized to check for any locally supercritical regions on the designed wing-winglet. All of the design camber surface  $Z/c$  values were rescaled by multiplying by the cosine of the local dihedral to obtain local airfoil cambers perpendicular to the plane of the wing or winglet. Also, the local  $n$  values had to be recomputed in terms of the fractional wing-winglet peripheral length. These input data were in a simplified namelist format developed under contract for NASA/Langley Research Center (LaRC) by the Computer Sciences Corporation. The resultant panel geometry for the modified code design is shown in figure 5, and sample chordwise pressure plots are shown in figure 6. There was a region of nearly constant  $\Delta C_p$ , over about the middle 70 percent of the local chord, with the pressure difference falling to zero at the trailing edge, and with a slight rise at the leading edge. The minimum pressure coefficient computed on the configuration designed using the original code (ref. 8) was -0.5675, while the minimum found on the shape computed using the modified code (ref. 12) was -0.7461. These values occurred near the winglet root. The value of  $C_p$  for sonic conditions at  $M = 0.8$  is -0.6910, so it is felt that there will not be any regions of supercritical flow on the model designed using the original code (ref. 8). The modified code model will have a small region of slightly supercritical flow near the root of the winglet. It is also noted that the chosen design point,  $C_L = 0.5$  and  $M = 0.8$ , is as high as possible without appreciably violating the assumption of subcritical flow.

This summarizes the aerodynamic considerations undertaken for the design of the current models. The more complete design process, such as described in reference 17, was not undertaken, largely because these models must be tested to discover how useful the computer codes of references 8 and 12 are as design tools. The wing-winglet configuration chosen should provide a good test, while at the same time yielding information about which version of the design code is preferable. More sophisticated analysis programs modeling the flow over complete aircraft configurations,

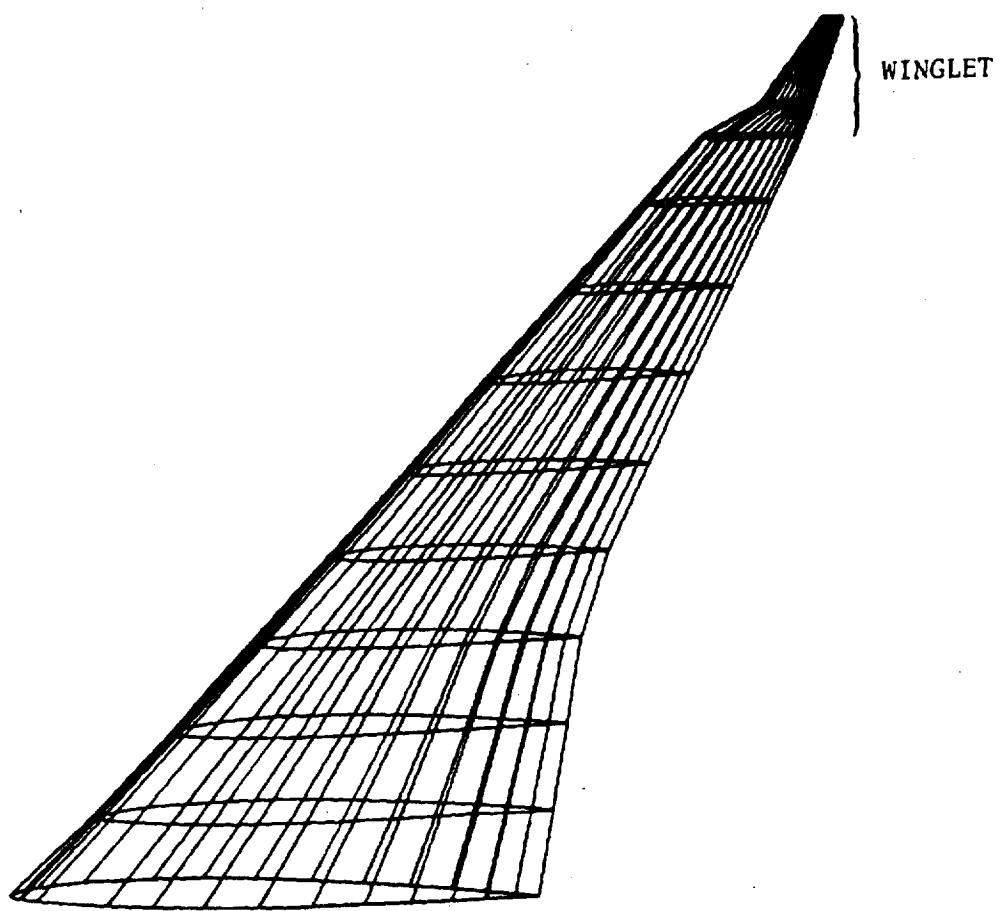


Figure 5. Perspective view of wing-winglet panel geometry for code of reference 16; design results of reference 12.

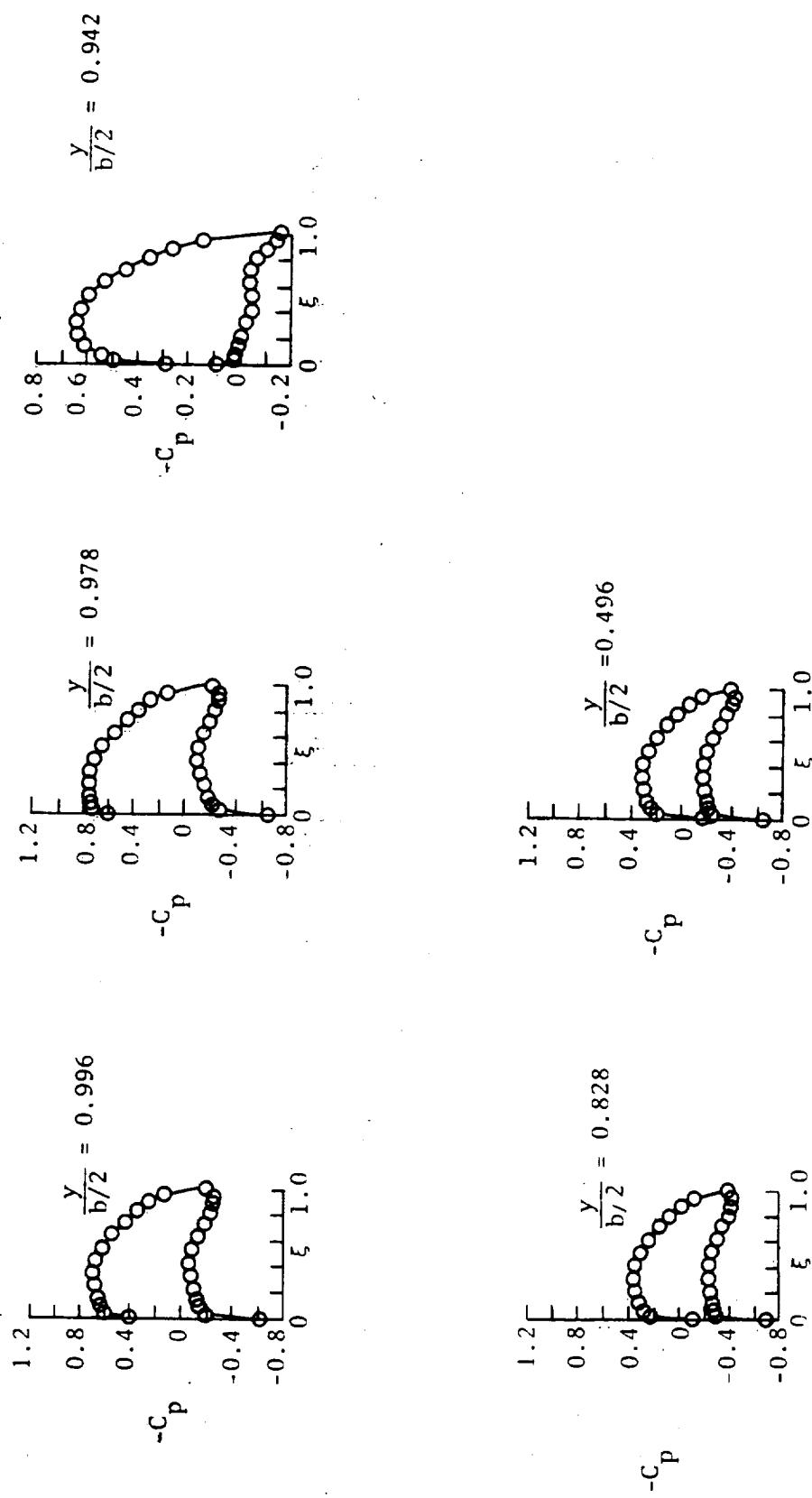


Figure 6. Hess code chordwise pressure coefficient distributions for wing-winglet designed by method of reference 12.

including the effects of bodies, thickness, shocks, and even viscous effects, as described in references 18 and 19 would be expected to yield more accurate performance predictions. The recent aerodynamic optimization programs of references 20 and 21 should allow determination of optimum configurations including the above nonideal effects.

#### DESIGN DETAILS

Several other basic model design specifications and criteria have been developed relating to the construction of the model itself. Since the wing cambers from both codes differed only in the region immediately adjacent to the wing-winglet junction, it was decided to build only one wing model, using the camber values from the modified design code (ref 12). The wing and winglet models will be cut using numerically controlled machining from steel, since the test dynamic pressures will be in the vicinity of  $q = 34,100 \text{ Pa}$  ( $720 \text{ lb/ft}^2$ ) at the design point (ref. 14). The wing and all winglet models will be cut separately so all surface coordinates will be measured perpendicular to the plane of the wing or the winglets. Four separate pairs of winglets will be constructed. These winglets will bolt to the model wing tip. Two pairs of winglets will be machined having the camber shape computed using the original design code (ref. 8). One of these winglet pairs will have static pressure ports at the 12.5 and 42.5 percent peripheral distance stations. Upper surface pressures will be sensed on one winglet; lower surface pressure taps will be placed at the same x/c values on the other winglet. The pressure tubing will join to larger tubing in the wing itself in a cutout cavity in the wing near the wing-winglet junction. The second winglet pair will have no pressure instrumentation, but will be fitted with full span 0.2 c trailing edge flaps which bolt to the winglet. The flat deflection angles will be  $0^\circ$ ,  $\pm 2^\circ$ ,  $\pm 4^\circ$ . The remaining two pairs of winglet models will be constructed having the camber shape of the modified design code (ref. 12); one pair will be fitted with pressure taps, while the second pair will be fitted with flaps, as described above. The wing model will have two chordwise rows of static pressure taps, at the 31 and 74 percent peripheral distance locations. All pressure tubing will be carried inside the fuselage to three scannivalves. The region of the junction between wing and winglets

will be formed by handwork using templates. The wing root region will be beveled to allow it to bolt to the fuselage strongback. Also, if feasible, the wing root region will be gaged to allow measurement of the wing root bending moment.

#### NUMERICALLY CONTROLLED MACHINE INPUT

Finally, a description is now given of the steps necessary to prepare an input deck to prepare a tape for use on the numerically controlled machine (type TX-23). A small computer program was written to rescale the camber shapes to be perpendicular to the local  $\phi$ , by multiplying by  $\cos \phi$ . Then the t/c values were added to get upper and lower surface values, which were then multiplied by the local chord value in inches. This yielded a set of upper and lower surface coordinates, in inches, measured perpendicular to the wing or winglet planes. Next, these coordinates were extrapolated linearly to obtain coordinates at the wing root and tip, the location of the trailing edge break on the wing, the winglet root and tip, and the location of the leading edge break on the winglet. These values were then punched on cards in a 7F10.6 format. The airfoil shapes were also plotted using LaRC subroutine INFOPLT. The program listing and output are shown in Appendix B, along with the final decks to cut the wing and the winglet. Both decks shown were for the modified design code results (ref. 12). Also included are the N/C machine input deck preparation instructions. Examples of the wing and winglet airfoil sections are shown in figure 7.

The NASA/LaRC model shop personnel can supply sample data checks which aid in building an input deck for numerically controlled machining of a general wing. Categories I and II (see TX-23 Input, Appendix B) must be largely defined by the engineer, while items III, IV, and V are fairly standard and any needed changes in these cards can be made by the personnel in the model shop. Item II contains the bulk of the geometrical information, beginning with (X, Y) pairs, in inches, for the leading edge and trailing edge [Item (3), Link (1)]. These are followed by the Y values, in inches, at which the airfoil upper and lower surface coordinates are specified [Item (5), Link (1)]. The Items (8) and (9), Link (1), contain the percent chord locations, followed by the corresponding upper surface coordinates, in

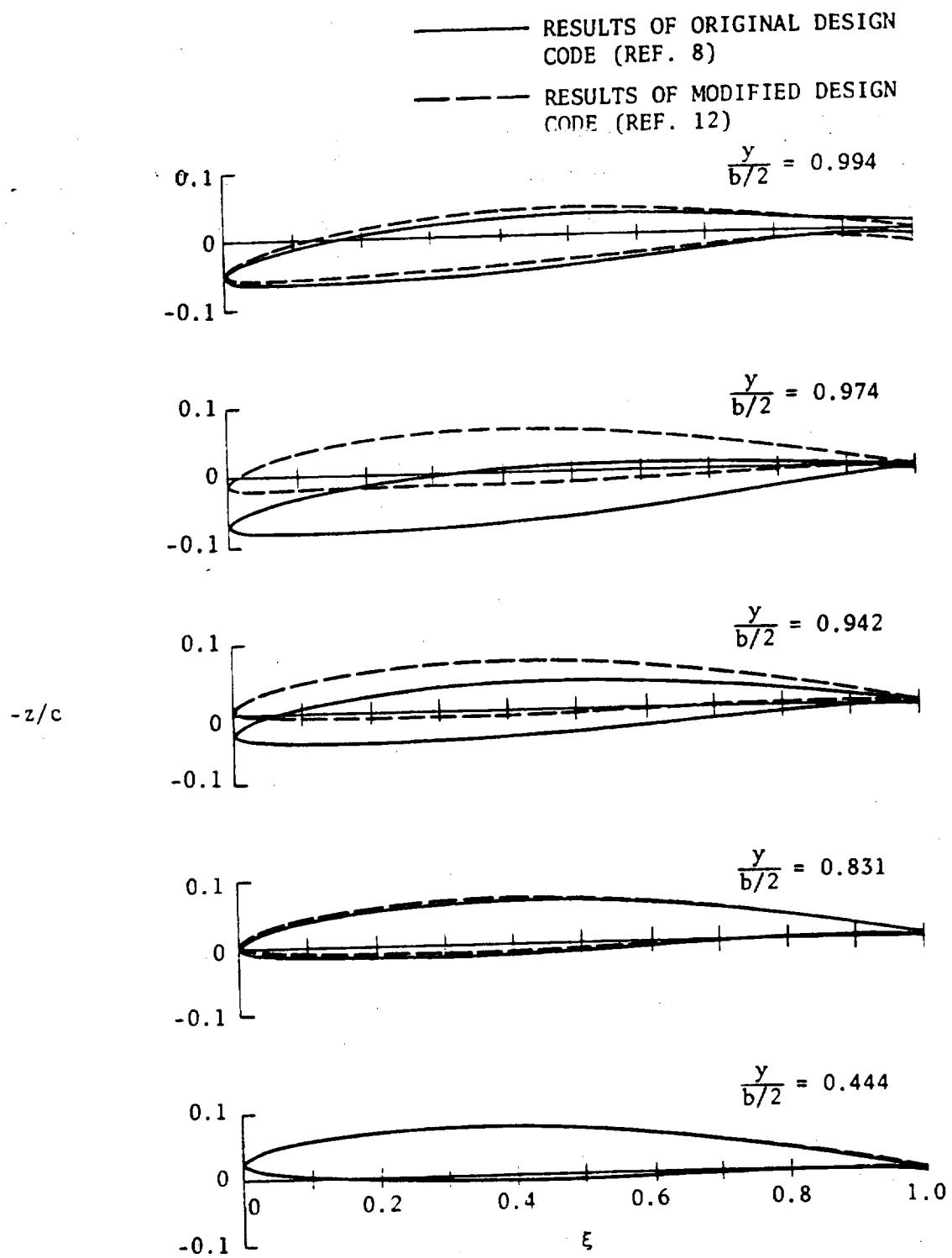


Figure 7. Comparison of wing-winglet model airfoil sections.

inches, and lower surface coordinates, in inches, at each airfoil station. A maximum of 21 airfoils may be specified, as has been done for the current wing model (Appendix B). A maximum of 30 coordinate triples may be specified for each airfoil. Straight line curve fitting in the spanwise direction and cubic curve fitting chordwise was used for the current models.

The detailed design work is currently being implemented under contract by LTV, and the final design will be constructed in-house by the model shop at NASA/LaRC.

#### CONCLUSIONS

The design process for construction of a wind-tunnel model of a subsonic transport wing fitted with winglets has been described. The camber shapes of the winglet models have been computed using two potential-flow wing-design programs. The two codes give quite different results on these winglets. As a result, these wind-tunnel models are to be used to determine which program gives a design shape with better performance. Also, the wind-tunnel test will provide information as to the utility of these potential flow programs in the design process. Also documented were the data preparation procedures necessary to obtain an input deck for numerically controlled machining of the models.

**APPENDIX A**

**INPUT DATA AND OUTPUT FOR WING-WINGLET  
DESIGN USING CODES OF REFERENCES 8  
AND 12**

SI 3049 1400250  
ATLANTIC 4000 25

	1.	26.9696	2353.6293
4.	0.	0.	0.
36.5332	-0.	6.	0.
-23.7143	-69.34	77.5	1.
-26.2111	-59.2777	77.5	1.
-23.5237	-71.4997	6.	1.
-35.3462	-71.4907	77.5	1.
-32.7053	-69.9777	77.5	1.
-31.3274	-69.34	6.	1.
-14.0667	-27.736	6.	1.
-8.1529	-0.	0.	1.
100.	10.	20.	0.8 0.5
1.0			
2.0			
3.	35.		
25.	16.		

ORIGINAL  
OF POOR PAGE  
QUALITY

GEOOMETRY DATA

REFERENCE PLANFORM HAS 8 CURVES

ROOT CHORD HEIGHT = 0.00000

VARIABLE SWEEP PIVOT POSITION

X(S) = 0.00000

BREAK POINTS FOR THE REFERENCE PLANFORM

POINT	X REF	Y REF	SWEEP ANGLE	DIHEDRAL ANGLE	MOVE CODE
1	30.83320	0.00000	30.19097	6.00000	1
2	-23.71430	-69.34000	83.32828	77.50000	1
3	-23.31110	-69.67770	72.99002	77.50000	1
4	-23.59370	-71.43070	90.00000	0.00000	1
5	-35.34020	-71.43670	53.52736	77.50000	1
6	-32.70530	-69.67770	58.52190	77.50000	1
7	-31.92710	-69.34000	23.18709	6.00000	1
8	-14.0670	-27.73600	9.92625	6.00000	1
9	-9.15290	0.00000			

CONFIGURATION NO. 100.

CURVE 1 IS SWEEPED 36.19097 DEGREES ON PLANFORM 1

BREAK POINTS FOR THIS CONFIGURATION

POINT	X	Y	Z	SWEET ANGLE	DIHEDRAL ANGLE	MOVE CODE
1	36.82320	0.00000	0.00000	36.19097	6.00000	1
2	-23.71420	-62.34000	-7.28793	83.32828	77.50000	1
3	-24.31140	-63.87770	-9.71334	72.99002	77.50000	1
4	-22.56370	-71.45970	-16.88911	90.00000	0.00000	1
5	-35.32050	-71.43070	-16.62911	58.52736	77.50000	1
5	-22.70530	-63.67770	-9.71334	58.52190	77.50000	1
7	-31.42270	-49.34600	-7.28793	23.18709	6.00000	1
8	-14.000670	-27.73600	-2.31517	9.92625	6.00000	1
9	-5.15290	0.00000	0.00000			
			-71.495402			

378 HORSESHOE VORTICES USED ON THE LEFT HALF OF THE CONFIGURATION

PLANFORM TOTAL SPANWISE

1 278 21

18. HORSESHOE VORTICES IN EACH CHORDWISE ROW

X SHIFT OF ORIGIN = 0.0000 UNITS

MINIMUM FIELD LENGTH = 63300

ORIGINAL PAGE IS  
OF POOR QUALITY

	X	Y	Z	S	C/4 SWEEP ANGLE	DIHEDRAL ANGLE	GAMMA/U AT CLOES= .5000
	374	3C/4					
-32.29592	-32.27729	-71.05557	-15.04485	1.99147	72.87795	77.50000	.04911
-32.34567	-32.41404	-71.05767	-15.04485	1.99147	72.41497	77.50000	.04911
-32.49241	-32.52079	-71.05957	-15.04485	1.99147	71.92712	77.50000	.04911
-32.61416	-32.63753	-71.06157	-15.04485	1.99147	71.41240	77.50000	.04911
-32.75591	-32.62423	-71.06357	-15.04485	1.99147	70.56651	77.50000	.04911
-32.16262	-32.56102	-71.06557	-15.04485	1.99147	70.29240	77.50000	.04911
-32.02946	-32.66777	-71.06757	-15.04485	1.99147	69.53400	77.50000	.04911
-32.16614	-32.23452	-71.06957	-15.04485	1.99147	69.03746	77.50000	.04911
-32.36292	-32.37126	-71.07157	-15.04485	1.99147	68.35044	77.50000	.04911
-32.62554	-32.56501	-71.07357	-15.04485	1.99147	67.61925	77.50000	.04911
-32.57638	-32.64476	-71.07557	-15.04485	1.99147	66.92975	77.50000	.04911
-32.71313	-32.76150	-71.07757	-15.04485	1.99147	66.00730	77.50000	.04911
-32.64937	-32.91425	-71.07957	-15.04485	1.99147	65.11671	77.50000	.04911
-32.99662	-34.05492	-71.08157	-15.04485	1.99147	64.16215	77.50000	.04911
-32.42337	-32.16174	-71.08357	-15.04485	1.99147	63.13705	77.50000	.04911
-32.76011	-32.32449	-71.08557	-15.04485	1.99147	62.03406	77.50000	.04911
-32.36706	-32.46523	-71.08757	-15.04485	1.99147	60.94483	77.50000	.04911
-32.12591	-32.66165	-71.08957	-15.04485	1.99147	59.36000	77.50000	.04911
-32.52564	-32.74594	-71.09157	-15.04485	1.99147	58.87795	77.50000	.04911
-29.37692	-29.56154	-70.25317	-11.40696	1.73475	72.41497	77.50000	.04911
-32.91636	-32.21567	-70.25517	-11.40696	1.73475	71.73475	77.50000	.04911
-32.22556	-30.32594	-70.25717	-11.40696	1.73475	71.40695	77.50000	.04911
-32.42499	-30.52602	-70.26017	-11.40696	1.73475	70.86564	77.50000	.04911
-32.64160	-30.74561	-70.26317	-11.40696	1.73475	70.29340	77.50000	.04911
-32.05101	-30.95652	-70.26617	-11.40696	1.73475	69.68400	77.50000	.04911
-32.59102	-32.16602	-70.26917	-11.40696	1.73475	69.03746	77.50000	.04911
-32.27192	-32.57462	-70.27317	-11.40696	1.73475	71.41240	77.50000	.04911
-32.44195	-32.78607	-70.27517	-11.40696	1.73475	63.35044	77.50000	.04911
-32.59167	-32.76457	-70.27817	-11.40696	1.73475	67.51925	77.50000	.04911
-32.60198	-32.60569	-70.28117	-11.40696	1.73475	65.83975	77.50000	.04911
-32.11103	-32.21410	-70.28417	-11.40696	1.73475	64.03730	77.50000	.04911
-32.22110	-32.42611	-70.28717	-11.40696	1.73475	65.11671	77.50000	.04911
-32.53112	-32.63512	-70.29017	-11.40696	1.73475	64.16215	77.50000	.04911
-32.74612	-32.84614	-70.29317	-11.40696	1.73475	63.13705	77.50000	.04911
-32.55114	-32.05415	-70.29517	-11.40696	1.73475	62.03405	77.50000	.04911
-32.16116	-32.32414	-70.29817	-11.40696	1.73475	60.84483	77.50000	.04911
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-27.44627	-27.46493	-69.61085	-8.50063	1.73475	81.77264	77.50000	.10927
-27.43464	-28.01935	-69.61085	-8.50063	1.73475	81.29591	77.50000	.10927
-24.118405	-28.25776	-69.61085	-8.50063	1.73475	81.76105	77.50000	.10927



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-18.51154	-59.43721	-6.24710	1.99147	35.07116	6.00000
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-21.26504	-59.43721	-6.24710	1.99147	29.36684	6.00000
-21.26507	-59.43721	-6.24710	1.99147	28.49317	6.00000
-21.59270	-59.43721	-6.24710	1.99147	27.60480	6.00000
-21.59272	-59.43721	-6.24710	1.99147	26.70178	6.00000
-22.26457	-59.43721	-6.24710	1.99147	25.78422	6.00000
-22.27174	-59.43721	-6.24710	1.99147	24.85224	6.00000
-22.27175	-59.43721	-6.24710	1.99147	23.90600	6.00000
-23.45027	-59.43721	-6.24710	1.99147	23.01439	6.00000
-24.10416	-59.43721	-6.24710	1.99147	37.29953	6.00000
-24.50111	-59.43721	-6.24710	1.99147	36.57081	6.00000
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-25.15597	-59.43721	-6.24710	1.99147	34.29998	6.00000
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-27.09651	-59.43721	-6.24710	1.99147	31.9942	6.00000
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-14.46311	-14.29547	-5.5.47610	-5.83077	1.99147	29.36684
-15.16582	-15.53317	-5.5.47610	-5.83077	1.99147	28.49317
-15.39592	-16.25998	-5.5.47610	-5.83077	1.99147	27.60480
-16.56253	-16.91458	-5.5.47610	-5.83077	1.99147	26.70178
-17.54683	-17.71329	-5.5.47610	-5.83077	1.99147	25.78422
-18.97161	-18.46946	-5.5.47610	-5.83077	1.99147	24.85224
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-12.41032	-12.71280	-51.51499	-51.51499	1.99147	35.02608
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-13.32214	-13.32392	-51.51499	-51.51499	1.99147	33.51435
-14.72670	-14.3234	-51.51499	-51.51499	1.99147	32.71419
-15.53729	-15.93504	-51.51499	-51.51499	1.99147	31.9942
-16.32722	-16.74661	-51.51499	-51.51499	1.99147	31.06996
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-14.75077	-11.51973	-4.85387	1.99147	21802
-15.81103	-11.46126	-4.75367	1.99147	21802
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-23.26239	-18.75659	-4.75387	1.99147	21802
-24.30279	-19.70973	-4.75387	1.99147	21802
-25.34319	-20.65390	-4.75387	1.99147	21802
-26.38359	-21.60321	-4.75387	1.99147	21802
-27.42399	-21.55656	-4.75387	1.99147	21802
-28.46439	-21.50725	-4.75387	1.99147	21802
-29.50479	-21.45754	-4.75387	1.99147	21802
-30.54519	-21.40783	-4.75387	1.99147	21802
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-32.62599	-21.30841	-4.75387	1.99147	21802
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-43.03000	-20.80932	-4.75387	1.99147	21802
-44.07039	-20.75961	-4.75387	1.99147	21802
-45.11079	-20.70989	-4.75387	1.99147	21802
-46.15119	-20.65018	-4.75387	1.99147	21802
-47.19159	-20.60047	-4.75387	1.99147	21802
-48.23199	-20.54976	-4.75387	1.99147	21802
-49.27239	-20.49005	-4.75387	1.99147	21802
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-51.35319	-20.37063	-4.75387	1.99147	21802
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-54.47439	-20.19150	-4.75387	1.99147	21802
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-72.26159	-19.11672	-4.75387	1.99147	21802
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-90.98879	-18.02994	-4.75387	1.99147	21802
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-4.23372	-6.79427	-35.67053	-3.74912	1.99147	32.51435	6.00000	*24535
-5.35476	-5.91525	-35.67053	-3.74912	1.99147	32.71419	6.00000	*24535
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-13.20164	-13.76213	-35.67053	-3.74912	1.99147	26.70178	6.00000	*24535
-14.32262	-14.66112	-35.67053	-3.74912	1.99147	25.76422	6.00000	*24535
-15.44361	-16.60110	-35.67053	-3.74912	1.99147	24.85224	6.00000	*24535
-16.56459	-17.12464	-35.67053	-3.74912	1.99147	23.90600	6.00000	*24535
5.59149	4.59657	-21.70941	-3.32779	1.99147	38.01439	6.00000	*25231
6.33965	3.75673	-21.70941	-3.32779	1.99147	37.29953	6.00000	*25231
2.18561	2.15759	-21.70941	-3.32779	1.99147	36.57051	6.00000	*25231
1.32197	1.29695	-21.70941	-3.32779	1.99147	35.82803	6.00000	*25231
7.76913	7.1421	-21.70941	-3.32779	1.99147	35.07118	6.00000	*25231
-4.41071	-1.01063	-21.70241	-3.32779	1.99147	34.29998	6.00000	*25231
-1.61055	-2.21046	-21.70541	-3.32779	1.99147	33.51435	6.00000	*25231
-2.31133	-3.41010	-21.70341	-3.32779	1.99147	32.71419	6.00000	*25231
-4.61022	-4.61014	-21.70641	-3.32779	1.99147	31.86942	6.00000	*25231
-5.80065	-5.80065	-21.70341	-3.32779	1.99147	31.06996	6.00000	*25231
-6.40030	-7.00062	-31.70341	-3.32779	1.99147	30.22577	6.00000	*25231
-7.500374	-8.30062	-31.70741	-3.32779	1.99147	29.35684	6.00000	*25231
-8.20059	-9.40060	-31.70941	-3.32779	1.99147	28.49317	6.00000	*25231
-10.40064	-10.60063	-31.70941	-3.32779	1.99147	27.50480	6.00000	*25231
-11.20925	-11.40061	-21.70941	-3.32779	1.99147	26.70178	6.00000	*25231
-12.40060	-13.00061	-31.70941	-3.32779	1.99147	25.78422	6.00000	*25231
-13.60062	-14.20062	-31.70941	-3.32779	1.99147	24.85224	6.00000	*25231
-14.30063	-14.30063	-41.70941	-3.32779	1.99147	23.90600	6.00000	*25231
7.91057	7.25602	-23.73243	-3.01590	1.00192	25.31439	6.00000	*25695
6.55666	5.67661	-23.73243	-3.01630	1.00192	27.29953	6.00000	*25695
2.39736	4.77741	-23.73243	-3.01630	1.00192	36.57051	6.00000	*25695
4.10676	3.50871	-23.73243	-3.01630	1.00192	35.92808	6.00000	*25695
2.37016	2.24961	-23.73243	-3.01630	1.00192	35.07118	6.00000	*25695

1.52005	-0.99050	-2.0.73243	-1.0.01990	1.0.0192	34.29998	6.00000
0.36091	-2.0.73243	-2.0.73243	-2.0.01970	1.0.00192	33.51435	6.00000
-0.39815	-1.0.52770	-2.0.73243	-3.0.01990	1.0.00192	32.71419	6.00000
-1.0.52770	-2.0.73243	-3.0.01990	-3.0.01990	1.0.00192	31.0.00000	6.00000
-2.0.15725	-2.0.73243	-3.0.01990	-3.0.01990	1.0.00192	31.0.00000	6.00000
-3.0.41626	-2.0.73243	-3.0.01990	-3.0.01990	1.0.00192	31.0.00000	6.00000
-4.0.64561	-2.0.73243	-3.0.01990	-3.0.01990	1.0.00192	31.0.00000	6.00000
-5.0.33551	-2.0.73243	-3.0.01990	-3.0.01990	1.0.00192	31.0.00000	6.00000
-6.0.16411	-2.0.73243	-2.0.01960	-2.0.01960	1.0.00192	30.22577	6.00000
-7.0.45456	-2.0.73243	-2.0.01960	-2.0.01960	1.0.00192	29.3.00000	6.00000
-7.0.13366	-2.0.73243	-2.0.01960	-2.0.01960	1.0.00192	28.4.00000	6.00000
-6.0.45277	-2.0.73243	-2.0.01960	-2.0.01960	1.0.00192	27.6.00000	6.00000
-9.0.71157	-10.3.41442	-2.0.73243	-3.0.01990	1.0.00192	26.70178	6.00000
-10.0.97097	-11.6.05052	-2.0.73243	-3.0.01990	1.0.00192	25.70422	6.00000
-12.0.25007	-12.4.54663	-2.0.73243	-3.0.01990	1.0.00192	24.8.00000	6.00000
-13.0.43016	-13.4.1471	-2.0.73243	-3.0.01990	1.0.00192	23.9.00000	6.00000
-13.0.22061	-9.5.62556	-2.0.73243	-2.0.01960	1.0.00192	27.6.0480	6.00000
-9.0.36044	0.21632	-2.0.73243	-2.0.01960	1.0.00192	26.70305	6.00000
7.0.54520	6.0.77055	-2.0.73243	-2.0.01960	1.0.00192	25.70178	6.00000
6.0.17696	5.0.52983	-2.0.73243	-2.0.01960	1.0.00192	25.70422	6.00000
4.0.35071	4.0.17759	-2.0.73243	-2.0.01960	1.0.00192	24.8.00000	6.00000
3.0.52447	2.0.5125	-2.0.73243	-2.0.01960	1.0.00192	23.9.00000	6.00000
2.0.15623	1.0.45511	-2.0.73243	-2.0.01960	1.0.00192	22.0.00000	6.00000
0.21169	0.13837	-2.0.73243	-2.0.01960	1.0.00192	21.0.00000	6.00000
4.0.52625	-1.0.26737	-2.0.73243	-2.0.01960	1.0.00192	20.3.00000	6.00000
-1.0.58049	-2.0.25361	-2.0.73243	-2.0.01960	1.0.00192	19.0.00000	6.00000
-3.0.22673	-3.0.97985	-2.0.73243	-2.0.01960	1.0.00192	18.0.00000	6.00000
-4.0.57297	-5.0.24469	-2.0.73243	-2.0.01960	1.0.00192	17.0.00000	6.00000
-5.0.91622	-6.0.39234	-2.0.73243	-2.0.01960	1.0.00192	16.0.00000	6.00000
-7.0.26145	-7.0.93562	-2.0.73243	-2.0.01960	1.0.00192	15.0.00000	6.00000
-8.0.61170	-9.0.20462	-2.0.73243	-2.0.01960	1.0.00192	14.0.00000	6.00000
-9.0.47794	-1.0.63106	-2.0.73243	-2.0.01960	1.0.00192	13.0.00000	6.00000
-11.0.20410	-1.0.97730	-2.0.73243	-2.0.01960	1.0.00192	12.0.00000	6.00000
-12.0.56042	-1.0.32356	-2.0.73243	-2.0.01960	1.0.00192	11.0.00000	6.00000
13.0.31811	1.0.57769	-2.0.73243	-2.0.01960	1.0.00192	10.0.00000	6.00000
11.0.93726	1.0.69654	-2.0.73243	-2.0.01960	1.0.00192	9.0.00000	6.00000
10.0.35641	3.0.61599	-2.0.73243	-2.0.01960	1.0.00192	8.0.00000	6.00000
6.0.97597	5.0.12515	-2.0.73243	-2.0.01960	1.0.00192	7.0.00000	6.00000
7.0.29472	6.0.64330	-2.0.73243	-2.0.01960	1.0.00192	6.0.00000	6.00000
5.0.31264	5.0.17449	-2.0.73243	-2.0.01960	1.0.00192	5.0.00000	6.00000
4.0.43303	3.0.49321	-2.0.73243	-2.0.01960	1.0.00192	4.0.00000	6.00000
2.0.95219	0.0.21176	-2.0.73243	-2.0.01960	1.0.00192	3.0.00000	6.00000
-4.0.45294	-5.0.16267	-2.0.73243	-2.0.01960	1.0.00192	2.0.00000	6.00000
-5.0.72259	-6.0.67031	-2.0.73243	-2.0.01960	1.0.00192	1.0.00000	6.00000
-7.0.41374	-8.0.15416	-2.0.73243	-2.0.01960	1.0.00192	0.0.00000	6.00000
-8.0.39456	-9.0.63560	-2.0.73243	-2.0.01960	1.0.00192	-1.0.00000	6.00000
-10.0.37543	-1.0.11085	-2.0.73243	-2.0.01960	1.0.00192	-2.0.00000	6.00000
-11.0.45667	-1.0.34878	-2.0.73243	-2.0.01960	1.0.00192	-3.0.00000	6.00000

16.40253	-1.87435	1.99147	37.88905
15.59261	-17.53321	-1.67435	1.99147
15.67736	-17.33321	-1.67435	1.99147
15.87756	-17.33321	-1.67435	1.99147
12.26151	-17.33321	-1.67435	1.99147
10.74645	-17.33321	-1.67435	1.99147
9.55414	-17.33321	-1.67435	1.99147
9.51372	-17.33321	-1.67435	1.99147
9.32276	-17.33321	-1.67435	1.99147
9.76761	-17.33321	-1.67435	1.99147
5.92234	-17.63321	-1.67435	1.99147
4.25465	-17.63321	-1.67435	1.99147
3.47093	-17.63321	-1.67435	1.99147
2.46920	-17.63321	-1.67435	1.99147
1.96146	1.00375	-1.67435	1.99147
2.4692	-5.56170	-1.67435	1.99147
-1.36542	-2.17715	-1.67435	1.99147
-2.36487	-3.76265	-1.67435	1.99147
-6.56631	-5.66655	-1.67435	1.99147
-6.51577	-7.02557	-1.67435	1.99147
-7.43122	-9.32665	-1.67435	1.99147
-5.44667	-10.25440	-1.67435	1.99147
-11.66212	-11.63695	-1.67435	1.99147
19.47235	18.60793	-13.87210	-1.67435
17.72291	16.19576	-12.67210	-1.65622
15.49265	15.10760	-12.67210	-1.45622
14.23280	15.35777	-13.67210	-1.45602
12.46276	12.46971	-13.67210	-1.45602
10.73265	9.65976	-13.07210	-1.45602
9.39263	9.10260	-13.67210	-1.45602
7.23257	6.35795	-13.67210	-1.45602
5.49242	4.67449	-12.67210	-1.45602
3.73264	2.75747	-13.67210	-1.45602
1.26241	1.15731	-13.67210	-1.45602
0.23237	-4.46267	-13.67210	-1.45602
-1.21770	-2.39273	-12.67210	-1.45602
-3.26774	-4.14278	-13.67210	-1.45602
-5.21771	-6.14286	-13.67210	-1.45602
-6.75772	-7.44289	-13.67210	-1.45602
-2.56772	-9.36295	-13.67210	-1.45602
-10.46276	-11.43295	-12.67210	-1.45602
-3.26774	-3.26774	-13.67210	-1.45602
-5.21771	-5.21771	-13.67210	-1.45602
-6.75772	-7.44289	-13.67210	-1.45602
-2.56772	-9.36295	-13.67210	-1.45602
-10.46276	-11.43295	-12.67210	-1.45602
22.54539	21.64206	-9.91099	-1.04169
20.68671	19.68671	-9.91099	-1.04169
18.79667	17.81174	-9.91099	-1.04169
15.91141	15.91141	-9.91099	-1.04169
16.72675	16.68442	-9.91099	-1.04169
13.44297	12.18376	-9.91099	-1.04169
10.51510	-9.21099	-9.91099	-1.04169
8.36264	-8.91099	-9.91099	-1.04169
6.65175	-6.91099	-9.91099	-1.04169
5.62245	4.66116	-9.91099	-1.04169
2.71471	2.77746	-9.91099	-1.04169
1.43471	1.43471	-9.91099	-1.04169
0.43413	0.43413	-9.91099	-1.04169
-0.50593	-0.99265	-9.91099	-1.04169

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REF. CHORD	CVERAGE	TRUE AREA	REFERENCE AREA	R/2	REF. AR	TRUE AR	MACH NUMBER
-1.93519	-2.87752	-2.71099	-1.04169	18.59357	1.99147	6.00000	27495
-3.21985	-4.76210	-2.31059	-1.04169	16.82693	1.99147	6.00000	27495
-5.70451	-5.6484	-2.71079	-1.04169	15.02672	1.99147	5.00000	27495
-7.69317	-4.53550	-2.71099	-1.04169	13.19564	1.99147	6.00000	27495
-6.47522	-1.04151	-2.71069	-1.04169	1.73247	11.33671	6.00000	27495
25.64742	24.23914	-5.64927	-5.64927	-6.2536	1.99147	37.8805	27649
22.52453	22.6192	-5.64927	-5.64927	-6.2526	1.99147	36.65626	27649
21.30922	20.57965	-5.64927	-5.64927	-6.2536	1.99147	35.38270	27649
18.29702	18.56939	-5.64927	-5.64927	-6.2536	1.99147	34.06763	27649
17.5776	16.36113	-5.64927	-5.64927	-6.2536	1.99147	32.71043	27649
15.55169	16.5626	-5.64927	-5.64927	-6.2536	1.99147	31.31065	27649
14.52222	14.52269	-5.64927	-5.64927	-6.2536	1.99147	29.86601	27649
11.12956	10.12932	-5.64927	-5.64927	-6.2536	1.99147	28.38241	27649
10.41664	2.49370	-5.64927	-5.64927	-6.2536	1.99147	26.85399	27649
7.44744	6.46650	-5.64927	-5.64927	-6.2536	1.99147	25.28316	27649
5.45617	4.44554	-5.64927	-5.64927	-6.2536	1.99147	23.67056	27649
3.43591	2.42627	-2.94237	-2.94237	-6.2536	1.99147	22.01719	27649
1.41664	1.41731	-5.64927	-5.64927	-6.2536	1.99147	20.32431	27649
-1.69652	-1.61721	-5.24387	-5.24387	-6.2536	1.99147	18.59357	27649
-2.62142	-3.63162	-5.74287	-5.74287	-6.2536	1.99147	16.82693	27649
-4.61115	-5.65079	-5.94997	-5.94997	-6.2536	1.99147	15.02672	27649
-6.63041	-7.67059	-5.64997	-5.64997	-6.2536	1.99147	13.19564	27649
-8.63796	-9.66921	-5.94997	-5.94997	-6.2536	1.99147	11.33671	27649
28.73343	27.65643	-1.93466	-1.93466	-20.860	1.99559	37.86905	27726
26.87642	25.50242	-1.98466	-1.98466	-20.860	1.99559	36.65626	27726
24.42542	23.76421	-1.98456	-1.98456	-20.860	1.99559	35.36270	27726
22.77141	21.10460	-1.90456	-1.90456	-20.860	1.99559	34.06763	27726
20.11740	19.04640	-1.05466	-1.05466	-20.860	1.99559	32.71043	27726
17.76333	16.37433	-1.27466	-1.27466	-20.860	1.99559	31.31065	27726
15.36938	14.78230	-1.98456	-1.98456	-20.860	1.99559	29.86801	27726
13.05537	12.57337	-1.98456	-1.98456	-20.860	1.99559	28.38241	27726
11.20137	10.62436	-1.98456	-1.98456	-20.860	1.99559	26.85399	27726
9.34736	8.27035	-1.28456	-1.28456	-20.860	1.99559	25.28316	27726
7.19334	6.11335	-1.98456	-1.98456	-20.860	1.99559	23.67056	27726
5.92934	3.56234	-1.98456	-1.98456	-20.860	1.99559	22.01719	27726
2.65537	1.65422	-1.98456	-1.98456	-20.860	1.99559	20.32431	27726
0.73132	-2.34552	-1.56465	-1.56465	-20.860	1.99559	18.59357	27726
-1.42265	-2.49262	-1.98456	-1.98456	-20.860	1.99559	16.82693	27726
-2.57669	-4.65370	-1.98456	-1.98456	-20.860	1.99559	15.02672	27726
-5.73070	-6.20770	-1.98466	-1.98466	-20.860	1.99559	13.19564	27726
-7.39471	-8.96171	-1.98466	-1.98466	-20.860	1.99559	11.33671	27726

A = 1.000000

F I R S T P L A N F O R M S P A N L O A D I N G

Y	CL+C
-71.05967	.28265
-70.25317	.65546
-69.60295	.85137
-67.35944	4.98427
-63.39533	5.7309
-59.43721	6.36234
-55.47610	6.90517
-51.51479	7.28248
-47.55397	7.00560
-43.59276	8.17307
-39.63164	8.49876
-35.67053	8.78426
-31.70941	9.03333
-28.73243	9.19549
-25.72544	9.34767
-21.72433	9.51519
-17.62321	9.65255
-13.87210	9.75213
-9.91099	9.84404
-5.94937	9.89900
-1.94656	9.92670

CL DEVELOPED ON THIS PLANFORM = .500091  
CH DEVELOPED ON THIS PLANFORM = -.128556

CL DESIGN = .500000 CH COMPUTED = .500091 CH COMPUTED = -.128556 CD V = .008141

## LOCAL ELEVATION DATA

Y = -72.0537      YFR/2 = -.58940      CHORD = 2.4614

## SLOPES, DIST, AT SLOPE POINTS, FROM FRONT TO REAR

• 5851 • 7224 • 5856 • 5244 • 6550 • 3956 • 3611 • 2912 • 2432 • 1964 • 1432 • 1003 • 0420 • 0101 • 0763 • 1661 • 3010 • 6781  
 CORRECTION POINTS X/C LOCATIONS FROM FRONT TO REAR  
 • 6117 • 3072 • 1523 • 2052 • 2639 • 3124 • 3750 • 4306 • 4861 • 5417 • 5972 • 6528 • 7083 • 7639 • 8194 • 8750 • 9306 • 9861

## LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
-6000	-2364	-0000	-5671
-5250	-2677	-0615	-5111
-4510	-1650	-1231	-4555
-3760	-1612	-1646	-4031
-3020	-1449	-2451	-3565
-2450	-1273	-2077	-3145
-1830	-1119	-3692	-2755
-1750	-0971	-4308	-2309
-2090	-0932	-4923	-2047
-2260	-0765	-5539	-1728
-2540	-0591	-6154	-1629
-2720	-0464	-6769	-1148
-3040	-0352	-7354	-6894
-3220	-0197	-8000	-6337
-3290	-0164	-8615	-0405
-3750	-2076	-9240	-0198
-4160	-5095	-9546	-0015
-4570	-0074	-1.0651	-0.0204
-4630	-0129	-1.1076	-0.0379
-4710	-0270	-1.1692	-0.0542
-4760	-0281	-1.2307	-0.0690
-5250	-0236	-1.7923	-0.0826
-5290	-0285	-1.3538	-0.0949
-5760	-0420	-1.4153	-0.1059
-6160	-0575	-1.6769	-0.1156
-6350	-0594	-1.5384	-0.1240
-6560	-0632	-1.5909	-0.1310

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• 6750	-• 0555	1.5615	-• 1266
• 7001	-• 0172	1.7225	-• 1409
• 7240	-• 0023	1.7545	-• 1425
• 7500	-• 0363	1.8661	-• 1446
• 7750	-• 0515	1.9075	-• 1441
• 8000	-• 0676	1.9591	-• 1419
• 8250	-• 0530	2.0307	-• 1377
• 8500	-• 0532	2.0922	-• 1310
• 8750	-• 0445	2.1522	-• 1213
• 9000	-• 0450	2.2193	-• 1108
• 9250	-• 0374	2.2768	-• 0971
• 9500	-• 0104	2.3354	-• 0753
• 9750	-• 0167	2.3933	-• 0612
1.0000	0.0000	2.4614	0.0000

Y\* -70.232 Y\* -70.12\* -5827 CHORD 3.7802

STOPE S, 97/98, AT SLOPE POINTS, FROM FRONT TO REAR  
 CHOPPER DRIVING Y/C LOCATIONS FROM FRONT TO REAR

• 6757 • 70.91 • 1366 • 5372 • 6552 • 3435 • 3164 • 2572 • 1093 • 1402 • 0.917 • 0.712 • 0.430 • 1.137 • 1.957 • 2.996 • 4.566 • 8.874  
 • 6417 • 0.972 • 1528 • 2043 • 2639 • 3194 • 3750 • 4306 • 4661 • 5417 • 5972 • 6528 • 7083 • 7639 • 8194 • 8750 • 9306 • 9861

LOCAL ELEVATION

Y/C	Z/C	DELTA X	DELTA Z
-0.6990	-0.1004	-0.0000	-6.821
-0.6250	-0.1570	-0.945	-5.893
-0.5500	-0.1115	-1.770	-4.971
-0.7790	-0.1617	-2.835	-4.107
-0.6660	-0.0474	-3.730	-3.324
-0.5235	-0.0764	-4.725	-2.662
-0.5016	-0.0528	-5.670	-2.035
-0.4710	-0.0383	-6.615	-1.450
-0.2220	-0.0240	-7.560	-0.607
-0.2250	-0.0167	-8.506	-0.406
-0.2500	-0.0016	-9.451	-0.059
-0.4750	-0.1350	-1.0375	-0.494
-0.3600	-0.0236	-1.1341	-0.692
-0.2250	-0.0734	-1.2266	-1.1263
-0.3500	-0.0424	-1.3231	-1.1604
-0.3750	-0.0209	-1.4176	-1.1919
-0.4000	-0.0524	-1.5121	-2.2206
-0.4250	-0.0453	-1.6066	-2.468
-0.4500	-0.0715	-1.7011	-2.2704
-0.4750	-0.0771	-1.7956	-2.2915
-0.5000	-0.0820	-1.8001	-3.101
-0.5250	-0.0743	-1.9646	-3.262
-0.5500	-0.0699	-2.0791	-3.3399
-0.5750	-0.0629	-2.1736	-3.511
-0.6000	-0.0552	-2.2681	-3.598
-0.6250	-0.0662	-2.3626	-3.660
-0.6500	-0.0674	-2.4571	-3.695
-0.6750	-0.0730	-2.5517	-3.705
-0.7000	-0.0776	-2.6462	-3.688
-0.7250	-0.0684	-2.7407	-3.642

ORIGINAL PAGE IS  
 OF POOR QUALITY

• 7500	• 0544	2.8352	• 3567
• 750	• 0916	2.9297	• 3461
• 6000	• 0879	3.0242	• 3324
• 2500	• 0323	2.1187	• 3151
• 1500	• 0775	3.2132	• 2931
• 5750	• 0705	3.3077	• 2667
• 9100	• 0627	3.4022	• 2370
• 2500	• 0532	3.4967	• 2023
• 6500	• 0406	3.5912	• 1534
• 9750	• 0213	3.6857	• 0829
1.0000	0.0000	3.7602	0.0000

Y= -59.6099      Y/P=2.0      -9737      CH020= 6.2535

SLIPES, D7/DY, AT SLICE POINTS, FROM FRONT TO REAR  
CORNERS FRONT X/C LOCATIONS FROM FRONT TO REAR  
• 5316 • 1672 • 4579 • 2279 • 1408 • 0764 • 0250 • 0172 • 0533 • 0959 • 1175 • 1504 • 1879 • 2349 • 3008 • 4092 • 7255  
• 0417 • 0972 • 1522 • 2082 • 2639 • 3154 • 3750 • 4106 • 4661 • 5117 • 5672 • 6528 • 7063 • 7639 • 8194 • 8750 • 9306 • 9861

LOCAL ELEVATION

X/C	Z/C	DELTAX	DELTAZ
-0.00	0.9598	-0.0000	373.0
.0250	0.9344	.1563	216.2
.0500	0.8995	.3127	559.9
.0750	0.8129	.4590	080.7
.1000	0.6912	.6254	1050.0
.1250	0.6160	.7817	287.7
.1500	0.5387	.9230	367.2
.1750	0.4696	1.0644	436.4
.2000	0.4072	1.2507	495.5
.2250	0.3472	1.4070	545.4
.2500	0.2939	1.5634	507.4
.2750	0.2496	1.7197	622.6
.3000	0.2042	1.9761	651.7
.3250	0.1609	2.0324	675.1
.3500	0.1109	2.1857	693.6
.3750	0.1132	2.3451	707.7
.4000	0.1148	2.5014	717.7
.4250	0.1156	2.6577	724.0
.4500	0.1163	2.8141	727.0
.4750	0.1163	2.9704	727.0
.5000	0.1163	3.1268	724.2
.5250	0.1160	3.2831	718.7
.5500	0.1157	3.4394	710.8
.5750	0.1150	3.5958	700.5
.6000	0.1140	3.7521	686.0
.6250	0.1076	3.9054	673.2
.6500	0.1049	4.0648	656.2
.6750	0.1019	4.2211	636.9
.7000	0.0984	4.3775	615.4
7250	0.0944	4.5338	595.5

ORIGINAL PAGE IS  
OF POOR QUALITY

•7500	-1.0903	4.6901	-•5649
•7750	-1.0357	4.8455	-•5357
•8000	-1.0295	5.0028	-•5037
•8250	-1.0748	5.1591	-•4681
•8500	-1.0584	5.3155	-•4278
•8750	-1.0612	5.4719	-•3826
•9000	-1.0534	5.6282	-•3342
•9250	-1.0448	5.7045	-•2903
•9500	-1.0135	5.9403	-•2094
•9750	-1.0174	6.0972	-•1122
1.0000	0.0000	6.2535	0.0000

Y = -67.3164      Y/R/2 = -0.9422      CHORD = 0.0225

STEPS, 22/10X, AT SLOPE POINTS, FROM FRONT TO REAR  
 •1240 •0724 •0707 •0536 •0382 •0257 •0136 •0024- •00P1- •0139- •0275- •0367- •0460- •0559- •0671- •0816- •1042- •1707  
 COPS SPACING X/C LOCATIONS FROM FRONT TO REAR

•6417 •6072 •1528 •2093 •2339 •3164 •3750 •4306 •4861 •5417 •5972 •6528 •7083 •7639 •8194 •8750 •9306 •9861

LOCAL ELEVATION

X/C	Z/C	7/C	DELTA X	DELTA Z
0.0000	-0.2005	0.0000	-0.0577	
•0250	-0.0047	•2206	-0.0857	
•0500	-0.5127	•411	-0.1135	
•0750	-0.012	•5617	-0.1391	
•1000	-0.0112	•6622	-0.1609	
•1250	-0.0294	1.1028	-0.1796	
•1500	-0.0222	1.3234	-0.1962	
•1750	-0.0235	1.5439	-0.2111	
•2000	-0.0254	1.7645	-0.2243	
•2250	-0.0257	1.9251	-0.2359	
•2500	-0.0279	2.0256	-0.2460	
•2750	-0.0293	2.4252	-0.2546	
•3000	-0.0297	2.6457	-0.2620	
•3250	-0.0304	2.8673	-0.2660	
•3500	-0.0309	3.0879	-0.2728	
•3750	-0.0313	3.3034	-0.2764	
•4000	-0.0316	3.5290	-0.2788	
•4250	-0.0317	3.7456	-0.2801	
•4500	-0.0319	3.9701	-0.2803	
•4750	-0.0317	4.1907	-0.2795	
•5000	-0.0315	4.4112	-0.2776	
•5250	-0.0311	4.6318	-0.2748	
•5500	-0.0307	4.9524	-0.2710	
•5750	-0.0302	5.0723	-0.2662	
•6000	-0.0295	5.2935	-0.2605	
•6250	-0.0289	5.5141	-0.2539	
•6500	-0.0279	5.7346	-0.2464	
•6750	-0.0272	5.9552	-0.2379	
•7000	-0.0259	6.1757	-0.2285	
•7250	-0.0247	6.3563	-0.2152	

•7500	-•0235	6•5169	-•2069
-7750	-•0221	6•8374	-•1946
-83000	-•0206	7•0000	-•1914
•1250	-•0100	7•2706	-•1669
•7760	-•0171	7•4911	-•1510
•81750	-•0161	7•7127	-•1336
•0000	-•0131	7•9402	-•1192
•9250	-•0128	8•1608	-•0952
•0500	-•0079	8•3814	-•0701
•9750	-•0042	8•6019	-•0373
1.00000	0.0000	8•3225	0.00000

ORIGINAL PAGE IS  
OF POOR QUALITY

Y = -62.3943      Y/E/2 = -.08868      CHORD = 10.2416

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.01221 .02995 .0539 .0532 .0404 .0299 .0137 .0089 .0005 .0098 .0191 .0288 .0390 .0502 .0632 .0797 .1046 .1730  
C/C: ESPC'DING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1522 .2083 .2639 .3191 .3759 .4306 .4961 .5417 .5972 .6523 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	Y/C	LOCAL ELEVATION	DELTA X	DELTA Z	DELTA Y
0.0000	-0.0035	0.0000	0.0000	-0.0355	-0.0355	-0.0355
.0250	-0.0055	.0250	.0250	-0.0670	-0.0670	-0.0670
.0500	-0.0096	.0512	.0512	-0.0983	-0.0983	-0.0983
.0750	-0.0124	.0763	.0763	-0.1271	-0.1271	-0.1271
.1000	-0.0142	.1024	.1024	-0.1516	-0.1516	-0.1516
.1250	-0.0160	.1250	.1250	-0.1726	-0.1726	-0.1726
.1500	-0.0167	.1517	.1517	-0.1914	-0.1914	-0.1914
.1750	-0.0203	.1793	.1793	-0.2063	-0.2063	-0.2063
.2000	-0.0218	.2000	.2000	-0.2234	-0.2234	-0.2234
.2250	-0.0231	.2304	.2304	-0.2368	-0.2368	-0.2368
.2500	-0.0243	.2505	.2505	-0.2486	-0.2486	-0.2486
.2750	-0.0253	.2755	.2755	-0.2591	-0.2591	-0.2591
.3000	-0.0252	.3072	.3072	-0.2661	-0.2661	-0.2661
.3250	-0.0259	.3285	.3285	-0.2759	-0.2759	-0.2759
.3500	-0.0276	.3564	.3564	-0.2825	-0.2825	-0.2825
.3750	-0.0281	.3807	.3807	-0.2878	-0.2878	-0.2878
.4000	-0.0295	.4053	.4053	-0.2920	-0.2920	-0.2920
.4250	-0.0299	.4329	.4329	-0.2951	-0.2951	-0.2951
.4500	-0.0320	.4616	.4616	-0.2971	-0.2971	-0.2971
.4750	-0.0321	.4849	.4849	-0.2980	-0.2980	-0.2980
.5000	-0.0321	.5120	.5120	-0.2978	-0.2978	-0.2978
.5250	-0.0290	.5377	.5377	-0.2956	-0.2956	-0.2956
.5500	-0.0287	.5633	.5633	-0.2943	-0.2943	-0.2943
.5750	-0.0284	.5891	.5891	-0.2949	-0.2949	-0.2949
.6000	-0.0280	.6146	.6146	-0.2864	-0.2864	-0.2864
.6250	-0.0274	.6412	.6412	-0.2808	-0.2808	-0.2808
.6500	-0.0263	.6597	.6597	-0.2741	-0.2741	-0.2741
.6750	-0.0262	.6713	.6713	-0.2663	-0.2663	-0.2663
.7000	-0.0251	.7162	.7162	-0.2574	-0.2574	-0.2574
.7250	-0.0241	.7454	.7454	-0.2472	-0.2472	-0.2472

7.500	7.6014	-2357
7.750	7.0375	-2229
8.000	6.1545	-2079
8.250	8.4496	-1931
8.500	8.7066	-1754
8.750	8.9617	-1556
9.000	9.2177	-1346
9.250	9.4734	-1117
9.500	9.7374	-0826
9.750	9.9919	-06429
10.000	10.2419	0.0000

31 3050 16000  
VIAJAS 8000 30

Y/3/2 - 2010-01-16 09:59:59.000000000

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CHOCOLATE 11.6613

SLOPES, 07/08, AT CLOSE POINTS, FROM FRONT TO REAR

לְכָאֵל אֶל-פְּרָתְּן

X/C	Z/C	DELTA X	DELTA Y	DELTA Z
0.6000	-0.051	0.2939	-0.0591	-0.0932
0.250	-0.3679	-0.2615	-0.5421	-0.1270
0.500	-0.0103	-0.7745	-0.1580	-0.1942
0.750	-0.2135	1.1561	-0.2066	-0.2265
1.000	-0.0132	1.4577	-0.2444	-0.2603
1.250	-0.0177	1.7492	-0.2743	-0.2865
1.500	-0.0104	2.0407	-0.2972	-0.3055
1.750	-0.0219	2.3223	-0.3143	-0.3208
2.000	-0.0223	2.6733	-0.3165	-0.3260
2.250	-0.0275	2.9153	-0.3299	-0.3342
2.500	-0.0246	3.2959	-0.3426	-0.3446
2.750	-0.0216	3.4686	-0.3538	-0.3550
3.000	-0.0243	3.6313	-0.3639	-0.3651
3.250	-0.0270	3.7162	-0.3730	-0.3742
3.500	-0.0275	4.0215	-0.3826	-0.3846
3.750	-0.0230	4.2730	-0.3929	-0.3946
4.000	-0.0283	4.6645	-0.4026	-0.4046
4.250	-0.0245	4.9561	-0.4122	-0.4146
4.500	-0.0257	5.2476	-0.4217	-0.4246
4.750	-0.0267	5.5391	-0.4313	-0.4346
5.000	-0.0286	5.8306	-0.4408	-0.4446
5.250	-0.0265	6.1222	-0.4503	-0.4546
5.500	-0.0292	6.4137	-0.4600	-0.4646
5.750	-0.0273	6.7052	-0.4696	-0.4746
6.000	-0.0274	6.9968	-0.3192	-0.3127
6.250	-0.0264	7.2883	-0.3050	-0.3030
6.500	-0.0242	7.5799	-0.2961	-0.2859
6.750	-0.0256	7.8714	-0.2766	-0.2744
7.000	-0.0245	8.1629	-0.2566	-0.2544
7.250	-0.0254	8.4544	-0.2366	-0.2344

ORIGINAL PAGE IS  
OF POOR QUALITY

*.7590	*.0224	0.7460	*.2615
-.7753	-.0212	9.0375	-.2473
-.5590	-.0159	5.3290	-.2215
*.6229	*.0184	9.6206	-.2141
,0560	*.0167	9.9121	-.1945
*.5750	*.0145	10.2056	-.1727
*.9069	*.0121	10.4952	-.1694
*.6250	*.0101	10.7867	-.1336
*.5500	*.0072	11.0782	-.0914
*.9750	*.0042	11.3693	-.0446
1.0000	0.0000	11.6613	0.0300

Y <sub>1</sub>	=	-55.4761	Y <sub>1</sub> P <sub>12</sub>	=	-0.7760	C4083	=	13.0307
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## LOCAL ELEVATION

DELTA Z	DELTA X	Z/C	X/C
-0.0000	-0.0000	-0.0075	-0.0000
-0.2700	-0.2700	-0.2183	-0.2183
-0.6540	-0.6540	-0.2139	-0.2139
-0.9111	-0.9111	-0.2135	-0.2135
-1.2051	-1.2051	-0.2176	-0.2176
-1.5251	-1.5251	-0.2134	-0.2134
-1.8621	-1.8621	-0.2210	-0.2210
-2.2191	-2.2191	-0.2124	-0.2124
-2.6161	-2.6161	-0.2146	-0.2146
-2.9452	-2.9452	-0.2247	-0.2247
-3.4792	-3.4792	-0.2137	-0.2137
-3.9772	-3.9772	-0.2164	-0.2164
-4.4742	-4.4742	-0.2172	-0.2172
-4.9742	-4.9742	-0.2177	-0.2177
-5.4742	-5.4742	-0.2169	-0.2169
-6.0051	-6.0051	-0.2145	-0.2145
-5.2363	-5.2363	-0.2134	-0.2134
-5.5563	-5.5563	-0.2150	-0.2150
-5.8663	-5.8663	-0.2139	-0.2139
-6.2131	-6.2131	-0.2120	-0.2120
-6.5403	-6.5403	-0.2116	-0.2116
-6.8574	-6.8574	-0.2156	-0.2156
-7.1944	-7.1944	-0.2133	-0.2133
-7.5214	-7.5214	-0.2179	-0.2179
-7.8444	-7.8444	-0.2174	-0.2174
-8.1754	-8.1754	-0.2168	-0.2168
-8.5025	-8.5025	-0.2160	-0.2160
-8.8295	-8.8295	-0.2152	-0.2152
-9.1555	-9.1555	-0.2143	-0.2143
-9.4825	-9.4825	-0.2133	-0.2133

ORIGINAL PAGE IS  
OF POOR QUALITY

• 7500	-.0222	• 8105	-.2904
• 7750	-.0210	16.1275	-.2741
• 8000	-.0196	16.4646	-.2563
• 8250	-.0181	16.7916	-.2367
• 8500	-.0167	17.1136	-.2147
• 8750	-.0145	17.4555	-.1965
• 9000	-.0126	11.7726	-.1646
• 9250	-.0104	12.0646	-.1361
• 9500	-.0087	12.4267	-.1064
• 9750	-.0061	12.7537	-.0534
1.0000	0.0000	13.0637	0.0000

Y =  $-37.0 \cdot 5459$       Y =  $13/2 = -7206$       CHOPE = 14.5001

Y/3/2 = -0.7206

Y/9/2 - -7206 CHORD - 14.5001

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	0.0000	-1.4268	-1.1803
-0.0250	-0.0224	-3.6255	-2.1755
-0.0500	-0.0550	-7.2500	-2.1755
-0.0750	-0.0773	1.0675	-2.7954
-0.1000	-0.0953	1.4500	-3.0319
-0.1250	-0.1019	1.6125	-3.0319
-0.1500	-0.1054	2.1750	-3.2428
-0.1750	-0.1087	2.3575	-3.6255
-0.2000	-0.0943	2.9000	-3.5999
-0.2250	-0.0756	3.2625	-3.7400
-0.2500	-0.0546	2.6250	-3.6622
-0.2750	-0.0373	3.0975	-3.9655
-0.3000	-0.0170	4.3500	-4.0522
-0.3250	-0.0094	4.7125	-4.1222
-0.3500	-0.0014	5.0750	-4.1776
-0.3750	-0.0061	5.4375	-4.2116
-0.4000	-0.0132	5.9000	-4.2441
-0.4250	-0.0230	6.1625	-4.2533
-0.4500	-0.0293	6.5250	-4.2500
-0.4750	-0.0392	6.8875	-4.2335
-0.5000	-0.0500	7.2500	-4.2066
-0.5250	-0.0687	7.6125	-4.1646
-0.5500	-0.0852	7.9751	-4.1099
-0.5750	-0.0979	8.3376	-4.0441
-0.6000	-0.0733	8.7091	-3.9660
-0.6250	-0.0267	9.0626	-3.8655
-0.6500	-0.0259	9.4251	-3.7558
-0.6750	-0.0251	9.7075	-3.6336
-0.7000	-0.0241	10.1501	-3.5000
-0.7250	-0.0231	10.5125	-3.3160

•7500	-.0220	10.8751	-.3183
•7750	-.0207	11.2376	-.3001
•8000	-.0163	11.6001	-.2862
•8250	-.0178	11.9626	-.2524
•8500	-.0161	12.3221	-.2341
•8750	-.0143	12.6876	-.2073
•9000	-.0123	13.0591	-.1799
•9250	-.0102	13.4126	-.1477
•9500	-.0075	13.7751	-.1087
•9750	-.0040	14.1375	-.0578
1.0000	0.0000	14.5661	0.0000

Y<sub>2</sub> = -47.5529      Y<sub>3/2</sub> = -6652      CHORD = 15.9195

SUMMARY OF SLOPES AT SLOPE POINTS FROM FRONT TO REAR

• 0.0000 • 0.074 • 0.093 • 0.0356 • 0.0693 • 0.0243 • 0.0145 • 0.0057 • 0.025 • 0.0101 • 0.0248 • 0.0337 • 0.0421 • 0.0514 • 0.0623 • 0.0763 • 0.0977 • 0.1574  
 • 0.0000      0.074      0.093      0.0356      0.0693      0.0243      0.0145      0.0057      0.025      0.0101      0.0248      0.0337      0.0421      0.0514      0.0623      0.0763      0.0977      0.1574  
 • 0.0000      0.074      0.093      0.0356      0.0693      0.0243      0.0145      0.0057      0.025      0.0101      0.0248      0.0337      0.0421      0.0514      0.0623      0.0763      0.0977      0.1574

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0123	0.0000	-0.1953
• 0.0250	-0.0147	• 32.30	-0.2336
• 0.0500	-0.0271	• 796.50	-0.2720
• 0.0750	-0.0593	1.1940	-0.3069
• 0.1000	-0.0211	1.5919	-0.3359
• 0.1250	-0.0226	1.9659	-0.3601
• 0.1500	-0.0219	2.3079	-0.3812
• 0.1750	-0.0251	2.7159	-0.3998
• 0.2000	-0.0261	3.1539	-0.4150
• 0.2250	-0.0273	3.5619	-0.4298
• 0.2500	-0.0277	3.9769	-0.4415
• 0.2750	-0.0283	4.3779	-0.4513
• 0.3000	-0.0278	4.7750	-0.4592
• 0.3250	-0.0293	5.1738	-0.4675
• 0.3500	-0.0295	5.5719	-0.4761
• 0.3750	-0.0297	5.9698	-0.4732
• 0.4000	-0.0298	6.3678	-0.4747
• 0.4250	-0.0293	6.7658	-0.4747
• 0.4500	-0.0297	7.1639	-0.4733
• 0.4750	-0.0296	7.5618	-0.4705
• 0.5000	-0.0292	7.9597	-0.4653
• 0.5250	-0.0289	8.3577	-0.4607
• 0.5500	-0.0285	8.7557	-0.4534
• 0.5750	-0.0280	9.1537	-0.4494
• 0.6000	-0.0274	9.5517	-0.4357
• 0.6250	-0.0267	9.9497	-0.4246
• 0.6500	-0.0259	10.3477	-0.4121
• 0.6750	-0.0260	10.7457	-0.3991
• 0.7000	-0.0264	11.1436	-0.3826
• 0.7250	-0.0265	11.5416	-0.3655

75.00	-.0212	11.9396
77.50	-.0205	12.3375
80.00	-.0191	12.7355
82.50	-.0176	13.1336
85.00	-.0159	13.5315
87.50	-.0141	12.9295
90.00	-.0121	14.3275
92.50	-.0109	14.7255
95.00	-.0097	15.1235
97.50	-.0083	15.5215
100.00	-.0066	15.9195
		0.0000

ORIGINAL PAGE IS  
OF POOR QUALITY

Yr - 1.3.5.28 Y/R 28 - .6008 - .6008 CHORD 17.3369

SLIDES, 2077DX, AT SLOPE POINTS, FROM FRONT TO REAR

.5236 .2620 .5446 .5315 .3255 .5117 .6027 .0051 .0126 .0200 .0273 .0349 .0429 .0519 .0622 .0756 .0961 .1534  
COPPIES SHOWING X/C LOCATIONS FOR FRONT TO REAR

.2617 .0671 .1728 .2043 .2623 .3174 .3750 .6526 .4361 .5417 .5972 .6528 .7003 .7639 .8194 .8750 .9106 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	0.063	0.0000	.2488
.0250	.0163	.4335	.2680
.0500	.0223	.3669	.3269
.0750	.0209	1.3694	.3622
.1000	.0226	1.7343	.3914
.1250	.0145	2.1674	.4155
.1500	.0252	2.6506	.4365
.1750	.0252	3.0243	.4546
.2000	.0271	3.4673	.4705
.2250	.0279	3.9013	.4838
.2500	.0256	4.1647	.4946
.2750	.0261	4.7642	.5039
.3000	.0275	5.2017	.5110
.3250	.0292	5.6351	.5164
.3500	.0309	6.0646	.5200
.3750	.0301	6.5224	.5220
.4000	.0301	6.9236	.5224
.4250	.0261	7.3460	.5213
.4500	.0274	7.4629	.5156
.4750	.0227	8.2360	.5145
.5000	.0174	8.6676	.5090
.5250	.0250	9. LC29	.5020
.5500	.0285	0.5354	.4935
.5750	.0279	9.9649	.4837
.6000	.0272	10.4033	.4724
.6250	.0265	10.8362	.4597
.6500	.0257	11.2703	.4454
.6750	.0243	11.7638	.4297
.7000	.0228	12.1272	.4125
.7250	.0224	12.5707	.3961

172.09	12.0042	-1.2729
177.56	12.4275	-1.3566
182.03	12.8711	-1.3264
186.50	13.0173	-1.3061
190.97	13.0156	-1.2866
195.44	13.0158	-1.2711
200.91	13.0159	-1.2594
205.38	13.0159	-1.2559
210.85	13.0161	-1.2494
215.32	13.0161	-1.2442
220.79	13.0162	-1.2342
226.26	13.0162	-1.0659
231.73	13.0000	0.0000

ORIGINAL PAGE IS  
OF POOR QUALITY

Y = -39.6315      Y/9/2 = -.5544      CHORD = 18.7583

SLOPES,DX/CHORD AT SLOPE POINTS, FROM FRONT TO REAR

.00747 .00777 .00773 .0158 .00770 .0079 .0079 .0151 .0221 .0291 .0363 .0439 .0524 .0623 .0750 .0947 .1496  
CHORD SPECIFYING X/C LOCATIONS FROM FRONT TO REAR  
.6117 .5972 .1522 .2623 .2639 .3104 .3750 .4306 .4661 .5417 .5972 .6528 .7053 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.7950	-.0166	0.0000	-.3107
.5950	-.0157	.4149	-.3501
.4950	-.0203	.9379	-.3692
.3950	-.0226	1.4069	-.4246
.2950	-.0242	1.9753	-.4536
.1950	-.0254	2.4468	-.4774
.0950	-.0265	2.8157	-.4976
-.0950	-.0275	3.2927	-.5154
-.1950	-.0275	3.7617	-.5304
-.2950	-.0279	4.2226	-.5428
-.3950	-.0282	4.6125	-.5529
-.4950	-.0289	5.1592	-.5609
-.5950	-.0292	5.6275	-.5669
-.6950	-.0294	6.0954	-.5711
-.7950	-.0296	6.5634	-.5735
-.8950	-.0298	7.0364	-.5741
-.9950	-.0300	7.5093	-.5731
-.4950	-.0304	7.9723	-.5704
-.5950	-.0305	8.4412	-.5644
-.6950	-.0306	8.9102	-.5608
-.7950	-.0308	9.3791	-.5536
-.8950	-.0311	9.8481	-.5459
-.9950	-.0314	10.3171	-.5249
-.4950	-.0315	10.7860	-.5233
-.5950	-.0317	11.2550	-.5102
-.6950	-.0319	11.7239	-.4957
-.7950	-.0322	12.1922	-.4796
-.8950	-.0325	12.6619	-.4619
-.9950	-.0325	13.1303	-.4427
-.7250	-.0325	13.5996	-.4218

17.750	17.0213	16.0627	15.3991
17.750	17.0200	16.5377	17.3747
17.750	17.014	16.6965	17.3493
17.750	17.0171	15.4756	17.2196
17.750	17.0164	15.4466	17.2112
17.750	17.015	15.4139	17.2144
17.750	17.014	15.3829	17.2144
17.750	17.013	17.3414	17.1193
17.750	17.012	17.3204	17.1213
17.750	17.0117	18.2693	17.0695
17.750	17.0000	18.7523	0.0000

ORIGINAL PAGE IS  
OF POOR QUALITY

Y<sub>0</sub> = -15.4705      Y<sub>10/20</sub> = -4.920      CHORD = 20.1777

CLIPPING DIVERGENT SLOPE POINTS, FRONT TO REAR

• 9749 .0513 .9250 .0223 .3127 .0046-.0111-.0160-.0247-.0313-.0454-.0534-.0628-.0749-.0936-.1463  
 CIRCLES DETERMINING X/C LOCATIONS FROM FRONT TO REAR  
 • 3417 .2772 .1529 .2683 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7063 .7539 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.6000	-0.100	0.0000	-3.860
0.6050	-0.011	.5044	-4.251
0.6100	-0.030	1.0039	-4.639
0.6150	-0.047	1.5133	-4.960
0.6200	-0.061	2.0174	-5.273
0.6250	-0.073	2.5122	-5.501
0.6300	-0.082	3.0267	-5.695
0.6350	-0.090	3.5311	-5.761
0.6400	-0.097	4.0355	-5.800
0.6450	-0.093	4.5450	-6.110
0.6500	-0.097	5.0644	-6.197
0.6550	-0.0910	5.5449	-6.262
0.6600	-0.0813	6.0533	-6.307
0.6650	-0.0714	6.5579	-6.332
0.6700	-0.0714	7.0622	-6.337
0.6750	-0.0714	7.5666	-6.328
0.6800	-0.0712	8.0711	-6.301
0.6850	-0.0712	8.5755	-6.256
0.6900	-0.0707	9.0800	-6.196
0.6950	-0.0703	9.5844	-6.120
0.7000	-0.0700	10.0888	-6.028
0.7050	-0.0692	10.5933	-5.921
0.7100	-0.0687	11.0977	-5.769
0.7150	-0.0681	11.6022	-5.562
0.7200	-0.0673	12.1066	-5.510
0.7250	-0.0665	12.6111	-5.343
0.7300	-0.0656	13.1155	-5.160
0.7350	-0.0649	13.6179	-4.961
0.7400	-0.0642	14.1244	-4.746
0.7444	-0.0638	14.6348	-4.514

ORIGINAL PAGE IS  
OF POOR QUALITY

-0.7500	-0.0211	15.1333	-0.4264
-0.7700	-0.0195	15.6377	-0.3605
-0.7900	-0.0174	16.1422	-0.3709
-0.8100	-0.0154	16.6456	-0.3399
-0.8250	-0.0165	17.1510	-0.2061
-0.8250	-0.0152	17.6555	-0.2695
-0.8750	-0.0134	18.1639	-0.2309
-0.9000	-0.0114	18.6644	-0.1392
-0.9250	-0.0094	19.1638	-0.1392
-0.9750	-0.0066	19.6733	-0.0731
-0.9750	-0.0026	20.1777	0.0000
1.0000	0.0000		

Y<sub>r</sub> = 51.07054, Y<sub>1/2</sub> = -0.67055, Y<sub>3/2</sub> = -0.67055, CHORD = 21.5971

STATION, SURFACE, AT SURFACE POINTS, FROM FRONT TO REAR  
CROSSING X/R LOCATIONS FROM FRONT TO REAR

• 57.11 • 54.52 • 52.95 • 51.75 • 50.76 • 50.03 • 49.36 • 48.15 • 47.07 • 46.25 • 45.52 • 44.83 • 44.20 • 43.62 • 43.04 • 42.50 • 41.96 • 41.42 • 40.90 • 40.40 • 40.00 • 39.60 • 39.20 • 38.80 • 38.40 • 38.00 • 37.60 • 37.20 • 36.80 • 36.40 • 36.00 • 35.60 • 35.20 • 34.80 • 34.40 • 34.00 • 33.60 • 33.20 • 32.80 • 32.40 • 32.00 • 31.60 • 31.20 • 30.80 • 30.40 • 30.00 • 29.60 • 29.20 • 28.80 • 28.40 • 28.00 • 27.60 • 27.20 • 26.80 • 26.40 • 26.00 • 25.60 • 25.20 • 24.80 • 24.40 • 24.00 • 23.60 • 23.20 • 22.80 • 22.40 • 22.00 • 21.60 • 21.20 • 20.80 • 20.40 • 20.00 • 19.60 • 19.20 • 18.80 • 18.40 • 18.00 • 17.60 • 17.20 • 16.80 • 16.40 • 16.00 • 15.60 • 15.20 • 14.80 • 14.40 • 14.00 • 13.60 • 13.20 • 12.80 • 12.40 • 12.00 • 11.60 • 11.20 • 10.80 • 10.40 • 10.00 • 9.60 • 9.20 • 8.80 • 8.40 • 8.00 • 7.60 • 7.20 • 6.80 • 6.40 • 6.00 • 5.60 • 5.20 • 4.80 • 4.40 • 4.00 • 3.60 • 3.20 • 2.80 • 2.40 • 2.00 • 1.60 • 1.20 • 0.80 • 0.40 • 0.00

LOCAL ELEVATION

X/R	Y/R	Z/R	DELTA Y	DELTA Z
0.0560	-0.2229	0.0000	-49.53	
0.2278	-0.9247	-1.29	-52.36	
0.3986	-0.8265	1.0799	-57.24	
0.5694	-0.8273	1.6159	-60.53	
0.7302	-0.8279	2.4137	-62.72	
0.8910	-0.8284	3.4664	-64.37	
0.9518	-0.8284	3.2346	-67.14	
1.1126	-0.8284	3.7765	-69.62	
1.2734	-0.8283	4.3196	-69.63	
1.4342	-0.8287	4.3593	-70.70	
1.5950	-0.8290	5.3993	-71.35	
1.7558	-0.8292	5.9592	-71.77	
1.9166	-0.8293	6.4791	-71.69	
2.0774	-0.8292	7.0291	-71.62	
2.2382	-0.8292	7.5599	-71.60	
2.3990	-0.8292	8.0936	-71.43	
2.5608	-0.8292	8.6309	-70.68	
2.7216	-0.8295	9.1769	-70.16	
2.8824	-0.8221	9.7147	-69.26	
3.0432	-0.8156	10.2549	-68.21	
3.2040	-0.8110	10.7863	-66.99	
3.3648	-0.8064	11.3203	-65.67	
3.5256	-0.8027	11.8684	-64.08	
3.6864	-0.7970	12.4183	-63.40	
3.8472	-0.7913	12.9580	-60.55	
4.0080	-0.7859	13.4694	-58.55	
4.1688	-0.7821	14.0231	-56.39	
4.3296	-0.7750	14.6736	-54.07	
4.4904	-0.7674	15.3146	-51.99	
4.6512	-0.7590	15.9559	-48.94	

• 7500	-0.018	16.1572	-4.606
• 7570	-0.016	16.7577	-6.107
• 7640	-0.014	17.2777	-39.86
• 7710	-0.012	17.7775	-36.63
• 7780	-0.010	18.2575	-32.71
• 7850	-0.008	18.7775	-28.72
• 7920	-0.006	19.3375	-24.53
• 7990	-0.004	19.8375	-20.01
• 8060	-0.002	20.3375	-16.59
• 8130	-0.001	20.8372	-0.770
• 8200	0.000	21.3372	0.0000
• 8270	0.000	21.8371	

Y2 = 12.7126 Y3 = 7.72\* Y4 = 7.72\* CHG2D = 22.6630

4.000E-5\*0.0710X, AT SLOPE FRONT, FROM FRONT TO REAR

\* 6.37 -0.01 0.0003 -0.127 -0.2121 -0.3645 -0.125 -0.210 -0.248 -0.0354 -0.0425 -0.0427 -0.0556 -0.0629 -0.0713 -0.0816 -0.0972 -0.1434

\* 6.37 -0.072 -0.129 -0.203 -0.269 -0.3156 -0.3750 -0.4304 -0.4633 -0.5127 -0.5572 -0.5928 -0.7093 -0.7639 -0.8194 -0.8750 -0.9306 -0.9861

UNITS: METERS

Z/6	DELTA X	DELTA Z
0.8809	-0.9246	0.3990
-0.9259	-0.9537	-0.5656
-0.9799	-0.9123	-1.1322
-0.9749	-0.9183	1.6995
-0.9599	-0.9744	2.4464
-0.9250	-0.9552	2.4210
-0.9159	-0.9559	3.3095
-0.9252	-0.9562	3.7542
-0.9253	-0.9563	4.5532
-0.9254	-0.9572	5.0634
-0.9254	-0.9573	5.5650
-0.9254	-0.9574	6.2364
-0.9254	-0.9574	6.7592
-0.9255	-0.9572	7.3458
-0.9255	-0.9579	7.9723
-0.9255	-0.9557	8.4768
-0.9255	-0.9553	9.0655
-0.9255	-0.9554	9.5371
-0.9255	-0.9552	10.1047
-0.9255	-0.9544	10.7733
-0.9250	-0.9557	11.3119
-0.9250	-0.9550	11.8985
-0.9250	-0.9574	12.4691
-0.9250	-0.9512	13.0717
-0.9250	-0.9507	13.5983
-0.9250	-0.9591	14.1640
-0.9250	-0.9576	14.7315
-0.9250	-0.9557	15.2891
-0.9250	-0.9554	15.3647
-0.9250	-0.9523	15.4312

ORIGINAL PAGE IS  
OF POOR QUALITY

14.2579	15.2643	16.1331	17.5649	18.6735	19.5944	20.6277	21.5507	22.6138	23.6973	24.5966	25.5000	26.4992	27.4984	28.4976	29.4968	30.4960	31.4952	32.4944	33.4936	34.4928	35.4920	36.4912	37.4904	38.4896	39.4888	40.4880	41.4872	42.4864	43.4856	44.4848	45.4840	46.4832	47.4824	48.4816	49.4808	50.4800	51.4792	52.4784	53.4776	54.4768	55.4760	56.4752	57.4744	58.4736	59.4728	60.4720	61.4712	62.4704	63.4696	64.4688	65.4680	66.4672	67.4664	68.4656	69.4648	70.4640	71.4632	72.4624	73.4616	74.4608	75.4600	76.4592	77.4584	78.4576	79.4568	80.4560	81.4552	82.4544	83.4536	84.4528	85.4520	86.4512	87.4504	88.4496	89.4488	90.4480	91.4472	92.4464	93.4456	94.4448	95.4440	96.4432	97.4424	98.4416	99.4408	100.4400	101.4392	102.4384	103.4376	104.4368	105.4360	106.4352	107.4344	108.4336	109.4328	110.4320	111.4312	112.4304	113.4296	114.4288	115.4280	116.4272	117.4264	118.4256	119.4248	120.4240	121.4232	122.4224	123.4216	124.4208	125.4200	126.4192	127.4184	128.4176	129.4168	130.4160	131.4152	132.4144	133.4136	134.4128	135.4120	136.4112	137.4104	138.4096	139.4088	140.4080	141.4072	142.4064	143.4056	144.4048	145.4040	146.4032	147.4024	148.4016	149.4008	150.4000	151.4092	152.4084	153.4076	154.4068	155.4060	156.4052	157.4044	158.4036	159.4028	160.4020	161.4012	162.4004	163.4000	164.4092	165.4084	166.4076	167.4068	168.4060	169.4052	170.4044	171.4036	172.4028	173.4020	174.4012	175.4004	176.4000	177.4092	178.4084	179.4076	180.4068	181.4060	182.4052	183.4044	184.4036	185.4028	186.4020	187.4012	188.4004	189.4000	190.4092	191.4084	192.4076	193.4068	194.4060	195.4052	196.4044	197.4036	198.4028	199.4020	200.4012	201.4004	202.4000	203.4092	204.4084	205.4076	206.4068	207.4060	208.4052	209.4044	210.4036	211.4028	212.4020	213.4012	214.4004	215.4000	216.4092	217.4084	218.4076	219.4068	220.4060	221.4052	222.4044	223.4036	224.4028	225.4020	226.4012	227.4004	228.4000	229.4092	230.4084	231.4076	232.4068	233.4060	234.4052	235.4044	236.4036	237.4028	238.4020	239.4012	240.4004	241.4000	242.4092	243.4084	244.4076	245.4068	246.4060	247.4052	248.4044	249.4036	250.4028	251.4020	252.4012	253.4004	254.4000	255.4092	256.4084	257.4076	258.4068	259.4060	260.4052	261.4044	262.4036	263.4028	264.4020	265.4012	266.4004	267.4000	268.4092	269.4084	270.4076	271.4068	272.4060	273.4052	274.4044	275.4036	276.4028	277.4020	278.4012	279.4004	280.4000	281.4092	282.4084	283.4076	284.4068	285.4060	286.4052	287.4044	288.4036	289.4028	290.4020	291.4012	292.4004	293.4000	294.4092	295.4084	296.4076	297.4068	298.4060	299.4052	300.4044	301.4036	302.4028	303.4020	304.4012	305.4004	306.4000	307.4092	308.4084	309.4076	310.4068	311.4060	312.4052	313.4044	314.4036	315.4028	316.4020	317.4012	318.4004	319.4000	320.4092	321.4084	322.4076	323.4068	324.4060	325.4052	326.4044	327.4036	328.4028	329.4020	330.4012	331.4004	332.4000	333.4092	334.4084	335.4076	336.4068	337.4060	338.4052	339.4044	340.4036	341.4028	342.4020	343.4012	344.4004	345.4000	346.4092	347.4084	348.4076	349.4068	350.4060	351.4052	352.4044	353.4036	354.4028	355.4020	356.4012	357.4004	358.4000	359.4092	360.4084	361.4076	362.4068	363.4060	364.4052	365.4044	366.4036	367.4028	368.4020	369.4012	370.4004	371.4000	372.4092	373.4084	374.4076	375.4068	376.4060	377.4052	378.4044	379.4036	380.4028	381.4020	382.4012	383.4004	384.4000	385.4092	386.4084	387.4076	388.4068	389.4060	390.4052	391.4044	392.4036	393.4028	394.4020	395.4012	396.4004	397.4000	398.4092	399.4084	400.4076	401.4068	402.4060	403.4052	404.4044	405.4036	406.4028	407.4020	408.4012	409.4004	410.4000	411.4092	412.4084	413.4076	414.4068	415.4060	416.4052	417.4044	418.4036	419.4028	420.4020	421.4012	422.4004	423.4000	424.4092	425.4084	426.4076	427.4068	428.4060	429.4052	430.4044	431.4036	432.4028	433.4020	434.4012	435.4004	436.4000	437.4092	438.4084	439.4076	440.4068	441.4060	442.4052	443.4044	444.4036	445.4028	446.4020	447.4012	448.4004	449.4000	450.4092	451.4084	452.4076	453.4068	454.4060	455.4052	456.4044	457.4036	458.4028	459.4020	460.4012	461.4004	462.4000	463.4092	464.4084	465.4076	466.4068	467.4060	468.4052	469.4044	470.4036	471.4028	472.4020	473.4012	474.4004	475.4000	476.4092	477.4084	478.4076	479.4068	480.4060	481.4052	482.4044	483.4036	484.4028	485.4020	486.4012	487.4004	488.4000	489.4092	490.4084	491.4076	492.4068	493.4060	494.4052	495.4044	496.4036	497.4028	498.4020	499.4012	500.4004	501.4000	502.4092	503.4084	504.4076	505.4068	506.4060	507.4052	508.4044	509.4036	510.4028	511.4020	512.4012	513.4004	514.4000	515.4092	516.4084	517.4076	518.4068	519.4060	520.4052	521.4044	522.4036	523.4028	524.4020	525.4012	526.4004	527.4000	528.4092	529.4084	530.4076	531.4068	532.4060	533.4052	534.4044	535.4036	536.4028	537.4020	538.4012	539.4004	540.4000	541.4092	542.4084	543.4076	544.4068	545.4060	546.4052	547.4044	548.4036	549.4028	550.4020	551.4012	552.4004	553.4000	554.4092	555.4084	556.4076	557.4068	558.4060	559.4052	560.4044	561.4036	562.4028	563.4020	564.4012	565.4004	566.4000	567.4092	568.4084	569.4076	570.4068	571.4060	572.4052	573.4044	574.4036	575.4028	576.4020	577.4012	578.4004	579.4000	580.4092	581.4084	582.4076	583.4068	584.4060	585.4052	586.4044	587.4036	588.4028	589.4020	590.4012	591.4004	592.4000	593.4092	594.4084	595.4076	596.4068	597.4060	598.4052	599.4044	600.4036	601.4028	602.4020	603.4012	604.4004	605.4000	606.4092	607.4084	608.4076	609.4068	610.4060	611.4052	612.4044	613.4036	614.4028	615.4020	616.4012	617.4004	618.4000	619.4092	620.4084	621.4076	622.4068	623.4060	624.4052	625.4044	626.4036	627.4028	628.4020	629.4012	630.4004	631.4000	632.4092	633.4084	634.4076	635.4068	636.4060	637.4052	638.4044	639.4036	640.4028	641.4020	642.4012	643.4004	644.4000	645.4092	646.4084	647.4076	648.4068	649.4060	650.4052	651.4044	652.4036	653.4028	654.4020	655.4012	656.4004	657.4000	658.4092	659.4084	660.4076	661.4068	662.4060	663.4052	664.4044	665.4036	666.4028	667.4020	668.4012	669.4004	670.4000	671.4092	672.4084	673.4076	674.4068	675.4060	676.4052	677.4044	678.4036	679.4028	680.4020	681.4012	682.4004	683.4000	684.4092	685.4084	686.4076	687.4068	688.4060	689.4052	690.4044	691.4036	692.4028	693.4020	694.4012	695.4004	696.4000	697.4092	698.4084	699.4076	700.4068	701.4060	702.4052	703.4044	704.4036	705.4028	706.4020	707.4012	708.4004	709.4000	710.4092	711.4084	712.4076	713.4068	714.4060	715.4052	716.4044	717.4036	718.4028	719.4020	720.4012	721.4004	722.4000	723.4092	724.4084	725.4076	726.4068	727.4060	728.4052	729.4044	730.4036	731.4028	732.4020	733.4012	734.4004	735.4000	736.4092	737.4084	738.4076	739.4068	740.4060	741.4052	742.4044	743.4036	744.4028	745.4020	746.4012	747.4004	748.4000	749.4092	750.4084	751.4076	752.4068	753.4060	754.4052	755.4044	756.4036	757.4028	758.4020	759.4012	760.4004	761.4000	762.4092	763.4084	764.4076	765.4068	766.4060	767.4052	768.4044	769.4036	770.4028	771.4020	772.4012	773.4004	774.4000	775.4092	776.4084	777.4076	778.4068	779.4060	780.4052	781.4044	782.4036	783.4028	784.4020	785.4012	786.4004	787.4000	788.4092	789.4084	790.4076	791.4068	792.4060	793.4052	794.4044	795.4036	796.4028	797.4020	798.4012	799.4004	800.4000	801.4092	802.4084	803.4076	804.4068	805.4060	806.4052	807.4044	808.4036	809.4028	810.4020	811.4012	812.4004	813.4000	814.4092	815.4084	816.4076	817.4068	818.4060	819.4052	820.4044	821.4036	822.4028	823.4020	824.4012	825.4004	826.4000	827.4092	828.4084	829.4076	830.4068	831.4060	832.4052	833.4044	834.4036	835.4028	836.4020	837.4012	838.4004	839.4000	840.4092	841.4084	842.4076	843.4068	844.4060	845.4052	846.4044	847.4036	848.4028	849.4020	850.4012	851.4004	852.4000	853.4092	854.4084	855.4076	856.4068	857.4060	858.4052	859.4044	860.4036	861.4028	862.4020	863.4012	864.4004	865.4000	866.4092	867.4084	868.4076	869.4068	870.4060	871.4052	872.4044	873.4036	874.4028	875.4020	876.4012	877.4004	878.4000	879.4092	880.4084	881.4076	882.4068	883.4060	884.4052	885.4044	886.4036	887.4028	888.4020	889.4012	890.4004	891.4000	892.4092	893.4084	894.
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Y\* = -25.7554      Y/5/2 = -3603      CHORD= 24.2323

STATION 5,007 EXTRAPOLATED STATION POINTS, EACH FRONT TO REAR  
CROSS SECTIONING X/C LOCATIONS FWD FRONT TO REAR

\*.0617 \*.0772 \*1521 \*2043 \*2639 \*3104 \*3730 \*4305 \*4761 \*5217 \*5972 \*6528 \*7093 \*7639 \*8194 \*8750 \*9306 \*9861

LOCAL ELEVATION

X/C	Y/C	Z/C	LOCAL ELEVATION	DELTA X	DELTA Z
0.0000	-0.9275	0.0000	0.0000	-6.693	-7.6947
0.0000	-0.9191	0.0000	0.0000	-7.545	-7.7345
0.0000	-0.9052	1.216	1.216	-7.706	-7.7442
0.0000	-0.8919	1.6174	1.6174	-8.116	-8.2556
0.0000	-0.8774	2.4732	2.4732	-8.2556	-8.3652
0.0000	-0.8626	3.0249	3.0249	-8.485	-8.6435
0.0000	-0.8461	3.6349	3.6349	-8.6435	-8.8435
0.0000	-0.8295	4.2697	4.2697	-8.8435	-9.0435
0.0000	-0.8129	4.8455	4.8455	-9.0435	-9.2435
0.0000	-0.7952	5.4174	5.4174	-9.2435	-9.4435
0.0000	-0.7774	6.0541	6.0541	-9.4435	-9.6435
0.0000	-0.7594	6.6679	6.6679	-9.6435	-9.8435
0.0000	-0.7414	7.2637	7.2637	-9.8435	-10.0435
0.0000	-0.7234	7.8375	7.8375	-10.0435	-10.2435
0.0000	-0.7045	8.4813	8.4813	-10.2435	-10.4435
0.0000	-0.6861	9.071	9.071	-10.4435	-10.6435
0.0000	-0.6671	9.6505	9.6505	-10.6435	-10.8435
0.0000	-0.6479	10.2397	10.2397	-10.8435	-11.0435
0.0000	-0.6286	10.8046	10.8046	-11.0435	-11.2435
0.0000	-0.6093	11.3596	11.3596	-11.2435	-11.4435
0.0000	-0.5899	11.9144	11.9144	-11.4435	-11.6435
0.0000	-0.5696	12.4694	12.4694	-11.6435	-11.8435
0.0000	-0.5493	13.0239	13.0239	-11.8435	-12.0435
0.0000	-0.5289	13.5779	13.5779	-12.0435	-12.2435
0.0000	-0.5086	14.1312	14.1312	-12.2435	-12.4435
0.0000	-0.4882	14.6842	14.6842	-12.4435	-12.6435
0.0000	-0.4678	15.2372	15.2372	-12.6435	-12.8435
0.0000	-0.4474	15.7901	15.7901	-12.8435	-13.0435
0.0000	-0.4270	16.3431	16.3431	-13.0435	-13.2435
0.0000	-0.4066	16.8961	16.8961	-13.2435	-13.4435
0.0000	-0.3862	17.4491	17.4491	-13.4435	-13.6435
0.0000	-0.3658	18.0021	18.0021	-13.6435	-13.8435
0.0000	-0.3454	18.5551	18.5551	-13.8435	-14.0435
0.0000	-0.3250	19.1081	19.1081	-14.0435	-14.2435
0.0000	-0.3046	19.6611	19.6611	-14.2435	-14.4435
0.0000	-0.2842	20.2141	20.2141	-14.4435	-14.6435
0.0000	-0.2638	20.7671	20.7671	-14.6435	-14.8435
0.0000	-0.2434	21.3201	21.3201	-14.8435	-15.0435
0.0000	-0.2230	21.8731	21.8731	-15.0435	-15.2435
0.0000	-0.2026	22.4261	22.4261	-15.2435	-15.4435
0.0000	-0.1822	22.9791	22.9791	-15.4435	-15.6435
0.0000	-0.1618	23.5321	23.5321	-15.6435	-15.8435
0.0000	-0.1414	24.0851	24.0851	-15.8435	-16.0435
0.0000	-0.1210	24.6381	24.6381	-16.0435	-16.2435
0.0000	-0.0996	25.1911	25.1911	-16.2435	-16.4435
0.0000	-0.0792	25.7441	25.7441	-16.4435	-16.6435
0.0000	-0.0588	26.2971	26.2971	-16.6435	-16.8435
0.0000	-0.0384	26.8501	26.8501	-16.8435	-17.0435
0.0000	-0.0180	27.4031	27.4031	-17.0435	-17.2435
0.0000	0.0000	27.9561	27.9561	-17.2435	-17.4435

ORIGINAL PAGE IS  
OF POOR QUALITY



Y • -71.7062 Y/16/72 • -.3049 CHORD • 26.6552

CHORD, AT SLICE POINTS, EACH FORTY 13' REAR  
CROSSING X/C LOCATIONS FROM FRONT TO REAR

.6117 • .6072 • 1.621 • .3012 • .3030 • .3194 • .3710 • .6206 • .4061 • .5117 • .5972 • .7528 • .7083 • .7639 • .8194 • .8750 • .9306 • .9861

LEGS ELEVATION

LEG	Z/C	DELTA X	DELTA Z
1	-.6217	• .6609	-.7121
2	-.6519	• .6616	-.7462
3	-.6170	1.3323	-.7709
4	-.6094	1.3341	-.8023
5	-.6012	2.8652	-.8314
6	-.5915	3.3319	-.8673
7	-.5842	3.7663	-.8954
8	-.5742	4.6547	-.9264
9	-.5624	5.2310	-.9542
10	-.5521	5.8574	-.9771
11	-.5426	6.6653	-.9774
12	-.5320	7.3202	-.8754
13	-.5227	7.9566	-.7711
14	-.5124	8.6146	-.8648
15	-.5021	9.2922	-.8561
16	-.4917	9.8521	-.8463
17	-.4814	10.6671	-.8243
18	-.4709	11.3765	-.8066
19	-.4605	11.9863	-.8057
20	-.4501	12.6012	-.7463
21	-.4400	13.2276	-.7667
22	-.4301	13.8490	-.7496
23	-.4205	14.4712	-.7270
24	-.4106	15.0930	-.7049
25	-.4006	15.6931	-.6903
26	-.3906	16.6535	-.6542
27	-.3807	17.3255	-.6266
28	-.3708	17.6923	-.5975
29	-.3609	18.4117	-.5664
30	-.3510	18.3263	-.5345

ORIGINAL PAGE IS  
OF POOR QUALITY



Y = -17.0377    Y1 = 17.07 = .2494    C1143 = 29.0731

SLCPT1.01/X.41 STRE POINTS FROM FRONT TO REAR  
C1143 = 29.0731 X/Y/C LOCATIONS FROM FRONT TO REAR  
X1 = 17.07 Y1 = 17.07 Z1 = .2494  
X2 = 17.07 Y2 = 17.07 Z2 = .2494  
X3 = 17.07 Y3 = 17.07 Z3 = .2494  
X4 = 17.07 Y4 = 17.07 Z4 = .2494  
X5 = 17.07 Y5 = 17.07 Z5 = .2494  
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X98 = 17.07 Y98 = 17.07 Z98 = .2494  
X99 = 17.07 Y99 = 17.07 Z99 = .2494  
X100 = 17.07 Y100 = 17.07 Z100 = .2494

LOCAL ELEVATION

Y/C	Z/C	DELTA X	DELTA Y	DELTA Z
0.0000	-0.0078	0.0000	-0.0000	-0.5042
-0.0250	-0.0259	-0.7270	-0.4402	-0.4402
-0.0500	-0.0500	1.4539	-0.6719	-0.6719
-0.0750	-0.0759	2.1629	-0.8991	-0.8991
-0.1000	-0.1021	2.4678	-0.9169	-0.9169
-0.1250	-0.1271	3.5340	-0.9225	-0.9225
-0.1500	-0.1514	4.2711	-0.9271	-0.9271
-0.1750	-0.1724	5.0117	-0.9486	-0.9486
-0.2000	-0.2027	5.5129	-0.9514	-0.9514
-0.2250	-0.2227	6.5420	-0.9522	-0.9522
-0.2500	-0.2527	7.2029	-0.9496	-0.9496
-0.2750	-0.2729	7.9065	-0.9451	-0.9451
-0.3000	-0.3029	8.7226	-0.9382	-0.9382
-0.3250	-0.3229	9.5193	-0.9242	-0.9242
-0.3500	-0.3529	10.4173	-0.9182	-0.9182
-0.3750	-0.3729	10.9643	-0.9054	-0.9054
-0.4000	-0.4029	11.6113	-0.8904	-0.8904
-0.4250	-0.4229	12.3542	-0.8744	-0.8744
-0.4500	-0.4529	13.0941	-0.8564	-0.8564
-0.4750	-0.4729	13.6121	-0.8369	-0.8369
-0.5000	-0.5029	14.5191	-0.8157	-0.8157
-0.5250	-0.5229	15.2669	-0.7931	-0.7931
-0.5500	-0.5529	15.8630	-0.7689	-0.7689
-0.5750	-0.5729	16.7199	-0.7433	-0.7433
-0.6000	-0.6029	17.4469	-0.7163	-0.7163
-0.6250	-0.6229	18.1739	-0.6876	-0.6876
-0.6500	-0.6529	18.9553	-0.6578	-0.6578
-0.6750	-0.6729	19.6277	-0.6263	-0.6263
-0.7000	-0.7029	20.3047	-0.5955	-0.5955
-0.7250	-0.7229	21.2116	-0.5547	-0.5547

ORIGINAL PAGE IS  
OF POOR QUALITY

21.80	-0.5225
21.80	21.8086
22.67	-0.6347
22.67	22.2355
23.52	-0.4451
23.52	23.2625
23.52	-0.4634
23.52	23.9094
24.39	-0.3502
24.39	24.7164
25.24	-0.3125
25.24	25.4423
26.09	-0.2949
26.09	26.1703
26.95	-0.2127
26.95	26.9675
27.80	-0.1719
27.80	27.8743
28.65	-0.0632
28.65	28.3512
29.50	0.0000
29.50	29.6731

ECONOMIC GROWTH AND INSTITUTE ECONOMIC GROWTH 2612

LETTER FROM THE EDITOR

246 DELTA Z DELTA X 7.00

ORIGINAL PAGE IS  
OF POOR QUALITY

23.5257	-5524
24.6163	-5114
25.2003	-4637
25.633	-4240
26.7795	-3768
27.5634	-3271
28.3706	-2759
29.1314	-2256
29.9115	-1753
30.6916	-1250
30.7115	-0822
31.5610	5.0266
31.5600	6.0000



-0.0174	25.4427
-0.5161	26.2910
-0.5459	27.1361
-0.5459	27.9874
-0.5459	28.8552
-0.5459	29.7034
-0.5459	30.5512
-0.5459	31.3795
-0.5459	32.2277
-0.5459	33.0758
-0.5459	33.9237
1.0000	0.0000

ORIGINAL PAGE IS  
OF POOR QUALITY

Y\* = -5.3423 Y\*9/2 = -.0832 CHORD = 36.3468

SLOPES AT SLOPE POINTS, FROM FRONT TO REAR

0.1177 - 0.003 - 0.114 - 0.114 - 0.253 - 0.114 - 0.310 - 0.114 - 0.424 - 0.465 - 0.415 - 0.413 - 0.542 - 0.574 - 0.612 - 0.662 - 0.747 - 1.011  
 0.3875 SLOPES AT LOCAL CHORDS FROM FRONT TO REAR  
 0.1177 - 0.072 - 0.221 - 0.263 - 0.3194 - 0.3750 - 0.4361 - 0.5117 - 0.5772 - 0.6528 - 0.7023 - 0.7639 - 0.8194 - 0.8750 - 0.9306 - 0.9661

LOCAL ELEVATION

X/C	Z/C	Y/C	DELTA X	DELTA Z
-0.200	-0.67	-0.000	-1.4418	
-0.120	-0.91	-0.037	-1.4536	
-0.060	-0.96	-1.3172	-1.4745	
-0.030	-0.903	2.7250	-1.4958	
-0.010	-0.871	3.6547	-1.4862	
-0.005	-0.869	6.5453	-1.4658	
-0.002	-0.8697	5.4736	-1.4761	
-0.001	-0.8701	6.1607	-1.4650	
-0.000	-0.8700	7.7269	-1.4525	
-0.005	-0.8695	2.1712	-1.4349	
-0.010	-0.8700	0.0067	-1.4149	
-0.015	-0.8703	9.3654	-1.3916	
-0.020	-0.8706	10.9660	-1.3665	
-0.025	-0.8708	11.4127	-1.3373	
-0.030	-0.8708	12.7214	-1.3147	
-0.035	-0.8702	13.8200	-1.2772	
-0.040	-0.8703	14.6337	-1.2465	
-0.045	-0.8704	15.4174	-1.2123	
-0.050	-0.8700	16.3560	-1.1765	
-0.055	-0.8699	17.2647	-1.1393	
-0.060	-0.8697	18.1794	-1.1007	
-0.065	-0.8697	19.0520	-1.0624	
-0.070	-0.8692	19.9007	-1.0197	
-0.075	-0.8686	20.8016	-0.9774	
-0.080	-0.8679	21.3091	-0.9338	
-0.085	-0.8670	22.7157	-0.8890	
-0.090	-0.8669	23.6254	-0.8451	
-0.095	-0.8661	24.5341	-0.7961	
-0.100	-0.8656	25.4227	-0.7571	

1.7255	-0.072	27.9231	-6475
1.7256	-0.073	28.3607	-5554
1.7258	-0.074	28.0774	-5426
1.7260	-0.075	27.7841	-4667
1.7262	-0.076	27.4907	-4275
1.7264	-0.077	27.1974	-3803
1.7266	-0.078	26.8941	-3226
1.7268	-0.079	26.5907	-2696
1.7270	-0.080	26.2964	-2165
1.7272	-0.081	25.9921	-1634
1.7274	-0.082	25.6978	-1103
1.7276	-0.083	25.3935	-572
1.7278	-0.084	25.0902	405
1.7280	-0.085	24.7869	836
1.7282	-0.086	24.4826	1265
1.7284	-0.087	24.1783	1694
1.7286	-0.088	23.8740	2123
1.7288	-0.089	23.5697	2552
1.7290	-0.090	23.2654	2980

$$Y = -1.05747 \cdot Y_{1/2} + 0.3278 \quad \text{CHDR = } 3.9 \cdot 7722$$

SOCIETY, ECONOMY AND POLITICS IN PEARL

LOCAL ELEVATION

DELTIA X	DELTIA Z
-2.1743	-2.1743
-2.1706	-2.1706
-2.1654	-2.1654
-2.1699	-2.1699
-2.1396	-2.1396
-2.1125	-2.1125
-2.0912	-2.0912
-2.0476	-2.0476
-2.0101	-2.0101
-1.9592	-1.9592
-1.9256	-1.9256
-1.8796	-1.8796
-1.8216	-1.8216
-1.7612	-1.7612
-1.7037	-1.7037
-1.6459	-1.6459
-1.5877	-1.5877
-1.5295	-1.5295
-1.4713	-1.4713
-1.4131	-1.4131
-1.3549	-1.3549
-1.2967	-1.2967
-1.2385	-1.2385
-1.1793	-1.1793
-1.1211	-1.1211
-1.0629	-1.0629
-1.0047	-1.0047
-0.9465	-0.9465
-0.8883	-0.8883
-0.8299	-0.8299
-0.7717	-0.7717
-0.7135	-0.7135
-0.6553	-0.6553
-0.5971	-0.5971
-0.5389	-0.5389
-0.4807	-0.4807
-0.4225	-0.4225
-0.3643	-0.3643
-0.3061	-0.3061
-0.2479	-0.2479
-0.1897	-0.1897
-0.1315	-0.1315
-0.0733	-0.0733
-0.0151	-0.0151
0.0433	0.0433
0.0915	0.0915
0.1397	0.1397
0.1879	0.1879
0.2361	0.2361
0.2843	0.2843
0.3325	0.3325
0.3807	0.3807
0.4289	0.4289
0.4771	0.4771
0.5253	0.5253
0.5735	0.5735
0.6217	0.6217
0.6699	0.6699
0.7181	0.7181
0.7663	0.7663
0.8145	0.8145
0.8627	0.8627
0.9109	0.9109
0.9591	0.9591
1.0073	1.0073
1.0555	1.0555
1.1037	1.1037
1.1519	1.1519
1.1991	1.1991
1.2473	1.2473
1.2955	1.2955
1.3437	1.3437
1.3919	1.3919
1.4391	1.4391
1.4873	1.4873
1.5355	1.5355
1.5837	1.5837
1.6319	1.6319
1.6791	1.6791
1.7273	1.7273
1.7755	1.7755
1.8237	1.8237
1.8719	1.8719
1.9191	1.9191
1.9673	1.9673
2.0155	2.0155
2.0637	2.0637
2.1119	2.1119
2.1591	2.1591
2.2073	2.2073
2.2555	2.2555
2.3037	2.3037
2.3519	2.3519
2.3991	2.3991
2.4473	2.4473
2.4955	2.4955
2.5437	2.5437
2.5919	2.5919
2.6391	2.6391
2.6873	2.6873
2.7355	2.7355
2.7837	2.7837
2.8319	2.8319
2.8791	2.8791
2.9273	2.9273
2.9755	2.9755
3.0237	3.0237
3.0719	3.0719
3.1191	3.1191
3.1673	3.1673
3.2155	3.2155
3.2637	3.2637
3.3119	3.3119
3.3591	3.3591
3.4073	3.4073
3.4555	3.4555
3.5037	3.5037
3.5519	3.5519
3.5991	3.5991
3.6473	3.6473
3.6955	3.6955
3.7437	3.7437
3.7919	3.7919
3.8391	3.8391
3.8873	3.8873
3.9355	3.9355
3.9837	3.9837
4.0319	4.0319
4.0791	4.0791
4.1273	4.1273
4.1755	4.1755
4.2237	4.2237
4.2719	4.2719
4.3191	4.3191
4.3673	4.3673
4.4155	4.4155
4.4637	4.4637
4.5119	4.5119
4.5591	4.5591
4.6073	4.6073
4.6555	4.6555
4.7037	4.7037
4.7519	4.7519
4.7991	4.7991
4.8473	4.8473
4.8955	4.8955
4.9437	4.9437
4.9919	4.9919
5.0391	5.0391
5.0873	5.0873
5.1355	5.1355
5.1837	5.1837
5.2319	5.2319
5.2791	5.2791
5.3273	5.3273
5.3755	5.3755
5.4237	5.4237
5.4719	5.4719
5.5191	5.5191
5.5673	5.5673
5.6155	5.6155
5.6637	5.6637
5.7119	5.7119
5.7591	5.7591
5.8073	5.8073
5.8555	5.8555
5.9037	5.9037
5.9519	5.9519
6.0001	6.0001

ORIGINAL PAGE IS  
OF POOR QUALITY

-1.6126	23.0724	-• 7616
-1.6179	36.5454	-• 6678
-1.6182	31.5377	-• 6372
-1.6184	31.5870	-• 5265
-1.6186	32.4346	-• 6863
-1.6188	33.8256	-• 4171
-1.6191	36.3649	-• 3449
-1.6193	35.3442	-• 2712
-1.6195	36.4732	-• 1869
-1.6197	37.4421	-• 0330
-1.6199	36.7722	6.0000

1.	1.	20.9696	2353.6296
8.	0.	0.	0.
-30.8332	-69.34	77.5	1.
-23.7143	-69.34	77.5	1.
-28.3111	-69.8777	77.5	1.
-33.5837	-71.4907	0.	1.
-35.3403	-71.4907	77.5	1.
-32.7053	-69.8777	77.5	1.
-31.8271	-69.34	6.	1.
-14.0067	-27.736	6.	1.
-9.1529	-0.		
100. 18.	20. 0.8	0.5	
	1.0		

GEOOMETRY DATA

ROOT CHORD HEIGHT = 0.000000 REFERENCE PLANFORM HAS 8 CURVES  
 VARIABLE SWEEP PIVOT POSITION X(S) = 0.000000 Y(S) = 0.000000

BREAK POINTS FOR THE REFERENCE PLANFORM

POINT	X REF	Y REF	SWEEP ANGLE	DIHEDRAL ANGLE	MOVE CODE
1	30.83320	0.00000	38.19097	6.00000	1
2	-23.71430	-69.34000	83.32828	77.50000	1
3	-28.31110	-69.87770	72.99002	77.50000	1
4	-13.5R370	-71.49070	90.00000	0.00000	1
5	-35.34030	-71.49070	58.52736	77.50000	1
6	-32.70530	-69.87770	58.52190	77.50000	1
7	-31.82710	-69.34000	23.18709	6.00000	1
8	-14.00670	-27.73600	9.92625	6.00000	1
9	-9.15290	0.00000			

CONFIGURATION NO. 100.

CURVE 1 IS SWEEP 38.19097 DEGREES ON PLANFORM 1

BREAK POINTS FOR THIS CONFIGURATION

POINT	X	Y	Z	SWEEP ANGLE	DIHEDRAL ANGLE	MOVE CODE
1	30.83320	0.00000	0.00000	38.19097	6.00000	1
2	-23.71430	-69.34000	-7.28793	83.32828	77.50000	1
3	-28.31110	-69.87770	-9.71334	72.99002	77.50000	1
4	-33.58370	-71.49070	-16.98911	90.00000	0.00000	1
5	-35.34030	-71.49070	-16.98911	58.52736	77.50000	1
6	-32.70530	-69.87770	-9.71334	58.52190	77.50000	1
7	-31.62710	-69.34000	-7.28793	23.18709	6.00000	1
8	-14.00670	-27.73660	-2.91517	9.92625	6.00000	1
9	-9.15290	0.00000	0.00000			

378 HORSESHOE VORTICES USED ON THE LEFT HALF OF THE CONFIGURATION

PLANFORM	TOTAL	SPANWISE
	1	378

18. HORSESHOE VORTICES IN EACH CHORDWISE ROW

MINIMUM FIELD LENGTH = 63000

ORIGINAL PAGE IS  
OF POOR QUALITY

X C/4	X 3C/4	Y	Z	S	C/4 SWEEP ANGLE	DIHEDRAL ANGLE	GAMMA/U AT CLDESA = .5000
-32.20892	-32.27729	-71.05967	-15.04485	1.99147	72.87795	77.50000	.02889
-32.34567	-32.41404	-71.05967	-15.04485	1.99147	72.41497	77.50000	.02889
-32.48241	-32.55079	-71.05967	-15.04485	1.99147	71.92712	77.50000	.02889
-32.61916	-32.68753	-71.05967	-15.04485	1.99147	71.41240	77.50000	.02889
-32.75591	-32.82428	-71.05967	-15.04485	1.99147	70.86864	77.50000	.02889
-32.89265	-32.96102	-71.05967	-15.04485	1.99147	70.29340	77.50000	.02889
-33.02940	-33.09777	-71.05967	-15.04485	1.99147	69.68400	77.50000	.02889
-33.16614	-33.23452	-71.05967	-15.04485	1.99147	69.03746	77.50000	.02889
-33.30289	-33.37126	-71.05967	-15.04485	1.99147	68.35044	77.50000	.02889
-33.43964	-33.50801	-71.05967	-15.04485	1.99147	67.61925	77.50000	.02889
-33.57638	-33.64476	-71.05967	-15.04485	1.99147	66.83975	77.50000	.02889
-33.71313	-33.78150	-71.05967	-15.04485	1.99147	66.00730	77.50000	.02889
-33.84987	-33.91825	-71.05967	-15.04485	1.99147	65.11671	77.50000	.02889
-33.98662	-34.05499	-71.05967	-15.04485	1.99147	64.16215	77.50000	.02889
-34.12337	-34.19174	-71.05967	-15.04485	1.99147	63.13706	77.50000	.02889
-34.26011	-34.32849	-71.05967	-15.04485	1.99147	62.03406	77.50000	.02889
-34.39686	-34.46523	-71.05967	-15.04485	1.99147	60.84483	77.50000	.02889
-34.53361	-34.60198	-71.05967	-15.04485	1.99147	59.56000	77.50000	.02889
-29.59094	-29.69594	-70.25317	-11.40696	1.73475	72.87795	77.50000	.02889
-29.80095	-29.90596	-70.25317	-11.40696	1.73475	72.41497	77.50000	.02889
-30.01096	-30.11597	-70.25317	-11.40696	1.73475	71.92712	77.50000	.02889
-30.22098	-30.32598	-70.25317	-11.40696	1.73475	71.41240	77.50000	.02889
-30.43099	-30.53600	-70.25317	-11.40696	1.73475	70.86864	77.50000	.02889
-30.64100	-30.74601	-70.25317	-11.40696	1.73475	70.29340	77.50000	.02889
-30.85101	-30.95602	-70.25317	-11.40696	1.73475	69.68400	77.50000	.02889
-31.06103	-31.16603	-70.25317	-11.40696	1.73475	69.03746	77.50000	.02889
-31.27104	-31.37605	-70.25317	-11.40696	1.73475	68.35044	77.50000	.02889
-31.46105	-31.58606	-70.25317	-11.40696	1.73475	67.61925	77.50000	.02889
-31.69107	-31.79607	-70.25317	-11.40696	1.73475	66.83975	77.50000	.02889
-31.90108	-32.00608	-70.25317	-11.40696	1.73475	66.00730	77.50000	.02889
-32.11109	-32.21610	-70.25317	-11.40696	1.73475	65.11671	77.50000	.02889
-32.32110	-32.42611	-70.25317	-11.40696	1.73475	64.16215	77.50000	.02889
-32.53112	-32.63612	-70.25317	-11.40696	1.73475	63.13706	77.50000	.02889
-32.74113	-32.84614	-70.25317	-11.40696	1.73475	62.03406	77.50000	.02889
-32.95114	-33.05615	-70.25317	-11.40696	1.73475	60.84483	77.50000	.02889
-33.16116	-33.26616	-70.25317	-11.40696	1.73475	59.56000	77.50000	.02889
-26.09955	-26.27326	-69.60885	-8.50063	1.24215	83.25316	77.50000	.05629
-26.44697	-26.62068	-69.60885	-8.50063	1.24215	82.93507	77.50000	.05629
-26.79439	-26.96810	-69.60885	-8.50063	1.24215	82.58568	77.50000	.05629
-27.14180	-27.31151	-69.60885	-8.50063	1.24215	82.20016	77.50000	.05629
-27.48922	-27.66293	-69.60885	-8.50063	1.24215	81.77264	77.50000	.05629
-27.83664	-28.01035	-69.60885	-8.50063	1.24215	81.29591	77.50000	.05629
-28.11405	-28.35776	-69.60885	-8.50063	1.24215	80.76105	77.50000	.05629

10.8037 16.6191  
ATLANTIC ROCK

-28.53147	-28.70518	-69.60885	-8.50063	1.24215	80.15684	77.50000	0.5629
-28.87889	-29.05260	-69.60885	-8.50063	1.24215	79.46902	77.50000	0.5629
-29.22630	-29.45001	-69.60885	-8.50063	1.24215	78.67921	77.50000	0.5629
-29.57372	-29.74743	-69.60885	-8.50063	1.24215	77.76326	77.50000	0.5629
-29.92114	-30.09485	-69.60885	-8.50063	1.24215	76.68896	77.50000	0.5629
-30.26855	-30.44226	-69.60885	-8.50063	1.24215	75.41234	77.50000	0.5629
-30.61597	-30.78968	-69.60885	-8.50063	1.24215	73.87202	77.50000	0.5629
-30.96339	-31.13710	-69.60885	-8.50063	1.24215	71.98001	77.50000	0.5629
-31.31080	-31.48451	-69.60885	-8.50063	1.24215	69.60631	77.50000	0.5629
-31.65822	-31.83193	-69.60885	-8.50063	1.24215	66.55250	77.50000	0.5629
-32.00564	-32.17935	-69.60885	-8.50063	1.24215	62.50521	77.50000	0.5629
-32.27580	-32.52386	-67.35944	-7.07976	1.99147	38.01439	6.00000	0.9776
-32.76893	-33.01400	-67.35944	-7.07976	1.99147	37.29953	6.00000	0.9776
-23.25907	-23.50414	-67.35944	-7.07976	1.99147	36.57081	6.00000	0.9776
-23.74921	-23.99428	-67.35944	-7.07976	1.99147	35.82806	6.00000	0.9776
-24.23935	-24.48442	-67.35944	-7.07976	1.99147	35.07118	6.00000	0.9776
-24.72949	-24.97456	-67.35944	-7.07976	1.99147	34.29998	6.00000	0.9776
-25.21963	-25.46670	-67.35944	-7.07976	1.99147	33.51435	6.00000	0.9776
-25.70977	-25.95484	-67.35944	-7.07976	1.99147	32.71419	6.00000	0.9776
-26.19991	-26.44498	-67.35944	-7.07976	1.99147	31.89942	6.00000	0.9776
-26.69005	-26.93511	-67.35944	-7.07976	1.99147	31.06996	6.00000	0.9776
-27.18018	-27.42525	-67.35944	-7.07976	1.99147	30.22577	6.00000	0.9776
-27.67032	-27.91539	-67.35944	-7.07976	1.99147	29.36684	6.00000	0.9776
-28.16046	-28.40553	-67.35944	-7.07976	1.99147	28.49317	6.00000	0.9776
-28.65060	-28.89567	-67.35944	-7.07976	1.99147	27.60480	6.00000	0.9776
-29.14074	-29.35281	-67.35944	-7.07976	1.99147	26.70178	6.00000	0.9776
-29.63088	-29.87595	-67.35944	-7.07976	1.99147	25.78422	6.00000	0.9776
-30.12102	-30.36609	-67.35944	-7.07976	1.99147	24.85224	6.00000	0.9776
-30.61116	-30.85623	-67.35944	-7.07976	1.99147	23.90600	6.00000	0.9776
-19.18243	-19.46693	-63.39833	-6.66343	1.99147	38.01439	6.00000	0.13985
-19.75143	-20.03592	-63.39833	-6.66343	1.99147	37.29953	6.00000	0.13985
-20.32042	-20.60492	-63.39833	-6.66343	1.99147	36.57081	6.00000	0.13985
-20.88941	-21.17739	-63.39833	-6.66343	1.99147	35.82808	6.00000	0.13985
-21.45841	-21.74291	-63.39833	-6.66343	1.99147	35.07118	6.00000	0.13985
-22.02740	-22.31190	-63.39833	-6.66343	1.99147	34.29998	6.00000	0.13985
-22.59640	-22.68089	-63.39833	-6.66343	1.99147	33.51435	6.00000	0.13985
-23.16539	-23.44989	-63.39833	-6.66343	1.99147	32.71419	6.00000	0.13985
-23.73439	-24.01888	-63.39833	-6.66343	1.99147	31.89942	6.00000	0.13985
-24.30338	-24.58788	-63.39833	-6.66343	1.99147	31.06996	6.00000	0.13985
-24.87237	-25.15687	-63.39833	-6.66343	1.99147	30.22577	6.00000	0.13985
-25.44137	-25.72587	-63.39833	-6.66343	1.99147	29.36684	6.00000	0.13985
-26.01036	-26.29486	-63.39833	-6.66343	1.99147	28.49317	6.00000	0.13985
-26.57936	-26.86386	-63.39833	-6.66343	1.99147	27.60480	6.00000	0.13985
-27.14835	-27.43285	-63.39833	-6.66343	1.99147	26.70178	6.00000	0.13985
-27.71735	-28.00184	-63.39833	-6.66343	1.99147	25.78422	6.00000	0.13985
-28.28634	-28.57084	-63.39833	-6.66343	1.99147	24.85224	6.00000	0.13985
-28.85534	-29.13983	-63.39833	-6.66343	1.99147	23.90660	6.00000	0.13985
-16.08607	-16.40999	-59.43721	-6.24710	1.99147	38.01439	6.00000	0.16562
-16.73392	-17.05784	-59.43721	-6.24710	1.99147	37.29953	6.00000	0.16562

ORIGINAL PAGE IS  
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-17.38177	-17.70569	-59.43721	-6.24710	1.99147	36.57001	6.00000
-18.62962	-18.35354	-59.43721	-6.24710	1.99147	35.82806	6.00000
-18.67747	-19.00139	-59.43721	-6.24710	1.99147	35.07118	6.00000
-19.32532	-19.64924	-59.43721	-6.24710	1.99147	34.29998	6.00000
-19.67317	-20.29709	-59.43721	-6.24710	1.99147	33.51435	6.00000
-20.62102	-20.94494	-59.43721	-6.24710	1.99147	32.71419	6.00000
-21.26887	-21.59279	-59.43721	-6.24710	1.99147	31.89942	6.00000
-21.91672	-22.24064	-59.43721	-6.24710	1.99147	31.06996	6.00000
-22.56457	-22.88849	-59.43721	-6.24710	1.99147	30.22577	6.00000
-23.21242	-23.53634	-59.43721	-6.24710	1.99147	29.36684	6.00000
-23.86027	-24.18419	-59.43721	-6.24710	1.99147	28.49317	6.00000
-24.50811	-24.83204	-59.43721	-6.24710	1.99147	27.60480	6.00000
-25.15596	-25.47989	-59.43721	-6.24710	1.99147	26.70178	6.00000
-25.80381	-26.12274	-59.43721	-6.24710	1.99147	25.78422	6.00000
-26.45166	-26.77559	-59.43721	-6.24710	1.99147	24.85224	6.00000
-27.09951	-27.42344	-59.43721	-6.24710	1.99147	23.90600	6.00000
-12.98970	-13.35305	-55.47610	-5.83077	1.99147	38.01439	6.00000
-13.71641	-14.07976	-55.47610	-5.83077	1.99147	37.29953	6.00000
-14.44311	-14.80647	-55.47610	-5.83077	1.99147	36.57081	6.00000
-15.16982	-15.53317	-55.47610	-5.83077	1.99147	35.82808	6.00000
-15.46552	-16.25998	-55.47610	-5.83077	1.99147	35.07118	6.00000
-16.62323	-16.98658	-55.47610	-5.83077	1.99147	34.29998	6.00000
-17.34993	-17.71329	-55.47610	-5.83077	1.99147	33.51435	6.00000
-18.07664	-18.43999	-55.47610	-5.83077	1.99147	32.71419	6.00000
-18.80335	-19.16670	-55.47610	-5.83077	1.99147	31.89942	6.00000
-19.53005	-19.89340	-55.47610	-5.83077	1.99147	31.06996	6.00000
-20.25676	-20.62011	-55.47610	-5.83077	1.99147	30.22577	6.00000
-20.98346	-21.34681	-55.47610	-5.83077	1.99147	29.36684	6.00000
-21.71017	-22.07352	-55.47610	-5.83077	1.99147	28.49317	6.00000
-22.43687	-22.80022	-55.47610	-5.83077	1.99147	27.60480	6.00000
-23.16358	-23.52693	-55.47610	-5.83077	1.99147	26.70178	6.00000
-23.86028	-24.25364	-55.47610	-5.83077	1.99147	25.78422	6.00000
-24.61699	-24.98034	-55.47610	-5.83077	1.99147	24.85224	6.00000
-25.34369	-25.70705	-55.47610	-5.83077	1.99147	23.90600	6.00000
-9.99334	-10.29612	-51.51499	-5.41444	1.99147	38.01439	6.00000
-10.69890	-11.10168	-51.51499	-5.41444	1.99147	37.29953	6.00000
-11.50446	-11.90724	-51.51499	-5.41444	1.99147	36.57081	6.00000
-12.31002	-12.71280	-51.51499	-5.41444	1.99147	35.82808	6.00000
-13.11558	-13.51836	-51.51499	-5.41444	1.99147	35.07118	6.00000
-13.92114	-14.32392	-51.51499	-5.41444	1.99147	34.29998	6.00000
-14.72670	-15.12948	-51.51499	-5.41444	1.99147	33.51435	6.00000
-15.53226	-15.93504	-51.51499	-5.41444	1.99147	32.71419	6.00000
-16.33782	-16.74061	-51.51499	-5.41444	1.99147	31.89942	6.00000
-17.14339	-17.54617	-51.51499	-5.41444	1.99147	31.06996	6.00000
-17.94895	-18.35173	-51.51499	-5.41444	1.99147	30.22577	6.00000
-18.75451	-19.15729	-51.51499	-5.41444	1.99147	29.36684	6.00000
-19.56007	-20.76941	-51.51499	-5.41444	1.99147	28.49317	6.00000
-20.36563	-21.57397	-51.51499	-5.41444	1.99147	27.60480	6.00000
-21.17119					26.70178	6.00000

-21.97675	-22.37953	-51.51499	-5.41444	1.99147	25.78422	6.00000	*20387
-22.78231	-23.18509	-51.51499	-5.41444	1.99147	24.85224	6.00000	*20387
-23.58787	-23.99065	-51.51499	-5.41444	1.99147	23.90600	6.00000	*20387
-6.79697	-7.23918	-47.55387	-4.99811	1.99147	38.01439	6.00000	*21880
-7.68139	-8.12360	-47.55387	-4.99811	1.99147	37.29953	6.00000	*21880
-8.56581	-9.00801	-47.55387	-4.99811	1.99147	36.57081	6.00000	*21880
-9.45022	-9.89243	-47.55387	-4.99811	1.99147	35.82808	6.00000	*21880
-10.33464	-10.77685	-47.55387	-4.99811	1.99147	35.07118	6.00000	*21880
-11.21905	-11.66126	-47.55387	-4.99811	1.99147	34.29998	6.00000	*21880
-12.10347	-12.54568	-47.55387	-4.99811	1.99147	33.51435	6.00000	*21880
-12.98789	-13.43010	-47.55387	-4.99811	1.99147	32.71419	6.00000	*21880
-13.87230	-14.31451	-47.55387	-4.99811	1.99147	31.89942	6.00000	*21880
-14.75672	-15.19893	-47.55387	-4.99811	1.99147	31.06996	6.00000	*21880
-15.64114	-16.08335	-47.55387	-4.99811	1.99147	30.22577	6.00000	*21880
-16.52555	-16.96776	-47.55387	-4.99811	1.99147	29.36684	6.00000	*21880
-17.40997	-17.85219	-47.55387	-4.99811	1.99147	28.49317	6.00000	*21880
-18.29439	-18.73659	-47.55387	-4.99811	1.99147	27.60480	6.00000	*21880
-19.17880	-19.62101	-47.55387	-4.99811	1.99147	26.70178	6.00000	*21880
-20.06322	-20.50543	-47.55387	-4.99811	1.99147	25.78422	6.00000	*21880
-20.94764	-21.38984	-47.55387	-4.99811	1.99147	24.85224	6.00000	*21880
-21.83205	-22.27426	-47.55387	-4.99811	1.99147	23.90600	6.00000	*21880
-3.76061	-4.18224	-43.59276	-4.58178	1.99147	38.01439	6.00000	*23172
-4.66388	-5.14552	-43.59276	-4.58178	1.99147	37.29953	6.00000	*23172
-5.62715	-6.10879	-43.59276	-4.58178	1.99147	36.57081	6.00000	*23172
-6.59042	-7.07206	-43.59276	-4.58178	1.99147	35.82808	6.00000	*23172
-7.55370	-8.03533	-43.59276	-4.58178	1.99147	35.07118	6.00000	*23172
-8.51697	-8.99860	-43.59276	-4.58178	1.99147	34.29996	6.00000	*23172
-9.48024	-9.96188	-43.59276	-4.58178	1.99147	33.51435	6.00000	*23172
-10.44351	-10.92515	-43.59276	-4.58178	1.99147	32.71419	6.00000	*23172
-11.40678	-11.88842	-43.59276	-4.58178	1.99147	31.89942	6.00000	*23172
-12.37006	-12.85169	-43.59276	-4.58178	1.99147	31.06996	6.00000	*23172
-13.33333	-13.81496	-43.59276	-4.58178	1.99147	30.22577	6.00000	*23172
-14.29660	-14.77824	-43.59276	-4.58178	1.99147	29.36684	6.00000	*23172
-15.25987	-15.74151	-43.59276	-4.58178	1.99147	28.49317	6.00000	*23172
-16.22314	-16.70478	-43.59276	-4.58178	1.99147	27.60480	6.00000	*23172
-17.18642	-17.66805	-43.59276	-4.58178	1.99147	26.70178	6.00000	*23172
-18.14969	-18.63132	-43.59276	-4.58178	1.99147	25.78422	6.00000	*23172
-19.11296	-19.59460	-43.59276	-4.58178	1.99147	24.85224	6.00000	*23172
-20.07623	-20.55787	-43.59276	-4.58178	1.99147	23.90600	6.00000	*23172
-7.60424	-8.12531	-39.63164	-4.16545	1.99147	38.01439	6.00000	*24290
-1.64637	-2.16743	-39.63164	-4.16545	1.99147	37.29953	6.00000	*24290
-2.68850	-3.20956	-39.63164	-4.16545	1.99147	36.57081	6.00000	*24290
-3.73063	-4.25169	-39.63164	-4.16545	1.99147	35.82808	6.00000	*24290
-4.77275	-5.29382	-39.63164	-4.16545	1.99147	35.07118	6.00000	*24290
-5.81488	-6.33594	-39.63164	-4.16545	1.99147	34.29998	6.00000	*24290
-6.85701	-7.37807	-39.63164	-4.16545	1.99147	33.51435	6.00000	*24290
-7.89914	-8.42020	-39.63164	-4.16545	1.99147	32.71419	6.00000	*24290
-8.94126	-9.46233	-39.63164	-4.16545	1.99147	31.89942	6.00000	*24290
-9.98339	-10.50445	-39.63164	-4.16545	1.99147	31.06996	6.00000	*24290

ORIGINAL PAGE IS  
OF POOR QUALITY

• 24290	6.00000	30.222577
-11.54658	-39.63164	1.99147
-12.06765	-39.63164	-4.16545
-13.10977	-39.63164	-4.16545
-14.15190	-39.63164	-4.16545
-15.19403	-39.63164	-4.16545
-16.23616	-39.63164	-4.16545
-17.27828	-39.63164	-4.16545
-18.32041	-39.63164	-4.16545
2.49212	1.93163	-35.67053
1.37114	-8.1065	-35.67053
• 25016	-3.1034	-35.67053
-8.07083	-1.43132	-35.67053
1.99181	-2.5230	-35.67053
-3.11279	-3.67329	-35.67053
-4.23378	-6.79427	-35.67053
5.35476	-5.91525	-35.67053
6.47574	-7.03623	-35.67053
7.59673	-8.15722	-35.67053
8.71771	-9.27820	-35.67053
9.83869	-10.39918	-35.67053
1.0.65667	-11.52017	-35.67053
-1.1.2.08066	-12.64115	-35.67053
-1.3.20164	-13.76213	-35.67053
-1.4.32262	-14.83132	-35.67053
-1.5.44361	-16.00410	-35.67053
-1.6.56659	-17.12508	-35.67053
5.58849	4.98977	-31.70941
4.38865	3.78873	-31.70941
3.18881	2.58889	-31.70941
1.98897	1.38905	-31.70941
1.78913	-1.8921	-31.70941
-4.41071	-1.01063	-31.70941
-1.61055	-2.21046	-31.70941
-2.81038	-3.41030	-31.70941
-4.01022	-6.61014	-31.70941
-5.21006	-5.80998	-31.70941
-6.40990	-7.60982	-31.70941
-7.60974	-8.20966	-31.70941
-8.80958	-9.40950	-31.70941
-10.00941	-10.60933	-31.70941
-11.20925	-11.80917	-31.70941
-12.40909	-13.00901	-31.70941
-13.60909	-14.20885	-31.70941
-14.80958	-15.40869	-31.70941
-17.91577	7.24602	-28.73243
6.65646	6.02691	-28.73243
5.39736	4.76761	-28.73243
4.13826	3.50871	-28.73243
2.87916	2.24961	-28.73243

1.62005	.99050	-28.73243	-3.01990	1.00192	34.29998
.36095	-.26860	-28.73243	-3.01990	1.00192	33.51435
-.89815	-1.52770	-28.73243	-3.01990	1.00192	32.71419
-2.15725	-2.78681	-28.73243	-3.01990	1.00192	31.89942
-3.41636	-4.04591	-28.73243	-3.01990	1.00192	31.06996
-4.67546	-5.30501	-28.73243	-3.01990	1.00192	30.22577
-.53456	-6.56411	-28.73243	-3.01990	1.00192	29.36684
-7.19366	-7.82322	-28.73243	-3.01990	1.00192	28.49317
-8.45277	-9.08232	-28.73243	-3.01990	1.00192	27.60480
-9.71187	-10.34142	-28.73243	-3.01990	1.00192	26.70178
-10.97097	-11.60052	-29.73243	-3.01990	1.00192	25.78422
-12.23007	-12.85963	-28.73243	-3.01990	1.00192	24.85224
-13.48918	-14.11873	-28.73243	-3.01990	1.00192	23.90600
10.24568	9.16256	-25.75544	-2.70701	1.99147	37.88905
8.88944	8.21632	-25.75544	-2.70701	1.99147	36.65626
7.54320	6.87618	-25.75544	-2.70701	1.99147	35.38270
6.19696	5.52383	-25.75544	-2.70701	1.99147	34.06763
4.45071	4.17759	-25.75544	-2.70701	1.99147	32.71063
3.50447	2.83135	-25.75544	-2.70701	1.99147	31.31065
2.15823	1.48511	-25.75544	-2.70701	1.99147	29.86801
81199	.138887	-25.75544	-2.70701	1.99147	28.38241
-53425	-1.20737	-25.75544	-2.70701	1.99147	26.85399
-1.68049	-2.55361	-25.75544	-2.70701	1.99147	25.28316
-3.22673	-3.89985	-25.75544	-2.70701	1.99147	23.67056
-4.57297	-5.24609	-25.75544	-2.70701	1.99147	22.01719
-5.91922	-6.55234	-25.75544	-2.70701	1.99147	20.32431
-7.26546	-7.93858	-25.75544	-2.70701	1.99147	18.59357
-8.61170	-9.28482	-25.75544	-2.70701	1.99147	16.82693
-9.95794	-10.63106	-25.75544	-2.70701	1.99147	15.02672
-11.30418	-11.97730	-25.75544	-2.70701	1.99147	13.19564
-12.65042	-13.32354	-25.75544	-2.70701	1.99147	11.33671
13.31811	12.57768	-21.79433	-2.29068	1.99147	37.88905
11.63726	11.09684	-21.79433	-2.29068	1.99147	36.65626
10.35641	9.61599	-21.79433	-2.29068	1.99147	35.38270
8.87557	8.13515	-21.79433	-2.29068	1.99147	34.06763
7.39472	6.65430	-21.79433	-2.29068	1.99147	32.71043
5.91388	5.17345	-21.79433	-2.29068	1.99147	31.31065
4.43303	3.69261	-21.79433	-2.29068	1.99147	29.86801
2.65219	2.21176	-21.79433	-2.29068	1.99147	28.38241
1.47134	.73092	-21.79433	-2.29068	1.99147	26.85399
-0.0951	-7.4993	-21.79433	-2.29068	1.99147	25.28316
-1.49035	-2.23078	-21.79433	-2.29068	1.99147	23.67056
-2.97120	-3.71162	-21.79433	-2.29068	1.99147	22.01719
-4.45204	-5.19247	-21.79433	-2.29068	1.99147	20.32431
-5.93289	-6.67331	-21.79433	-2.29068	1.99147	18.59357
-7.41374	-8.15416	-21.79433	-2.29068	1.99147	16.82693
-8.69458	-9.63500	-21.79433	-2.29068	1.99147	15.02672
-10.37543	-11.1585	-21.79433	-2.29068	1.99147	13.19564
-11.85627	-12.59670	-21.79433	-2.29068	1.99147	11.33671

16.40053	15.59281	-17.83321	1.99147	6.00000	.28166
14.75508	13.97736	-17.63321	-1.87435	6.00000	.28166
13.16963	12.36191	-17.63321	-1.87435	6.00000	.28166
11.55418	10.74646	-17.63321	-1.87435	6.00000	.28166
9.93873	9.13101	-17.63321	-1.87435	6.00000	.28166
8.32328	7.51556	-17.63321	-1.87435	6.00000	.28166
6.70783	5.90011	-17.63321	-1.87435	6.00000	.28166
5.09238	4.25465	-17.63321	-1.87435	6.00000	.28166
3.47693	2.66920	-17.63321	-1.87435	6.00000	.28166
-4.60032	-5.40805	-17.63321	-1.87435	6.00000	.28166
1.86148	1.05375	-17.63321	-1.87435	6.00000	.28166
-6.21577	-7.02350	-17.63321	-1.87435	6.00000	.28166
2.4603	-5.26170	-17.63321	-1.87435	6.00000	.28166
-1.36942	-2.17715	-17.63321	-1.87435	6.00000	.28166
-2.98487	-3.79260	-17.63321	-1.87435	6.00000	.28166
19.49296	18.-60793	-17.63321	-1.87435	6.00000	.28166
17.73291	16.-85788	-13.-87210	-1.45802	1.99147	23.-67056
15.98285	15.-10782	-13.-87210	-1.45802	1.99147	15.-02672
-11.06212	-10.-25440	-13.-87210	-1.45802	1.99147	22.-01719
-11.86985	-11.-86985	-13.-87210	-1.45802	1.99147	28.-38241
13.-35777	13.-35777	-13.-87210	-1.45802	1.99147	20.-32431
12.-48274	11.-60771	-13.-87210	-1.45802	1.99147	26.-85399
10.-73269	9.-85766	-13.-87210	-1.45802	1.99147	18.-59357
8.98263	8.-10760	-13.-87210	-1.45802	1.99147	25.-28316
7.23258	6.-35755	-13.-87210	-1.45802	1.99147	37.-88905
5.-48252	4.-60749	-13.-87210	-1.45802	1.99147	11.-33671
3.-73246	2.-85744	-13.-87210	-1.45802	1.99147	16.-82693
1.-98241	1.-10738	-13.-87210	-1.45802	1.99147	31.-31065
.23235	-.64267	-13.-87210	-1.45802	1.99147	36.-65626
-1.-1170	-2.-39273	-13.-87210	-1.45802	1.99147	29.-86801
-3.-26776	-4.-14278	-13.-87210	-1.45802	1.99147	26.-38241
-5.-01781	-5.-69284	-13.-87210	-1.45802	1.99147	11.-33671
-6.-76787	-7.-64267	-13.-87210	-1.45802	1.99147	16.-82693
-7.-51792	-8.-39273	-13.-87210	-1.45802	1.99147	31.-31065
-10.-26798	-11.-14300	-13.-87210	-1.45802	1.99147	36.-65626
22.-56539	21.-62306	-9.-91099	-1.-04169	1.99147	15.-02672
20.-68073	19.-73840	-9.-91099	-1.-04169	1.99147	22.-01719
18.-79607	17.-85374	-9.-91099	-1.-04169	1.99147	35.-38270
16.-91141	15.-96908	-9.-91099	-1.-04169	1.99147	34.-06763
15.-C2675	14.-08442	-9.-91099	-1.-04169	1.99147	32.-71043
13.-14209	12.-19976	-9.-91099	-1.-04169	1.99147	25.-28316
11.-25743	10.-31510	-9.-91099	-1.-04169	1.99147	23.-67056
9.-37277	8.-43044	-9.-91099	-1.-04169	1.99147	22.-01719
7.-48811	6.-54578	-9.-91099	-1.-04169	1.99147	26.-85399
5.-60345	4.-66112	-9.-91099	-1.-04169	1.99147	25.-28316
3.-71879	2.-77646	-9.-91099	-1.-04169	1.99147	20.-32431
1.-83413	.89180	-9.-91099	-1.-04169	1.99147	20.-32431
-.05053	-.99286	-9.-91099	-1.-04169	1.99147	6.00000

REF. CHORD	C AVERAGE	TRUE AREA	REFRENCE AREA	B/2	REF. AR	TRUE AR	MACH NUMBER
-1.93519	-2.87752	-9.91099	-11.04169	1.99147	18.59357	6.00000	.28802
-3.61985	-4.76218	-9.91099	-11.04169	1.99147	16.82693	6.00000	.28802
-5.70451	-6.64684	-9.91099	-11.04169	1.99147	15.02672	6.00000	.28802
-7.58917	-8.53150	-9.91099	-11.04169	1.99147	13.19564	6.00000	.28802
-9.47383	-10.41616	-9.91099	-11.04169	1.99147	11.33671	6.00000	.28802
25.64782	24.63818	-5.94987	-6.62536	1.99147	37.88905	6.00000	.28986
23.62855	22.61892	-5.94987	-6.62536	1.99147	36.65626	6.00000	.28986
21.66929	20.59965	-5.94987	-6.62536	1.99147	35.38270	6.00000	.28986
19.59002	18.58039	-5.94987	-6.62536	1.99147	34.06763	6.00000	.28986
17.57076	16.56113	-5.94987	-6.62536	1.99147	32.71043	6.00000	.28986
15.55149	14.54186	-5.94987	-6.62536	1.99147	31.31065	6.00000	.28986
13.53223	12.52260	-5.94987	-6.62536	1.99147	29.86801	6.00000	.28986
21.51296	20.50333	-5.94987	-6.62536	1.99147	28.38241	6.00000	.28986
9.49370	8.48407	-5.94987	-6.62536	1.99147	26.85399	6.00000	.28986
7.47444	6.46480	-5.94987	-6.62536	1.99147	25.28316	6.00000	.28986
5.45517	4.44554	-5.94987	-6.62536	1.99147	23.67056	6.00000	.28986
3.43591	2.42627	-5.94987	-6.62536	1.99147	22.01719	6.00000	.28986
1.41664	.40701	-5.94987	-6.62536	1.99147	20.32431	6.00000	.28986
-6.02662	-1.61225	-5.94987	-6.62536	1.99147	18.59357	6.00000	.28986
-2.62199	-3.62152	-5.94987	-6.62536	1.99147	16.82693	6.00000	.28986
-4.64115	-5.65078	-5.94987	-6.62536	1.99147	15.02672	6.00000	.28986
-6.66061	-7.67075	-5.94987	-6.62536	1.99147	13.19564	6.00000	.28986
-8.67968	-9.69931	-5.94987	-6.62536	1.99147	11.33671	6.00000	.28986
28.73343	27.65643	-1.98466	-2.0860	1.99559	37.88905	6.00000	.29076
26.57942	25.50242	-1.98466	-2.0860	1.99559	36.65626	6.00000	.29076
24.42542	23.31341	-1.98466	-2.0860	1.99559	35.38270	6.00000	.29076
22.27141	21.19440	-1.98466	-2.0860	1.99559	34.06763	6.00000	.29076
20.11740	19.04040	-1.98466	-2.0860	1.99559	32.71043	6.00000	.29076
17.96339	16.88639	-1.98466	-2.0860	1.99559	31.31065	6.00000	.29076
15.80938	14.73238	-1.98466	-2.0860	1.99559	29.86801	6.00000	.29076
13.65537	12.57837	-1.98466	-2.0860	1.99559	28.38241	6.00000	.29076
11.50137	10.42436	-1.98466	-2.0860	1.99559	26.85399	6.00000	.29076
9.34736	8.27035	-1.98466	-2.0860	1.99559	25.28316	6.00000	.29076
7.19335	6.11635	-1.98466	-2.0860	1.99559	23.67056	6.00000	.29076
5.03934	3.96234	-1.98466	-2.0860	1.99559	22.01719	6.00000	.29076
2.88533	1.80833	-1.98466	-2.0860	1.99559	20.32431	6.00000	.29076
.73132	-.34568	-1.98466	-2.0860	1.99559	18.59357	6.00000	.29076
-1.42268	-2.49969	-1.98466	-2.0860	1.99559	16.82693	6.00000	.29076
-3.57669	-4.65370	-1.98466	-2.0860	1.99559	15.02672	6.00000	.29076
-5.73070	-6.80770	-1.98466	-2.0860	1.99559	13.19564	6.00000	.29076
-7.88471	-8.96171	-1.98466	-2.0860	1.99559	11.33671	6.00000	.29076

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REF. CHORD	C AVERAGE	TRUE AREA	REFRENCE AREA	B/2	REF. AR	TRUE AR	MACH NUMBER
20.96960	21.39785	3059.49486	2353.62960	71.49070	8.68602	6.68204	.80000

F I R S T   P L A N F O R M   S P A N   L O A D I N G

Y	CL+C
-71.05967	.022514
-70.25317	.046723
-69.60685	.043858
-67.35944	.0349994
-63.39833	.0500692
-59.43721	.0592968
-55.47610	.0667577
-51.51499	.0729915
-47.55387	.0783347
-43.59276	.0829622
-39.63164	.0869643
-35.67053	.0904525
-31.70941	.0934595
-26.73243	.0954440
-25.75544	.0971972
-21.79433	.0991962
-17.83321	.1008410
-13.87210	.1021487
-9.91099	.1031195
-5.94987	.1037792
-1.98466	.1040996

CL DEVELOPED ON THIS PLANFORM • .502247  
CH DEVELOPED ON THIS PLANFORM • -.112756

CL DESIGN = .500000 CL COMPUTED = .502247 CH COMPUTED = -.112756 CO V = .009034

## LOCAL ELEVATION DATA

Y= -71.0597      Y/B/2= -.9940      CHORD= 2.4614

SLOPES,  $dy/dx$ , AT SLOPE POINTS, FROM FRONT TO REAR  
 .6355 .5304 .4646 .4156 .3758 .3415 .3198 .2823 .2551 .2284 .2014 .1734 .1433 .1098 .0702 .0191-.0599-.2013  
 CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR  
 .0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

## LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
-.0000	.2471	-.0000	.6082
.0250	.2311	.0615	.5689
.0500	.2152	.1231	.5298
.0750	.2001	.1846	.4926
.1000	.1864	.2461	.4587
.1250	.1737	.3077	.4276
.1500	.1617	.3692	.3981
.1750	.1504	.4308	.3701
.2000	.1395	.4923	.3434
.2250	.1292	.5538	.3180
.2500	.1194	.6154	.2938
.2750	.1099	.6769	.2706
.3000	.1009	.7384	.2484
.3250	.0923	.8000	.2271
.3500	.0840	.8615	.2068
.3750	.0761	.9230	.1872
.4000	.0685	.9846	.1685
.4250	.0612	.1.0461	.1506
.4500	.0542	.1.1076	.1334
.4750	.0475	.1.1692	.1170
.5000	.0412	.1.2307	.1013
.5250	.0351	.1.2923	.0864
.5500	.0294	.1.3538	.0722
.5750	.0239	.1.4153	.0588
.6000	.0187	.1.4769	.0461
.6250	.0139	.1.5384	.0342
.6500	.0094	.1.5999	.0230

•6750	•0052	1•6615	•0127
•7000	•0013	1•7230	•0032
•7250	•-0022	1•7845	•-0055
•7500	•-0054	1•8461	•-0133
•7750	•-0082	1•9076	•-0201
•8000	•-0105	1•9691	•-0299
•8250	•-0124	2•0307	•-0306
•8500	•-0137	2•0922	•-0338
•8750	•-0144	2•1538	•-0356
•9000	•-0147	2•2153	•-0363
•9250	•-0144	2•2768	•-0354
•9500	•-0121	2•3384	•-0298
•9750	•-0069	2•3999	•-0170
1.0000	0.0000	2.4614	0.0000

Y= -70.2532      Y/B/2= -.9827      CHORD= 3.7602

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.6995 .5482 .4529 .3800 .3193 .2658 .2167 .1705 .1258 .0817 .0373-.0084-.0566-.1091-.1694-.2448-.3573-.6616  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
-.0000	.1128	-.0000	.4264
.0250	.0953	.0945	.3602
.0500	.0778	.1890	.2943
.0750	.0615	.2835	.2326
.1000	.0471	.3780	.1781
.1250	.0343	.4725	.1295
.1500	.0224	.5670	.0848
.1750	.0114	.6615	.0432
.2000	.0013	.7560	.0048
.2250	-.0081	.8506	-.0307
.2500	-.0168	.9451	-.0634
.2750	-.0246	1.0396	-.0937
.3000	-.0322	1.1341	-.1217
.3250	-.0390	1.2286	-.1474
.3500	-.0452	1.3231	-.1710
.3750	-.0509	1.4176	-.1925
.4000	-.0561	1.5121	-.2120
.4250	-.0607	1.6066	-.2295
.4500	-.0648	1.7011	-.2451
.4750	-.0685	1.7956	-.2588
.5000	-.0716	1.8901	-.2705
.5250	-.0742	1.9846	-.2805
.5500	-.0763	2.0791	-.2885
.5750	-.0779	2.1736	-.2946
.6000	-.0791	2.2681	-.2989
.6250	-.0797	2.3626	-.3013
.6500	-.0798	2.4571	-.3017
.6750	-.0794	2.5517	-.3001
.7000	-.0784	2.6462	-.2965
.7250	-.0769	2.7407	-.2908

ORIGINAL PAGE IS  
OF POOR QUALITY

.7500	-.0748	2.8352	-.2829
.7750	-.0721	2.9297	-.2727
.8000	-.0688	3.0242	-.2602
.8250	-.0648	3.1187	-.2450
.8500	-.0599	3.2132	-.2265
.8750	-.0542	3.3077	-.2047
.9000	-.0478	3.4022	-.1806
.9250	-.0404	3.4967	-.1528
.9500	-.0304	3.5912	-.1150
.9750	-.0164	3.6857	-.0618
1.0000	0.0000	3.7802	0.0000

Y= -69.6089      Y/8/2= -9737      CHORD= 6.2535

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.7046 .5460 .4554 .3956 .3539 .3249 .3056 .2941 .2884 .2867 .2872 .2884 .2888 .2863 .2776 .2579 .2142 .0616  
 CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR  
 .0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6526 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
-0.0000	.3377	-0.0000	2.1118
.0250	.3200	.1563	2.0009
.0500	.3023	.3127	1.8907
.0750	.2859	.4690	1.7880
.1000	.2715	.6254	1.6979
.1250	.2587	.7817	1.6179
.1500	.2469	.9380	1.5440
.1750	.2358	1.0944	1.4745
.2000	.2254	1.2507	1.4093
.2250	.2156	1.4070	1.3480
.2500	.2063	1.5634	1.2899
.2750	.1974	1.7197	1.2344
.3000	.1889	1.8761	1.1812
.3250	.1807	2.0324	1.1299
.3500	.1727	2.1887	1.0803
.3750	.1650	2.3451	1.0319
.4000	.1575	2.5014	.9846
.4250	.1500	2.6577	.9382
.4500	.1427	2.8161	.8923
.4750	.1354	2.9704	.8470
.5000	.1282	3.1268	.8019
.5250	.1210	3.2831	.7570
.5500	.1139	3.4394	.7121
.5750	.1067	3.5958	.6673
.6000	.0995	3.7521	.6225
.6250	.0924	3.9084	.5775
.6500	.0851	4.0648	.5325
.6750	.0779	4.2211	.4874
.7000	.0707	4.3775	.4422
.7250	.0635	4.5338	.3971

•.7500	•.0563	4.6901	•3521
•.7750	•.0491	4.8465	•3073
•.8000	•.0620	5.0020	•2629
•.8250	•.0350	5.1591	•2192
•.8500	•.0283	5.3155	•1766
•.8750	•.0217	5.4718	•1360
•.9000	•.0153	5.6282	•0960
•.9250	•.0093	5.7845	•0579
•.9500	•.0044	5.9408	•0277
•.9750	•.0016	6.0972	•0102
1.0000	0.0000	6.2535	0.0000

Y= -67.3594      Y= 8.225      Y= 8.225

SLOPES,  $dy/dx$ , AT SLOPE POINTS, FROM FRONT TO REAR

.1142 .0922 .0785 .0681 .0592 .0511 .0437 .0368 .0302 .0236 .0176 .0113 .0048-.0022-.0104-.0209-.0375-.0849  
 CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR  
 .0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	LOCAL ELEVATION	DELTA X	DELTA Z
0.0000	.0292	0.0000	.2578	
.0250	.0264	.2206	.2325	
.0500	.0235	.4421	.2073	
.0750	.0208	.6617	.1835	
.1000	.0184	.8822	.1622	
.1250	.0162	1.1028	.1430	
.1500	.0142	1.3234	.1251	
.1750	.0123	1.5439	.1081	
.2000	.0105	1.7645	.0923	
.2250	.0088	1.9851	.0774	
.2500	.0072	2.2056	.0635	
.2750	.0057	2.4262	.0504	
.3000	.0043	2.6467	.0381	
.3250	.0030	2.8673	.0266	
.3500	.0018	3.0879	.0159	
.3750	.0007	3.3084	.0059	
.4000	-.0004	3.5290	-.0034	
.4250	-.0014	3.7496	-.0120	
.4500	-.0023	3.9701	-.0200	
.4750	-.0031	4.1907	-.0272	
.5000	-.0038	4.4112	-.0339	
.5250	-.0045	4.6318	-.0398	
.5500	-.0051	4.8524	-.0452	
.5750	-.0057	5.0729	-.0499	
.6000	-.0061	5.2935	-.0540	
.6250	-.0065	5.5141	-.0575	
.6500	-.0068	5.7346	-.0604	
.6750	-.0071	5.9552	-.0627	
.7000	-.0073	6.1757	-.0643	
.7250	-.0074	6.3963	-.0652	

ORIGINAL PAGE IS  
OF POOR QUALITY

• 7500	-0.0074	6.6169
• 7750	-0.0074	-0.0655
• 8000	-0.0072	6.6374
• 8250	-0.0070	-0.0651
• 8500	-0.0067	7.0580
• 8750	-0.0062	-0.0651
• 9000	-0.0056	7.2786
• 9250	-0.0049	7.4991
• 9500	-0.0038	-0.0588
• 9750	-0.0021	7.7167
1.0000	0.0000	8.8225

Y= -63.3983      Y/8/2= -.8868      CHORD= 10.2419

STOPE, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR  
 .1166 .0886 .0709 .0574 .0460 .0359 .0264 .0174 .0086-.0002-.0092-.0184-.0283-.0391-.0516-.0672-.0902-.1513  
 CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR  
 .0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

## LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	.0044	0.0000	.0455
.0250	.0015	.2560	.0155
.0500	-.0014	.5121	-.0144
.0750	-.0041	.7681	-.0421
.1000	-.0065	1.0242	-.0662
.1250	-.0085	1.2802	-.0872
.1500	-.0104	1.5363	-.1063
.1750	-.0121	1.7923	-.1239
.2000	-.0137	2.0484	-.1398
.2250	-.0151	2.3044	-.1543
.2500	-.0163	2.5605	-.1674
.2750	-.0175	2.8165	-.1793
.3000	-.0185	3.0726	-.1899
.3250	-.0195	3.3286	-.1994
.3500	-.0203	3.5847	-.2078
.3750	-.0210	3.8407	-.2151
.4000	-.0216	4.0968	-.2214
.4250	-.0221	4.3529	-.2266
.4500	-.0225	4.6089	-.2308
.4750	-.0228	4.8649	-.2339
.5000	-.0230	5.1209	-.2361
.5250	-.0232	5.3770	-.2372
.5500	-.0232	5.6330	-.2373
.5750	-.0231	5.8891	-.2364
.6000	-.0229	6.1451	-.2345
.6250	-.0226	6.4012	-.2315
.6500	-.0222	6.6572	-.2274
.6750	-.0217	6.9133	-.2223
.7000	-.0211	7.1693	-.2160
.7250	-.0204	7.4254	-.2085

.7500	-.0195	7.6814	-.1999
.7750	-.0185	7.9375	-.1899
.8000	-.0174	8.1935	-.1787
.8250	-.0162	8.4496	-.1659
.8500	-.0148	8.7056	-.1513
.8750	-.0132	8.9617	-.1349
.9000	-.0114	9.2177	-.1171
.9250	-.0095	9.4738	-.0973
.9500	-.0070	9.7298	-.0720
.9750	-.0037	9.9859	-.0383
1.0000	0.0000	10.2419	0.0000

Y= -59.4372      Y/8/2=      -.0314      CHORD= 11.6613

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR  
 .1139 .0846 .0662 .0523 .0407 .0305 .0211 .0123 .0038-.0046-.0132-.0221-.0315-.0420-.0542-.0696-.0929-.1558  
 CURRENTING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	.0004	0.0000	.0050
*0250	-.0024	.2915	-.0285
*0500	-.0053	.5831	-.0617
*0750	-.0079	.8746	-.0924
*1000	-.0102	1.1661	-.1187
*1250	-.0121	1.4577	-.1414
*1500	-.0139	1.7492	-.1619
*1750	-.0155	2.0407	-.1805
*2000	-.0169	2.3323	-.1972
*2250	-.0182	2.6238	-.2122
*2500	-.0193	2.9153	-.2255
*2750	-.0204	3.2069	-.2375
*3000	-.0213	3.4984	-.2480
*3250	-.0221	3.7899	-.2573
*3500	-.0227	4.0815	-.2652
*3750	-.0233	4.3730	-.2720
*4000	-.0238	4.6645	-.2776
*4250	-.0242	4.9561	-.2820
*4500	-.0245	5.2476	-.2853
*4750	-.0246	5.5391	-.2874
*5000	-.0247	5.8306	-.2885
*5250	-.0247	6.1222	-.2884
*5500	-.0246	6.4137	-.2872
*5750	-.0244	6.7052	-.2850
*6000	-.0241	6.9968	-.2816
*6250	-.0238	7.2883	-.2770
*6500	-.0233	7.5798	-.2713
*6750	-.0227	7.8714	-.2644
*7000	-.0220	8.1629	-.2563
*7250	-.0212	8.4544	-.2469

.7500	-0.0202	8.7460	-0.2361
.7750	-0.0192	9.0375	-.2239
.8000	-0.0180	9.3290	-.2103
.8250	-0.0167	9.6206	-.1951
.8500	-0.0152	9.9121	-.1777
.8750	-0.0136	10.2036	-.1583
.9000	-0.0118	10.4952	-.1373
.9250	-0.0098	10.7867	-.1141
.9500	-0.0072	11.0782	-.0844
.9750	-0.0039	11.3698	-.0650
1.00000	0.0000	11.6613	0.0000

Y= -55.4761      Y/B/2= -0.7760      CHORD= 13.0807

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.1093 .0798 .0612 .0471 .0355 .0252 .0159 .0072-.0012-.0095-.0178-.0265-.0357-.0459-.0578-.0729-.0959-.1587  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2043 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0040	0.0000	-0.0529
0.0250	-0.0068	.3270	-.0890
0.0500	-0.0095	.6540	-.1247
0.0750	-0.0120	.9811	-.1576
0.1000	-0.0142	1.3081	-.1856
0.1250	-0.0160	1.6351	-.2095
0.1500	-0.0176	1.9621	-.2308
0.1750	-0.0191	2.2891	-.2500
0.2000	-0.0204	2.6161	-.2671
0.2250	-0.0216	2.9432	-.2822
0.2500	-0.0226	3.2702	-.2955
0.2750	-0.0235	3.5972	-.3072
0.3000	-0.0243	3.9242	-.3173
0.3250	-0.0249	4.2512	-.3260
0.3500	-0.0255	4.5782	-.3332
0.3750	-0.0259	4.9053	-.3391
0.4000	-0.0263	5.2323	-.3436
0.4250	-0.0265	5.5593	-.3469
0.4500	-0.0267	5.8863	-.3489
0.4750	-0.0267	6.2133	-.3497
0.5000	-0.0267	6.5403	-.3493
0.5250	-0.0266	6.8674	-.3476
0.5500	-0.0264	7.1944	-.3447
0.5750	-0.0260	7.5214	-.3406
0.6000	-0.0256	7.8484	-.3352
0.6250	-0.0251	8.1754	-.3286
0.6500	-0.0245	8.5025	-.3208
0.6750	-0.0238	8.8295	-.3116
0.7000	-0.0230	9.1565	-.3011
0.7250	-0.0221	9.4835	-.2892

•7500	-0.0211	9.8105
.7750	-0.0199	10.1375
.8000	-0.0187	10.4646
.8250	-0.0173	10.7916
.8500	-0.0157	11.1186
.8750	-0.0140	11.4456
.9000	-0.0121	11.7726
.9250	-0.0100	12.0996
.9500	-0.0074	12.4267
.9750	-0.0039	12.7537
1.0000	0.0000	13.0807

ORIGINAL PAGE IS  
OF POOR QUALITY

Y= -51.5150      Y/8/2= -7.7206      CHORD= 14.5001

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR.  
 .1039 .0747 .0563 .0424 .0308 .0208 .0116 .0031-.0051--.0132--.0213--.0297--.0386--.0485--.0600--.0748--.0972--.1589.  
 CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0076	0.0000	-.1105
*0250	-.0102	.3625	-.1485
*0500	-.0126	.7250	-.1862
*0750	-.0152	1.0875	-.2208
*1000	-.0172	1.4500	-.2499
*1250	-.0189	1.8125	-.2746
*1500	-.0204	2.1750	-.2964
*1750	-.0218	2.5375	-.3159
*2000	-.0230	2.9000	-.3331
*2250	-.0240	3.2625	-.3481
*2500	-.0249	3.6250	-.3612
*2750	-.0257	3.9875	-.3725
*3000	-.0263	4.3500	-.3820
*3250	-.0269	4.7125	-.3900
*3500	-.0273	5.0750	-.3964
*3750	-.0277	5.4375	-.4014
*4000	-.0279	5.8000	-.4049
*4250	-.0281	6.1625	-.4070
*4500	-.0281	6.5250	-.4077
*4750	-.0281	6.8875	-.4071
*5000	-.0279	7.2500	-.4052
*5250	-.0277	7.6125	-.4020
*5500	-.0274	7.9751	-.3974
*5750	-.0270	8.3376	-.3915
*6000	-.0265	8.7001	-.3843
*6250	-.0259	9.0626	-.3758
*6500	-.0252	9.4251	-.3659
*6750	-.0245	9.7876	-.3546
*7000	-.0236	10.1501	-.3418
*7250	-.0226	10.5126	-.3276

.7500	-0.0215
.7750	-0.0203
.8000	-0.0190
.8250	-0.0175
.8500	-0.0159
.8750	-0.0141
.9000	-0.0122
.9250	-0.0101
.9500	-0.0074
.9750	-0.0039
1.0000	0.0000
	10.8751
	11.2376
	11.6001
	11.9626
	12.3251
	12.6876
	13.0501
	13.4126
	13.7751
	14.1376
	14.5001
	0.0000

Y= -47.5539      Y/8/2= -6652      CHORD= 15.9195

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0982 .0696 .0515 .0378 .0265 .0167 .0078-.0005-.0163-.0242-.0323-.0409-.0504-.0616-.0759-.0977-.1578  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR  
.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7063 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-.0107	0.0000	-.1711
.0250	-.0132	.3980	-.2105
.0500	-.0157	.7960	-.2496
.0750	-.0179	1.1940	-.2853
.1000	-.0198	1.5919	-.3152
.1250	-.0214	1.9899	-.3403
.1500	-.0228	2.3879	-.3623
.1750	-.0240	2.7859	-.3818
.2000	-.0251	3.1839	-.3988
.2250	-.0260	3.5819	-.4135
.2500	-.0268	3.9799	-.4261
.2750	-.0274	4.3779	-.4368
.3000	-.0280	4.7758	-.4456
.3250	-.0284	5.1738	-.4527
.3500	-.0288	5.5719	-.4582
.3750	-.0290	5.9699	-.4620
.4000	-.0292	6.3678	-.4644
.4250	-.0292	6.7658	-.4652
.4500	-.0292	7.1638	-.4646
.4750	-.0291	7.5618	-.4626
.5000	-.0288	7.9597	-.4591
.5250	-.0285	8.3577	-.4542
.5500	-.0281	8.7557	-.4460
.5750	-.0277	9.1537	-.4403
.6000	-.0271	9.5517	-.4312
.6250	-.0264	9.9497	-.4207
.6500	-.0257	10.3477	-.4088
.6750	-.0248	10.7457	-.3953
.7000	-.0239	11.1436	-.3804
.7250	-.0229	11.5416	-.3638

ORIGINAL PAGE IS  
OF POOR QUALITY

<b>.7500</b>	<b>-.0217</b>	<b>11.9396</b>
.7750	-.0205	12.3376
.8000	-.0191	12.7356
.8250	-.0176	13.1336
.8500	-.0159	13.5316
.8750	-.0141	13.9296
.9000	-.0121	14.3275
.9250	-.0100	14.7255
.9500	-.0074	15.1235
.9750	-.0039	15.5215
<b>1.0000</b>	<b>0.0000</b>	<b>15.9195</b>

<b>-.3455</b>	<b>-.3256</b>	<b>-.3038</b>
<b>-.2799</b>	<b>-.2534</b>	<b>-.2243</b>
<b>-.1933</b>	<b>-.1594</b>	<b>-.1172</b>
<b>-.0622</b>	<b>0.0000</b>	

Y= -43.5928      Y/8/2= -0.6098      CHORD= 17.3389

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0922 .0643 .0467 .0333 .0223 .0128 .0041-.0039-.0116--.0192--.0268--.0346--.0429--.0521--.0628--.0765--.0976--.1560  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4366 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0136	0.0000	-.2364
.0250	-.0160	.4335	-.2768
.0500	-.0183	.8669	-.3168
.0750	-.0204	1.3004	-.3531
.1000	-.0221	1.7339	-.3834
.1250	-.0236	2.1674	-.4085
.1500	-.0248	2.6008	-.4303
.1750	-.0259	3.0343	-.4495
.2000	-.0269	3.4678	-.4661
.2250	-.0277	3.9013	-.4802
.2500	-.0284	4.3347	-.4920
.2750	-.0289	4.7692	-.5018
.3000	-.0294	5.2017	-.5097
.3250	-.0297	5.6351	-.5157
.3500	-.0300	6.0686	-.5200
.3750	-.0301	6.5021	-.5226
.4000	-.0302	6.9356	-.5236
.4250	-.0302	7.3690	-.5230
.4500	-.0300	7.8025	-.5209
.4750	-.0298	8.2360	-.5172
.5000	-.0295	8.6694	-.5121
.5250	-.0292	9.1029	-.5055
.5500	-.0287	9.5364	-.4974
.5750	-.0281	9.9699	-.4879
.6000	-.0275	10.4033	-.4768
.6250	-.0268	10.8368	-.4643
.6500	-.0260	11.2703	-.4503
.6750	-.0251	11.7038	-.4347
.7000	-.0241	12.1372	-.4175
.7250	-.0230	12.5707	-.3986

.7500	.0218	13.0042	-.3780
.7750	.0205	13.4376	-.3555
.8000	.0191	13.8711	-.3312
.8250	.0176	14.3046	-.3046
.8500	.0159	14.7381	-.2753
.8750	.0140	15.1715	-.2433
.9000	.0121	15.6050	-.2093
.9250	.0099	16.0385	-.1722
.9500	.0073	16.4720	-.1263
.9750	.0039	16.9054	-.0670
1.0000	0.0000	17.3389	0.0000

Y= -39.6316 Y/8/2= -.5544 CHORD= 18.7583

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0861 .0590 .0418 .0289 .0162 .0089 .0006-.0072-.0146-.0219-.0291-.0366-.0446-.0533-.0636-.0768-.0971-.1535  
 CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR  
 .0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-.0164	0.0000	-.3068
.0250	-.0185	.4690	-.3476
.0500	-.0207	.9379	-.3880
.0750	-.0226	1.4069	-.4246
.1000	-.0242	1.8758	-.4547
.1250	-.0256	2.3448	-.4795
.1500	-.0267	2.8137	-.5008
.1750	-.0277	3.2827	-.5193
.2000	-.0285	3.7517	-.5351
.2250	-.0292	4.2206	-.5482
.2500	-.0298	4.6896	-.5590
.2750	-.0303	5.1585	-.5677
.3000	-.0306	5.6275	-.5743
.3250	-.0309	6.0964	-.5790
.3500	-.0310	6.5654	-.5819
.3750	-.0311	7.0344	-.5830
.4000	-.0310	7.5033	-.5824
.4250	-.0309	7.9723	-.5802
.4500	-.0307	8.4412	-.5764
.4750	-.0304	8.9102	-.5710
.5000	-.0301	9.3791	-.5640
.5250	-.0296	9.8481	-.5556
.5500	-.0291	10.3171	-.5456
.5750	-.0285	10.7860	-.5340
.6000	-.0278	11.2550	-.5210
.6250	-.0270	11.7239	-.5063
.6500	-.0261	12.1929	-.4901
.6750	-.0252	12.6618	-.4723
.7000	-.0241	13.1308	-.4529
.7250	-.0230	13.5998	-.4317

•.7500	-•.0218	14.0687	-•.4086
.7750	-•.0205	14.5377	-•.3837
•.8000	-•.0190	15.0066	-•.3569
•.8250	-•.0175	15.4756	-•.3278
•.8500	-•.0158	15.9446	-•.2998
•.8750	-•.0139	16.4135	-•.2609
•.9000	-•.0119	16.8825	-•.2240
•.9250	-•.0098	17.3514	-•.1840
•.9500	-•.0072	17.8204	-•.1347
•.9750	-•.0038	18.2893	-•.0713
1.0000	0.0000	18.7583	0.0000

Y= -35.6705      Y/B/2= -0.4990      CHORD= 20.1777

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR  
 CORESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0797 .0534 .0367 .0241 .0137 .0047-.0034-.0109-.0181-.0250-.0320-.0391-.0467-.0550--.0648--.0774--.0968--.1512  
 .0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0194	0.0000	-0.3919
.0250	-0.0214	.5044	-.4325
.0500	-0.0234	1.0069	-.4728
.0750	-0.0252	1.5133	-.5091
.1000	-0.0267	2.0178	-.5386
.1250	-0.0279	2.5222	-.5625
.1500	-0.0289	3.0267	-.5827
.1750	-0.0297	3.5311	-.6001
.2000	-0.0305	4.0355	-.6146
.2250	-0.0310	4.5400	-.6263
.2500	-0.0315	5.0444	-.6356
.2750	-0.0318	5.5489	-.6427
.3000	-0.0321	6.0533	-.6476
.3250	-0.0322	6.5570	-.6505
.3500	-0.0323	7.0622	-.6515
.3750	-0.0322	7.5666	-.6507
.4000	-0.0321	8.0711	-.6481
.4250	-0.0319	8.5755	-.6438
.4500	-0.0316	9.0800	-.6378
.4750	-0.0312	9.5844	-.6302
.5000	-0.0308	10.0886	-.6210
.5250	-0.0302	10.5933	-.6102
.5500	-0.0296	11.0977	-.5979
.5750	-0.0289	11.6022	-.5839
.6000	-0.0282	12.1066	-.5684
.6250	-0.0273	12.6111	-.5513
.6500	-0.0264	13.1155	-.5326
.6750	-0.0254	13.6199	-.5122
.7000	-0.0243	14.1244	-.4901
.7250	-0.0231	14.6288	-.4663

ORIGINAL PAGE IS  
 OF POOR QUALITY

.7500	-0.0218	15.1333	-.4406
.7750	-0.0205	15.6377	-.4129
.8000	-0.0190	16.1422	-.3833
.8250	-0.0174	16.6466	-.3514
.8500	-0.0157	17.1510	-.3165
.8750	-0.0138	17.6555	-.2766
.9000	-0.0118	18.1599	-.2367
.9250	-0.0097	18.6644	-.1956
.9500	-0.0071	19.1688	-.1429
.9750	-0.0037	19.6733	-.0756
1.0000	0.0000	20.1777	0.0000

Y= -31.7094      Y/A/2= -4435      CHORD= 21.5971

SLOPES,DX/DZ,AT SLOPE POINTS, FROM FRONT TO REAR

.0728 .0472 .0308 .0165 .0082-.0006-.0086-.0160-.0230--.0298-.0365--.0433--.0505--.0583--.0675--.0792--.0975--.1497  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0600	-0.0237	0.0000	-5121
.0250	-0.0256	.5399	-5519
.0500	-0.0274	1.0799	-5913
.0750	-0.0290	1.6198	-6265
.1000	-0.0303	2.1597	-6546
.1250	-0.0313	2.6996	-6769
.1500	-0.0322	3.2396	-6954
.1750	-0.0329	3.7795	-7109
.2000	-0.0335	4.3194	-7233
.2250	-0.0339	4.8593	-7328
.2500	-0.0343	5.3993	-7398
.2750	-0.0345	5.9392	-7443
.3000	-0.0346	6.4791	-7467
.3250	-0.0346	7.0191	-7469
.3500	-0.0345	7.5590	-7451
.3750	-0.0343	8.0989	-7414
.4000	-0.0341	8.6388	-7359
.4250	-0.0337	9.1788	-7285
.4500	-0.0333	9.7187	-7194
.4750	-0.0328	10.2586	-7086
.5000	-0.0322	10.7985	-6960
.5250	-0.0316	11.3385	-6819
.5500	-0.0308	11.8784	-6661
.5750	-0.0300	12.4183	-6486
.6000	-0.0292	12.9583	-6296
.6250	-0.0282	13.4982	-6088
.6500	-0.0272	14.0381	-5865
.6750	-0.0260	14.5780	-5624
.7000	-0.0248	15.1180	-5366
.7250	-0.0236	15.6579	-5091

.7500	-0.0222	16.1978	-4.796
.7750	-0.0208	16.7377	-4.482
.8000	-0.0192	17.2777	-4.146
.8250	-0.0176	17.8176	-3.791
.8500	-0.0158	18.3575	-3.405
.8750	-0.0138	18.8975	-2.989
.9000	-0.0118	19.4374	-2.552
.9250	-0.0096	19.9773	-2.083
.9500	-0.0070	20.5172	-1.517
.9750	-0.0037	21.0572	-0.801
1.0000	0.0000	21.5971	0.000

Y= -28.7324      Y/8/2= -4019      CHORD= 22.6638

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0674 .0419 .0255 .0129 .0025-.0066-.0149-.0225-.0298-.0368-.0437-.0507-.0579-.0656-.0744-.0852-.1015-.1495  
CORRESPONDING X/C LOCATIONS FRM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0297	0.0000	-0.6727
*0250	-0.0314	*5666	-.7113
*0500	-0.0331	1.1332	-.7495
*0750	-0.0346	1.6998	-.7834
*1000	-0.0357	2.2664	-.8100
*1250	-0.0366	2.8330	-.8304
*1500	-0.0374	3.3996	-.8468
*1750	-0.0379	3.9662	-.8600
*2000	-0.0384	4.5328	-.8699
*2250	-0.0387	5.0994	-.8767
*2500	-0.0389	5.6660	-.8808
*2750	-0.0391	6.2326	-.8823
*3000	-0.0393	6.7992	-.8815
*3250	-0.0398	7.3658	-.8784
*3500	-0.0395	7.9323	-.8730
*3750	-0.0392	8.4989	-.8656
*4000	-0.0378	9.0655	-.8562
*4250	-0.0373	9.6321	-.8448
*4500	-0.0367	10.1987	-.8315
*4750	-0.0360	10.7653	-.8164
*5000	-0.0353	11.3319	-.7994
*5250	-0.0344	11.8985	-.7806
*5500	-0.0335	12.4651	-.7601
*5750	-0.0326	13.0317	-.7378
*6000	-0.0315	13.5983	-.7137
*6250	-0.0303	14.1649	-.6878
*6500	-0.0291	14.7315	-.6602
*6750	-0.0278	15.2981	-.6308
*7000	-0.0265	15.8647	-.5996
*7250	-0.0250	16.4313	-.5664

ORIGINAL PAGE IS  
OF POOR QUALITY

•7500	•0234	16.9979
•7750	-•0216	17.5645
•8000	-•0201	18.1311
•8250	-•0183	18.6977
•8500	-•0163	19.2643
•8750	-•0142	19.8309
•9000	-•0121	20.3975
•9250	-•0098	20.9641
•9500	-•0071	21.5307
•9750	-•0037	22.0973
1.0000	0.0000	22.6636

•5313	-•5313
-•4943	-•4943
-•4552	-•4552
-•4137	-•4137
-•3694	-•3694
-•3222	-•3222
-•2732	-•2732
-•2212	-•2212
-•1598	-•1598
-•0840	-•0840
0.0000	0.0000

Y = -25.7554      Y/8/2 = -.3603      CHORD = 24.2323

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0602 .0360 .0206 .0089-.0005-.0089-.0163-.0231-.0295-.0357-.0519-.0479-.0542-.0610-.0667-.0764-.0928-.1333  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.2288	0.0000	-0.6972
.0250	-0.0303	.6058	-.7341
.0500	-0.0318	1.2116	-.7706
.0750	-0.0331	1.8174	-.8028
.1000	-0.0341	2.4232	-.8274
.1250	-0.0349	3.0290	-.8458
.1500	-0.0355	3.6349	-.8602
.1750	-0.0360	4.2407	-.8715
.2000	-0.0363	4.8465	-.8794
.2250	-0.0365	5.4523	-.8844
.2500	-0.0366	6.0581	-.8866
.2750	-0.0366	6.6639	-.8863
.3000	-0.0365	7.2697	-.8838
.3250	-0.0363	7.8755	-.8790
.3500	-0.0360	8.4813	-.8721
.3750	-0.0356	9.0871	-.8632
.4000	-0.0352	9.6929	-.8523
.4250	-0.0346	10.2987	-.8396
.4500	-0.0341	10.9046	-.8251
.4750	-0.0334	11.5104	-.8088
.5000	-0.0326	12.1162	-.7909
.5250	-0.0318	12.7220	-.7712
.5500	-0.0309	13.3278	-.7498
.5750	-0.0300	13.9336	-.7268
.6000	-0.0290	14.5394	-.7021
.6250	-0.0279	15.1452	-.6758
.6500	-0.0267	15.7510	-.6478
.6750	-0.0255	16.3568	-.6182
.7000	-0.0242	16.9626	-.5868
.7250	-0.0228	17.5684	-.5536

7500	-0.0214	18.1743	-5186
7750	-0.0199	18.7801	-4618
8000	-0.0183	19.3859	-4430
8250	-0.0166	19.9917	-4021
8500	-0.0148	20.5975	-3584
8750	-0.0129	21.2033	-3120
9000	-0.0109	21.8091	-2637
9250	-0.0088	22.4149	-2125
9500	-0.0063	23.0207	-1528
9750	-0.0033	23.6265	-0801
11000	0.0000	24.2323	0.0000

Y= -21.7943      Y/8/2=      -3049      CHORD= 26.6552

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0527 .0302 .0159 .0053-.0034-.0108-.0174-.0234-.0290-.0344-.0397-.0450-.0505-.0564-.0633-.0720-.0854-.1233  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
.0000	-.0281	.0000	-.7486
.0250	-.0294	.6664	-.7841
.0500	-.0307	1.3328	-.8193
.0750	-.0319	1.9991	-.8500
.1000	-.0328	2.6655	-.8730
.1250	-.0334	3.3319	-.8897
.1500	-.0339	3.9983	-.9023
.1750	-.0342	4.6647	-.9117
.2000	-.0344	5.3310	-.9178
.2250	-.0345	5.9974	-.9208
.2500	-.0346	6.6638	-.9211
.2750	-.0345	7.3302	-.9190
.3000	-.0343	7.9966	-.9146
.3250	-.0341	8.6629	-.9080
.3500	-.0337	9.3293	-.8993
.3750	-.0333	9.9957	-.8886
.4000	-.0329	10.6621	-.8761
.4250	-.0323	11.3285	-.8618
.4500	-.0317	11.9949	-.8457
.4750	-.0311	12.6612	-.8279
.5000	-.0303	13.3276	-.8085
.5250	-.0295	13.9940	-.7874
.5500	-.0287	14.6604	-.7648
.5750	-.0278	15.3268	-.7405
.6000	-.0268	15.9931	-.7147
.6250	-.0258	16.6595	-.6873
.6500	-.0247	17.3259	-.6584
.6750	-.0236	17.9923	-.6278
.7000	-.0223	18.6587	-.5956
.7250	-.0211	19.3250	-.5616

.7500	-.0197	19.9914	-.5259
.7750	-.0183	20.6578	-.4884
.8000	-.0168	21.3242	-.4491
.8250	-.0153	21.9906	-.4076
.8500	-.0136	22.6569	-.3634
.8750	-.0119	23.3233	-.3164
.9000	-.0100	23.9897	-.2677
.9250	-.0081	24.6561	-.2159
.9500	-.0058	25.3225	-.1555
.9750	-.0031	25.9888	-.0815
1.0000	0.0000	26.6552	0.0000

20.3045 JAVINGEN  
KTHAUP 4000 20

Y= -17.8332      Y/8/2= -2494      CHORO= 29.0781

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0294	0.0000	-0.8539
.0250	-0.0305	.7270	-0.8873
.0500	-0.0317	1.4539	-0.9203
.0750	-0.0326	2.1809	-0.9488
.1000	-0.0333	2.9078	-0.9694
.1250	-0.0338	3.6348	-0.9836
.1500	-0.0342	4.3617	-0.9936
.1750	-0.0344	5.0887	-1.0003
.2000	-0.0345	5.8156	-1.0037
.2250	-0.0345	6.5426	-1.0040
.2500	-0.0344	7.2695	-1.0015
.2750	-0.0343	7.9965	-0.9966
.3000	-0.0340	8.7234	-0.9893
.3250	-0.0337	9.4504	-0.9798
.3500	-0.0333	10.1773	-0.9682
.3750	-0.0328	10.9043	-0.9547
.4000	-0.0323	11.6312	-0.9393
.4250	-0.0317	12.3582	-0.9220
.4500	-0.0311	13.0851	-0.9031
.4750	-0.0303	13.8121	-0.8825
.5000	-0.0296	14.5391	-0.8602
.5250	-0.0288	15.2660	-0.8364
.5500	-0.0279	15.9930	-0.8109
.5750	-0.0270	16.7199	-0.7839
.6000	-0.0260	17.4469	-0.7554
.6250	-0.0249	18.1738	-0.7253
.6500	-0.0239	18.9008	-0.6937
.6750	-0.0227	19.6277	-0.6605
.7000	-0.0215	20.3547	-0.6257
.7250	-0.0203	21.0816	-0.5892

ORIGINAL PAGE IS  
OF POOR QUALITY

.7500	-0.0190	21.8086
.7750	-0.0176	22.5355
.8000	-0.0161	23.2625
.8250	-0.0146	23.9894
.8500	-0.0130	24.7164
.8750	-0.0113	25.4433
.9000	-0.0096	26.1703
.9250	-0.0077	26.8973
.9500	-0.0055	27.6242
.9750	-0.0029	28.3512
1.0000	0.0000	29.0781

		-0.5510
		-0.5111
		-0.4693
		-0.4253
		-0.3787
		-0.3293
		-0.2782
		-0.2240
		-0.1610
		-0.0844
		0.0000

Y= -13.8721      Y/B/2=      -1.940      CHORD= 31.5010

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0379 .0180 .0055-.0039-.0114--.0176--.0234--.0285--.0331--.0375--.0418--.0461--.0505--.0553--.0609--.0682--.0795--.1123  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0072 .1520 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA Z
0.0000	-0.0317	0.0000
.0250	-0.0327	.7875
.0500	-0.0336	1.5750
.0750	-0.0346	2.3626
.1000	-0.0350	3.1501
.1250	-0.0353	3.9376
.1500	-0.0355	4.7251
.1750	-0.0356	5.5127
.2000	-0.0356	6.3002
.2250	-0.0355	7.0877
.2500	-0.0353	7.8752
.2750	-0.0350	8.6628
.3000	-0.0347	9.4503
.3250	-0.0342	10.2378
.3500	-0.0337	11.0253
.3750	-0.0332	11.8129
.4000	-0.0326	12.6004
.4250	-0.0319	13.3879
.4500	-0.0312	14.1754
.4750	-0.0304	14.9630
.5000	-0.0295	15.7505
.5250	-0.0287	16.5380
.5500	-0.0277	17.3255
.5750	-0.0268	18.1131
.6000	-0.0257	18.9066
.6250	-0.0247	19.6981
.6500	-0.0235	20.4756
.6750	-0.0224	21.2632
.7000	-0.0211	22.0507
.7250	-0.0199	22.8382

.7500	-.0186	23.6257	-.5844
.7750	-.0172	24.4133	-.5410
.8000	-.0157	25.2008	-.4957
.8250	-.0142	25.9883	-.4484
.8500	-.0126	26.7758	-.3985
.8750	-.0110	27.5634	-.3458
.9000	-.0093	28.3509	-.2914
.9250	-.0074	29.1384	-.2341
.9500	-.0053	29.9259	-.1676
.9750	-.0026	30.7135	-.0678
1.0000	0.0000	31.5010	0.0000

Y= -9.9110      Y= 1/8/2= -1.1386      CHORD= 33.9239

SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

.0295 .0106-.0013-.0102--.0173--.0285-.0331-.0333-.0412-.0450--.0488--.0526--.0568--.0617--.0682--.0785--.1089  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-0.0354	0.0000	-1.2019
.0250	-0.0362	.8481	-1.2274
.0500	-0.0369	1.6962	-1.2525
.0750	-0.0375	2.5443	-1.2727
.1000	-0.0379	3.3924	-1.2848
.1250	-0.0380	4.2405	-1.2901
.1500	-0.0381	5.0886	-1.2911
.1750	-0.0380	5.9367	-1.2887
.2000	-0.0378	6.7848	-1.2828
.2250	-0.0375	7.6329	-1.2736
.2500	-0.0372	8.4810	-1.2616
.2750	-0.0368	9.3291	-1.2471
.3000	-0.0363	10.1772	-1.2301
.3250	-0.0357	11.0253	-1.2110
.3500	-0.0351	11.8734	-1.1897
.3750	-0.0344	12.7215	-1.1665
.4000	-0.0336	13.5696	-1.1414
.4250	-0.0329	14.4176	-1.1146
.4500	-0.0320	15.2657	-1.0861
.4750	-0.0311	16.1138	-1.0559
.5000	-0.0302	16.9619	-1.0242
.5250	-0.0292	17.8100	-9909
.5500	-0.0282	18.6581	-9562
.5750	-0.0271	19.5062	-9200
.6000	-0.0260	20.3543	-8824
.6250	-0.0249	21.2024	-8433
.6500	-0.0237	22.0505	-8029
.6750	-0.0224	22.8986	-7610
.7000	-0.0212	23.7467	-7176
.7250	-0.0198	24.5948	-6727

.7500	.0185	25.4429	-.6262
.7750	-.0170	26.2910	-.5781
.8000	-.0156	27.1391	-.5284
.8250	-.0141	27.9872	-.4767
.8500	-.0125	28.8353	-.4224
.8750	-.0108	29.6834	-.3656
.9000	-.0091	30.5315	-.3070
.9250	-.0072	31.3796	-.2457
.9500	-.0052	32.2277	-.1756
.9750	-.0027	33.0758	-.0917
1.0000	0.0000	33.9239	0.0000

Y= -5.9499      Y/8/2= -.0832      CHORD= 36.3468

SLOPES,  $0Z/DX$ , AT SLOPE POINTS, FROM FRONT TO REAR

.0184 .0001-.0115-.0200-.0268-.0323-.0371-.0412-.0449-.0482-.0514-.0544-.0576-.0610--.0650--.0703--.0793--.1070  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
0.0000	-.0421	.0000	-1.5300
0.0250	-.0426	.9087	-1.5472
0.0500	-.0630	1.8173	-1.5640
0.0750	-.0434	2.7260	-1.5758
0.1000	-.0434	3.6347	-1.5791
0.1250	-.0433	4.5433	-1.5754
0.1500	-.0431	5.4520	-1.5671
0.1750	-.0428	6.3607	-1.5553
0.2000	-.0424	7.2694	-1.5399
0.2250	-.0619	8.1780	-1.5212
0.2500	-.0413	9.0867	-1.4996
0.2750	-.0406	9.9954	-1.4755
0.3000	-.0399	10.9040	-1.4489
0.3250	-.0391	11.8127	-1.4201
0.3500	-.0382	12.7214	-1.3892
0.3750	-.0373	13.6300	-1.3565
0.4000	-.0364	14.5387	-1.3219
0.4250	-.0354	15.4474	-1.2856
0.4500	-.0343	16.3560	-1.2478
0.4750	-.0332	17.2647	-1.2084
0.5000	-.0321	18.1734	-1.1676
0.5250	-.0310	19.0820	-1.1253
0.5500	-.0298	19.9907	-1.0817
0.5750	-.0285	20.8994	-1.0368
0.6000	-.0273	21.8081	-9907
0.6250	-.0260	22.7167	-9432
0.6500	-.0246	23.6254	-8946
0.6750	-.0232	24.5341	-8446
0.7000	-.0218	25.4427	-7934
0.7250	-.0204	26.3514	-7409

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.7500	-.0189
.7750	-.0174
.8000	-.0158
.8250	-.0142
.8500	-.0125
.8750	-.0108
.9000	-.0090
.9250	-.0072
.9500	-.0051
.9750	-.0027
1.0000	0.0000
	27.2601
	28.1687
	29.0774
	29.9861
	30.8947
	31.8034
	32.7121
	33.6208
	34.5294
	35.4381
	36.3468
	0.0000

Y- -1.9847      Y- 1/8/2\*      -0.0278      CHORD- 38.7722

## SLOPES, DZ/DX, AT SLOPE POINTS, FROM FRONT TO REAR

-0.0047-.0239-.0357-.0439-.0501-.0549-.0587-.0617-.0642-.0662-.0680-.0696-.0713-.0730-.0753-.0787-.0850-.1081  
CORRESPONDING X/C LOCATIONS FROM FRONT TO REAR

.0417 .0972 .1528 .2083 .2639 .3194 .3750 .4306 .4861 .5417 .5972 .6528 .7083 .7639 .8194 .8750 .9306 .9861

## LOCAL ELEVATION

X/C	Z/C	DELTA X	DELTA Z
.0000	-.0593	.0000	-2.2982
.0250	-.0592	.9693	-2.2942
.0500	-.0591	1.9386	-2.2897
.0750	-.0588	2.9079	-2.2796
.1000	-.0583	3.8772	-2.2600
.1250	-.0576	4.8465	-2.2327
.1500	-.0568	5.8158	-2.2005
.1750	-.0558	6.7851	-2.1645
.2000	-.0548	7.7544	-2.1248
.2250	-.0537	8.7237	-2.0817
.2500	-.0525	9.6930	-2.0357
.2750	-.0513	10.6623	-1.9873
.3000	-.0499	11.6316	-1.9366
.3250	-.0486	12.6009	-1.8839
.3500	-.0472	13.5703	-1.8294
.3750	-.0457	14.5396	-1.7733
.4000	-.0443	15.5089	-1.7158
.4250	-.0427	16.4782	-1.6569
.4500	-.0412	17.4475	-1.5967
.4750	-.0396	18.4168	-1.5355
.5000	-.0380	19.3861	-1.4733
.5250	-.0364	20.3554	-1.4101
.5500	-.0347	21.3247	-1.3460
.5750	-.0330	22.2940	-1.2811
.6000	-.0314	23.2633	-1.2155
.6250	-.0296	24.2326	-1.1491
.6500	-.0279	25.2019	-1.0821
.6750	-.0262	26.1712	-1.0143
.7000	-.0244	27.1405	-.9458
.7250	-.0226	28.1098	-.8766

•.7500	-•.0208	29.0791
.7750	-•.0190	30.0484
•.8000	-•.0171	31.0177
•.8250	-•.0153	31.9870
•.8500	-•.0133	32.9563
•.8750	-•.0114	33.9256
•.9000	-•.0094	34.8949
•.9250	-•.0074	35.8642
•.9500	-•.0052	36.8335
•.9750	-•.0027	37.8028
1.0000	0.0000	38.7722

•.7500	-•.0208	29.0791
.7750	-•.0190	30.0484
•.8000	-•.0171	31.0177
•.8250	-•.0153	31.9870
•.8500	-•.0133	32.9563
•.8750	-•.0114	33.9256
•.9000	-•.0094	34.8949
•.9250	-•.0074	35.8642
•.9500	-•.0052	36.8335
•.9750	-•.0027	37.8028
1.0000	0.0000	38.7722



APPENDIX B

DETAILS OF DATA PREPARATION FOR  
NUMERICALLY CONTROLLED MACHINING  
OF WING-WINGLET MODELS

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PROGRAM TX23Z(INPUT,OUTPUT,TAPE5,TAPE6=OUTPUT,TAPE10)

PROGRAM WRITTEN BY J KUHLMAN FOR PREPARING AIRFOIL COORDINATES, IN INCHES, FOR WING WITH WINGLET MODEL TO BE TESTED IN 7X10 FOOT TUNNEL. DESIGNED USING TN D-8090 DESIGN CODE BY LAMAR OR MODIFIED VERSION OF THIS CODE USING TREFFTZ PLANE WAKE MODEL OF CR-3154 BY KUHLMAN.

NAMELIST DATA INPUT INCLUDES CAMBERS (Z/C) FROM DESIGN CODES AT 21 SPAN STATIONS (PCTY HEREIN) AND 30 X/C STATIONS (PCTX HEREIN), AS WELL AS CHORD VALUES FOR WING, IN INCHES. THESE DATA SETS ARE STORED ON PERMANENT FILES ZOCJK AND ZCCOR.

TOC ARRAY IS SEMI-THICKNESS/C FOR NACA 64A008 BASIC THICKNESS FORM.

SINCH IS DISTANCE IN PLANE OF WING OR WINGLET MEASURED FROM ROOT.

LINEAR INTERPOLATION OR EXTRAPOLATION IN SPAN DIRECTION USING IUNI PERFORMED TO GENERATE ZS AT ROOT, TE BREAK, JCT OF WING AND WINGLET, LE BREAK ON WINGLET, AND WINGLET TIP.

THE Z/C TABLE IS SCALED BY THE LOCAL CHORD VALUE TIMES COSINE OF THE LOCAL DIHEDRAL ANGLE, SINCE WING AND WINGLET ARE TO BE MACHINED SEPARATELY.

THE YOB, CORD VALUES ARE THE INTERPOLATION STATIONS.

PCTX, YUP, YLO, ARE WRITTEN ON TAPE10 WHICH MAY THEN BE DISPOSED TO THE KEYPUNCH, TO OBTAIN PUNCHED INPUT CARDS FORMATTED FOR USE BY THE TX23 NUMERICAL CONTROL MACHINE.

INFOPLT PLOTS ZUP AND ZLO (UPPER AND LOWER SURFACE AIRFOIL COORDINATES) OVER CHORDS, VS PCTX.

DIMENSION CAMBER(30,2), PCTY(21), YOB(5), CHORD(21)  
DIMENSION PCTX(30), CORD(5)

GEOMETRY RESCALING PROGRAM

Listing of Computer Program for Rescaling of Geometry

```
DIMENSION ZTERP(30,6),PCTW(18),PCTT(3)
DIMENSION TOC(30)
DIMENSION CAM(21),ZUP(30),ZLO(30),ZUPC(30),ZLOC(30)
NAMELIST/DATA/CAMBER,CHORD
READ(5,DATA)
IF(EOF(5)) 10,20
10 WRITE(6,11)
11 FORMAT(/10X,13HNO DATA FOUND)
STOP
20 CONTINUE
REWIND 10
CALL PSEUDO
C CAMBER TABLES MUST BE INCREASING INDICES AS MOVE AFT AND AS MOVE
C OUTBOARD IN SPANWISE DIRECTION
TOC(1)=0.0
TOC(2)=1.353
TOC(3)=1.863
TOC(4)=2.245
TOC(5)=2.559
TOC(6)=2.830
TOC(7)=3.047
TOC(8)=3.233
TOC(9)=3.414
TOC(10)=3.556
TOC(11)=3.681
TOC(12)=3.781
TOC(13)=3.866
TOC(14)=3.929
TOC(15)=3.972
TOC(16)=3.990
TOC(17)=3.998
TOC(18)=3.972
TOC(19)=3.921
TOC(20)=3.757
TOC(21)=3.524
TOC(22)=3.234
TOC(23)=2.897
TOC(24)=2.521
TOC(25)=2.117
TOC(26)=1.698
TOC(27)=1.278
TOC(28)=0.858
```

```
TOC(29)=0.438
TOC(30)=0.018
RAD=4.*ATAN(1.)/180.
ANG1=6.*RAD
ANG2=77.5*RAD
WRITE(6,12) ANG1,ANG2
12 FORMAT(/20X,3F12.5/)
PCTY(1)=0.0278
PCTY(2)=0.0832
PCTY(3)=0.1386
PCTY(4)=0.1940
PCTY(5)=0.2494
PCTY(6)=0.3049
PCTY(7)=0.3603
PCTY(8)=0.4019
PCTY(9)=0.4435
PCTY(10)=0.4990
PCTY(11)=0.5544
PCTY(12)=0.6098
PCTY(13)=0.6652
PCTY(14)=0.7206
PCTY(15)=0.7760
PCTY(16)=0.8314
PCTY(17)=0.8868
PCTY(18)=0.9422
PCTY(19)=0.9737
PCTY(20)=0.9827
PCTY(21)=0.9940
YM=28.1459
YOB(1)=0.
YOB(2)=10.9197/YM
YOB(3)=27.2992/YM
YOB(4)=27.5109/YM
YOB(5)=1.0
CORD(1)=15.7426
CORD(2)=9.0633
CORD(3)=3.194
CORD(4)=1.73
CORD(5)=0.6916
DO 1 I=1,19
1 PCTX(I)=0.025*FLOAT(I-1)*100.
DO 2 I=20,30
```

```

PCTX(I)=0.05*FLOAT(I)-0.50
2 PCTX(I)=PCTX(I)*100.
ANG=ANG1
DO 30 I=1,21
IF(I.GE.19) ANG=ANG2
DO 22 J=1,30
CAMBER(J,I)=CAMBER(J,I)*COS(ANG)*CHORD(I)
THK=CHORD(I)*TOC(J)/100.
IF(J.EQ.1) GO TO 77
IF(THK.LT.0.01) THK=0.01
77 CONTINUE
C   ASK HOW THIN THE TRAILING EDGE CAN BE
ZUP(J)=CAMBER(J,I)+THK
ZLO(J)=ZUP(J)-2.*THK
ZUPC(J)=ZUP(J)/CHORD(I)+0.5
ZLOC(J)=ZLO(J)/CHORD(I)+0.5
22 CONTINUE
XI=FLOAT(I)
SINCH=28.1459*PCTY(I)/COS(ANG1)
IF(I.GE.19) SINCH=130.043125*PCTY(I)-126.131098
WRITE(10,120) XI,SINCH
120 FORMAT(7F10.6)
WRITE(10,120) (PCTX(L),L=1,30)
WRITE(10,120) (ZUP(L),L=1,30)
WRITE(10,120) (ZLO(L),L=1,30)
WRITE(6,129)
129 FORMAT(1H1)
WRITE(6,130) XI,SINCH
WRITE(6,833) CHORD(I),PCTY(I)
A33 FORMAT(20X,6HCHORD=,F10.6,6HY/B/2=,F10.6/)
130 FORMAT(20X,2HI=,F8.2,3X,8HS(INCH)=,F10.6/)
CALL INFOPLT(0,30,PCTX,1,ZUPC,1,0.,1.,0.,1.,0.0,3,
13HX/C,12,12HZ COS(PHI)/C,0)
CALL INFOPLT(0,30,PCTX,1,ZLOC,1,0.,1.,0.,1.,0.0,3,
13HX/C,12,12HZ COS(PHI)/C,0)
THET=0.
XL=5.5
YL=8.
HT=0.3
CALL NOTATE(XL,YL,HT,6HCHORD=,THET,6)
YL=7.
CALL NOTATE(XL,YL,HT,6HY/B/2=,THET,6)

```

```

XL=8.
YL=8.
CALL NUMBER(XL,YL,HT,CHORD(I),THET,3)
YL=7.
CALL NUMBER(XL,YL,HT,PCTY(I),THET,3)
CALL INFOPLT(1,0)
WRITE(6,135)
135 FORMAT(1/24X,1HI,6X,4HPCTX,6X,7HZUP(IN),4X,7HZLO(IN)/)
      WRITE(6,140) (L,PCTX(L),ZUP(L),ZLO(L),L=1,30)
140 FORMAT(21X,I5+3F11.6)
30 CONTINUE
IPT=-1
IORDER=1
DO 4 J=1,3
DO 3 I=1,30
DO 14 L=1,18
PCTW(L)=PCTY(L)
14 CAM(L)=CAMBER(I,L)
X0=Y0B(J)
IPT=-1
CALL IUNI(18,18,PCTW,1,CAM,IORDER,X0,Z0,IPT,IERR)
WRITE(6,100) IERR
ZTERP(I,J)=Z0
3 CONTINUE
4 CONTINUE
DO 5 I=1,3
WRITE(6,101) Y0B(I)
WRITE(6,111) (PCTX(J),ZTERP(J,I),J=1,30)
5 CONTINUE
DO 6 I=1,3
WRITE(10,110) (ZTERP(J,I),J=1,30)
6 CONTINUE
DO 8 J=3,5
J1=J+1
DO 7 I=1,30
DO 31 L=1,3
LP=18+L
PCTT(L)=PCTY(LP)
31 CAM(L)=CAMBER(I,LP)
X0=Y0B(J)
IPT=-1
IORDER=1

```

```

CALL IUNI(1B,3,PCTT,1,CAM,IORDER,X0,Z0,IPT,IERR)
WRITE(6,100) IERR
ZTERP(I,J1)=Z0
7 CONTINUE
8 CONTINUE
DO 9 J=3,5
J1=J+1
WRITE(6,101) YOB(J)
WRITE(6,111) (PCTX(I),ZTERP(I,J1),I=1,30)
9 CONTINUE
C ADD SCALING CODING HERE TO COMPUTE ZUP AND ZLO INTERP
DO 909 J=1,3
DO 908 I=1,30
THK=CORD(J)*TOC(I)/100.
IF(I.EQ.1) GO TO 967
IF(THK.LT.0.01) THK=0.01
967 CONTINUE
ZUP(I)=ZTERP(I,J)+THK
ZLO(I)=ZUP(I)-2.*THK
908 CONTINUE
WRITE(10,120) (PCTX(L),L=1,30)
WRITE(10,120) (ZUP(L),L=1,30)
WRITE(10,120) (ZLO(L),L=1,30)
WRITE(6,129)
WRITE(6,920)
WRITE(6,833) CORD(J),YOB(J)
901 FORMAT(120X,6HY/8/2=,F15.5/)
WRITE(6,135)
WRITE(6,140) (L,PCTX(L),ZUP(L),ZLO(L),L=1,30)
920 FORMAT(125X,25HINTERP ZS ON WING (INCH) /)
909 CONTINUE
DO 919 J=3,5
J1=J+1
DO 918 I=1,30
THK=CORD(J)*TOC(I)/100.
IF(I.EQ.1) GO TO 977
IF(THK.LT.0.01) THK=0.01
977 CONTINUE
ZUP(I)=ZTERP(I,J1)+THK
ZLO(I)=ZUP(I)-2.*THK
918 CONTINUE
WRITE(10,120) (PCTX(L),L=1,30)

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```
      WRITE(10,120) (ZUP(L),L=1,30)
      WRITE(10,120) (ZLO(L),L=1,30)
      WRITE(6,129)
      WRITE(6,921)
      WRITE(6,833) CORD(J),YOB(J)
      WRITE(6,135)
      WRITE(6,140) (L,PCTX(L),ZUP(L),ZLO(L),L=1,30)
921 FORMAT(1/25X,28HINTERP ZS ON WINGLET (INCH) /)
919 CONTINUE
      END FILE 10
      REWIND 10
100 FORMAT(20X,2I10)
101 FORMAT(1/7H Y/B/2=,F15.5//26X,3HXC,10X,8HINTERP Z//)
111 FORMAT(20X,2F15.5)
110 FORMAT(10F7.5)
      END
```

I= 1.00 S(INCH)= .786766

CHORD= 15.264600Y/R/2= .027800

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.851330	.851330
2	2.500000	1.056410	.643350
3	5.000000	1.132631	.563872
4	7.500000	1.187220	.501839
5	10.000000	1.227910	.446668
6	12.500000	1.259126	.395150
7	15.000000	1.280283	.350058
8	17.500000	1.295299	.308289
9	20.000000	1.308178	.265911
10	22.500000	1.313844	.228226
11	25.000000	1.315845	.192065
12	27.500000	1.313112	.158803
13	30.000000	1.307265	.127006
14	32.500000	1.297313	.097821
15	35.000000	1.283640	.071020
16	37.500000	1.265551	.047436
17	40.000000	1.245394	.024837
18	42.500000	1.219557	.006937
19	45.000000	1.189457	-.007593
20	50.000000	1.118607	-.028375
21	55.000000	1.035852	-.039997
22	60.000000	.943213	-.044101
23	65.000000	.842337	-.042094
24	70.000000	.734507	-.035134
25	75.000000	.621346	-.024958
26	80.000000	.504767	-.013619
27	85.000000	.386381	-.003782
28	90.000000	.266029	.004088
29	95.000000	.141446	.007728
30	100.000000	.010000	-.010000

Output of Computer Program for Rescaling of Wing-Winglet Geometry

I= 2.00 S(INCH)= 2.354638

CHORD= 14.309800Y/B/2= .083200

I	PCTX	ZUP(IN)	ZLO(IN)
1	0.000000	.564536	.564536
2	2.500000	.764623	.377400
3	5.000000	.843919	.310736
4	7.500000	.903030	.260520
5	10.000000	.949259	.216884
6	12.500000	.986706	.176772
7	15.000000	1.014749	.142710
8	17.500000	1.037020	.111748
9	20.000000	1.057253	.080180
10	22.500000	1.070669	.052956
11	25.000000	1.080571	.027083
12	27.500000	1.085937	.003830
13	30.000000	1.088273	-.018161
14	32.500000	1.086636	-.037828
15	35.000000	1.081373	-.055397
16	37.500000	1.071824	-.070098
17	40.000000	1.060180	-.084031
18	42.500000	1.043046	-.093725
19	45.000000	1.021743	-.100431
20	50.000000	.968609	-.106629
21	55.000000	.903546	-.105009
22	60.000000	.828402	-.097156
23	65.000000	.744680	-.084430
24	70.000000	.653542	-.067958
25	75.000000	.556460	-.049417
26	80.000000	.455181	-.030780
27	85.000000	.351105	-.014653
28	90.000000	.243085	-.001571
29	95.000000	.131297	.005943
30	100.000000	.010000	-.010000

I= 3.00 S(INCH)= 3.922510  
 CHORD= 13.355900Y/R/2= .138600

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.443664	.443664
2	2.500000	.633925	.272514
3	5.000000	.711442	.213802
4	7.500000	.770064	.170384
5	10.000000	.816571	.133016
6	12.500000	.854802	.098858
7	15.000000	.884207	.070298
8	17.500000	.908179	.044587
9	20.000000	.930201	.018261
10	22.500000	.945807	-.004065
11	25.000000	.958079	-.025182
12	27.500000	.966064	-.043909
13	30.000000	.971162	-.061517
14	32.500000	.972441	-.077016
15	35.000000	.970372	-.090620
16	37.500000	.964187	-.101614
17	40.000000	.955978	-.111960
18	42.500000	.942572	-.118421
19	45.000000	.925202	-.122168
20	50.000000	.896400	-.123162
21	55.000000	.824135	-.117189
22	60.000000	.755110	-.105750
23	65.000000	.683704	-.090137
24	70.000000	.601475	-.071430
25	75.000000	.514265	-.051224
26	80.000000	.422167	-.031399
27	85.000000	.326417	-.014460
28	90.000000	.222223	-.000964
29	95.000000	.123530	.006532
30	100.000000	.016666	-.116000

I = 4.00 S(INCH) = 5.490381

CHORD = 12.402000 Y/B/2 = .194000

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.368965	.368965
2	2.500000	.548121	.212523
3	5.000000	.622578	.160480
4	7.500000	.679399	.122550
5	10.000000	.724820	.090085
6	12.500000	.762431	.060478
7	15.000000	.791767	.035989
8	17.500000	.815995	.014082
9	20.000000	.838346	-.008462
10	22.500000	.854674	-.027357
11	25.000000	.867846	-.045189
12	27.500000	.876980	-.060859
13	30.000000	.883378	-.075545
14	32.500000	.886220	-.088330
15	35.000000	.885804	-.099411
16	37.500000	.881557	-.108123
17	40.000000	.875374	-.116290
18	42.500000	.864309	-.120906
19	45.000000	.849504	-.123060
20	50.000000	.810377	-.121509
21	55.000000	.760360	-.113733
22	60.000000	.701026	-.101135
23	65.000000	.633640	-.084932
24	70.000000	.559168	-.066141
25	75.000000	.478834	-.046267
26	80.000000	.394095	-.027077
27	85.000000	.306043	-.010952
28	90.000000	.214376	.001557
29	95.000000	.116554	.007913
30	100.000000	.010000	-.010000

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I= 5.00 S(INCH)= 7.058253

CHORD= 11.448100Y/B/2= .249400

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.316432	.316432
2	2.500000	.483867	.174082
3	5.000000	.554648	.128091
4	7.500000	.609044	.095024
5	10.000000	.652741	.066827
6	12.500000	.689084	.041122
7	15.000000	.717696	.020048
8	17.500000	.741517	.001283
9	20.000000	.763530	-.018147
10	22.500000	.779909	-.034280
11	25.000000	.793310	-.049499
12	27.500000	.802921	-.062784
13	30.000000	.809947	-.075220
14	32.500000	.813632	-.085959
15	35.000000	.814255	-.095183
16	37.500000	.811283	-.102275
17	40.000000	.806470	-.108920
18	42.500000	.797096	-.112341
19	45.000000	.784215	-.113545
20	50.000000	.749500	-.110710
21	55.000000	.704509	-.102353
22	60.000000	.650687	-.089776
23	65.000000	.589195	-.074108
24	70.000000	.520913	-.056300
25	75.000000	.446955	-.037758
26	80.000000	.368651	-.020126
27	85.000000	.286967	-.005647
28	90.000000	.201597	.005147
29	95.000000	.110036	.009750
30	100.000000	.010000	-.010000

I= 6.00 S(INCH)= 8.628955

CHORD= 10.494200Y/B/2= .304900

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.278829	.278829
2	2.500000	.434163	.150190
3	5.000000	.500886	.109872
4	7.500000	.552476	.081287
5	10.000000	.594067	.056974
6	12.500000	.628757	.034785
7	15.000000	.656257	.016740
8	17.500000	.679282	.000727
9	20.000000	.700565	-.015979
10	22.500000	.716602	-.029745
11	25.000000	.729836	-.042747
12	27.500000	.739527	-.054045
13	30.000000	.746782	-.064630
14	32.500000	.750910	-.073724
15	35.000000	.752167	-.081492
16	37.500000	.750069	-.087368
17	40.000000	.746221	-.092895
18	42.500000	.738131	-.095528
19	45.000000	.726767	-.096188
20	50.000000	.695652	-.092883
21	55.000000	.654876	-.084755
22	60.000000	.605762	-.073003
23	65.000000	.549368	-.058666
24	70.000000	.486498	-.042620
25	75.000000	.418159	-.026165
26	80.000000	.345564	-.010819
27	85.000000	.269558	.001326
28	90.000000	.189844	.009764
29	95.000000	.113972	.012043
30	100.000000	.010000	-.010000

I= 7.00 S(INCH)= 10.196827

CHORD= 9.540270Y/B/2= .360300

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.262052	.262052
2	2.500000	.405002	.146842
3	5.000000	.467384	.111914
4	7.500000	.515886	.087528
5	10.000000	.555088	.066817
6	12.500000	.587837	.047858
7	15.000000	.613931	.032547
8	17.500000	.635856	.018982
9	20.000000	.656093	.004683
10	22.500000	.671458	-.007046
11	25.000000	.684178	-.018177
12	27.500000	.693585	-.027851
13	30.000000	.700687	-.036967
14	32.500000	.704857	-.044818
15	35.000000	.706329	-.051550
16	37.500000	.704663	-.056650
17	40.000000	.701321	-.061519
18	42.500000	.694038	-.063841
19	45.000000	.683692	-.064456
20	50.000000	.655123	-.061733
21	55.000000	.617434	-.054964
22	60.000000	.571826	-.045238
23	65.000000	.519262	-.033501
24	70.000000	.460469	-.020551
25	75.000000	.396358	-.007577
26	80.000000	.328029	.004041
27	85.000000	.256228	.012379
28	90.000000	.180691	.016980
29	95.000000	.099089	.015516
30	100.000000	.010000	-.010000

I= 8.00 S(INCH)= 11.374146

CHORD= 8.922740Y/R/2= .401900

I	PCTX	ZUP(IN)	ZLO(IN)
1	0.000000	.253355	.253355
2	2.500000	.388587	.147138
3	5.000000	.448461	.116000
4	7.500000	.495273	.094642
5	10.000000	.533250	.076584
6	12.500000	.565066	.060039
7	15.000000	.590561	.046809
8	17.500000	.612069	.035124
9	20.000000	.631907	.022663
10	22.500000	.647100	.012515
11	25.000000	.659732	.002840
12	27.500000	.669183	-.005554
13	30.000000	.676396	-.013510
14	32.500000	.680785	-.020364
15	35.000000	.682569	-.026254
16	37.500000	.681338	-.030696
17	40.000000	.678460	-.035002
18	42.500000	.671815	-.037007
19	45.000000	.662227	-.037494
20	50.000000	.635443	-.035011
21	55.000000	.599810	-.029064
22	60.000000	.556449	-.020673
23	65.000000	.506255	-.010729
24	70.000000	.449901	.000016
25	75.000000	.388224	.010435
26	80.000000	.322249	.019233
27	85.000000	.252601	.024536
28	90.000000	.179044	.025930
29	95.000000	.099073	.020909
30	100.000000	.010000	-.010000

I= 9.00 ' S(INCH)= 12.551465

CHORD= 8.502760Y/B/2= .443500

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.193940	.193940
2	2.500000	.323953	.093868
3	5.000000	.382153	.065340
4	7.500000	.427888	.046114
5	10.000000	.465175	.030004
6	12.500000	.496577	.015321
7	15.000000	.521960	.003802
8	17.500000	.543554	-.006234
9	20.000000	.563570	-.016999
10	22.500000	.579172	-.025544
11	25.000000	.592351	-.033622
12	27.500000	.602517	-.040462
13	30.000000	.610569	-.046864
14	32.500000	.615952	-.052195
15	35.000000	.618873	-.056586
16	37.500000	.618943	-.059577
17	40.000000	.617465	-.062415
18	42.500000	.612420	-.063039
19	45.000000	.604592	-.062195
20	50.000000	.581749	-.057149
21	55.000000	.550553	-.048722
22	60.000000	.512063	-.037895
23	65.000000	.467116	-.025534
24	70.000000	.416332	-.012377
25	75.000000	.360470	.000463
26	80.000000	.300453	.011699
27	85.000000	.236758	.019428
28	90.000000	.168994	.023087
29	95.000000	.094360	.019876
30	100.000000	.010000	-.010000

I= 10.00 S(INCH)= 14.122167

CHORD= 7.943940Y/B/2= .499000

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.151121	.151121
2	2.500000	.273935	.058972
3	5.000000	.329651	.033660
4	7.500000	.373674	.016991
5	10.000000	.409726	.003156
6	12.500000	.440219	-.009408
7	15.000000	.465051	-.019053
8	17.500000	.486319	-.027337
9	20.000000	.506085	-.036327
10	22.500000	.521704	-.043269
11	25.000000	.535038	-.049795
12	27.500000	.545540	-.055181
13	30.000000	.554051	-.060175
14	32.500000	.560051	-.064184
15	35.000000	.563737	-.067330
16	37.500000	.564745	-.069182
17	40.000000	.564291	-.070906
18	42.500000	.560491	-.070576
19	45.000000	.554075	-.068889
20	50.000000	.534483	-.062424
21	55.000000	.507018	-.052871
22	60.000000	.472657	-.041157
23	65.000000	.432167	-.028105
24	70.000000	.386102	-.014431
25	75.000000	.335140	-.001206
26	80.000000	.280105	.010329
27	85.000000	.221383	.010336
28	90.000000	.158563	.022245
29	95.000000	.088912	.019323
30	100.000000	.010000	-.010000

I= 11.00 S(INCH)= 15.690039

CHORD= 7.385130Y/R/2= .554400

I	PCTX	ZUP(IN)	ZLO(IN)
1	0.000000	.121660	.121660
2	2.500000	.237017	.037176
3	5.000000	.289993	.014823
4	7.500000	.332045	.000452
5	10.000000	.366599	-.011372
6	12.500000	.395911	-.022087
7	15.000000	.419918	-.030132
8	17.500000	.440575	-.036948
9	20.000000	.459801	-.044456
10	22.500000	.475136	-.050094
11	25.000000	.488318	-.055376
12	27.500000	.498838	-.059626
13	30.000000	.507480	-.063538
14	32.500000	.513762	-.066561
15	35.000000	.517868	-.068807
16	37.500000	.519459	-.069874
17	40.000000	.519667	-.070848
18	42.500000	.516739	-.069936
19	45.000000	.511355	-.067786
20	50.000000	.494228	-.060691
21	55.000000	.469677	-.050827
22	60.000000	.438607	-.039064
23	65.000000	.401718	-.026176
24	70.000000	.359520	-.012838
25	75.000000	.312626	-.000061
26	80.000000	.261790	.010991
27	85.000000	.207340	.018576
28	90.000000	.148875	.022146
29	95.000000	.083752	.019059
30	100.000000	.010000	-.010000

I= 12.00 S(INCH)= 17.257910

CHORD= 6.826300Y/B/2= .609800

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.097412	.097412
2	2.500000	.205119	.020399
3	5.000000	.255160	.000812
4	7.500000	.295052	-.011449
5	10.000000	.327926	-.021444
6	12.500000	.355883	-.030486
7	15.000000	.378889	-.037106
8	17.500000	.398763	-.042626
9	20.000000	.417277	-.048823
10	22.500000	.432159	-.053327
11	25.000000	.445018	-.057534
12	27.500000	.455388	-.060817
13	30.000000	.463994	-.063815
14	32.500000	.470391	-.066020
15	35.000000	.474750	-.067532
16	37.500000	.476758	-.067981
17	40.000000	.477463	-.068368
18	42.500000	.475243	-.067038
19	45.000000	.470729	-.064590
20	50.000000	.455746	-.057182
21	55.000000	.433801	-.047316
22	60.000000	.405726	-.035799
23	65.000000	.372165	-.023351
24	70.000000	.333583	-.010599
25	75.000000	.290538	.001512
26	80.000000	.243717	.011896
27	85.000000	.193396	.018916
28	90.000000	.139186	.022046
29	95.000000	.078542	.018743
30	100.000000	.010000	-.010000

I= 13.00 S(INCH)= 18.825782

CHORD= 6.267480Y/B/2= .665200

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.076455	.076455
2	2.500000	.176343	.006745
3	5.000000	.223281	-.010245
4	7.500000	.260851	-.020559
5	10.000000	.291892	-.028877
6	12.500000	.318349	-.036390
7	15.000000	.340217	-.041723
8	17.500000	.359174	-.046081
9	20.000000	.376845	-.051098
10	22.500000	.391149	-.054594
11	25.000000	.403563	-.057849
12	27.500000	.413662	-.060284
13	30.000000	.422115	-.062486
14	32.500000	.428513	-.063986
15	35.000000	.433013	-.064875
16	37.500000	.435331	-.064814
17	40.000000	.436427	-.064721
18	42.500000	.434814	-.063075
19	45.000000	.431070	-.060426
20	50.000000	.418044	-.052895
21	55.000000	.398530	-.043202
22	60.000000	.373291	-.032090
23	65.000000	.342916	-.020222
24	70.000000	.307826	-.008180
25	75.000000	.268525	.003160
26	80.000000	.225635	.012792
27	85.000000	.179383	.019186
28	90.000000	.129392	.021842
29	95.000000	.073232	.018329
30	100.000000	.010000	-.010000

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I= 14.00 S(INCH)= 20.393654

CHORD= 5.708670Y/B/2= .720600

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.055906	.055906
2	2.500000	.147816	-.006660
3	5.000000	.191494	-.021211
4	7.500000	.226594	-.029725
5	10.000000	.255672	-.036498
6	12.500000	.280511	-.042599
7	15.000000	.301132	-.046754
8	17.500000	.319070	-.050052
9	20.000000	.335807	-.053981
10	22.500000	.349446	-.056555
11	25.000000	.361337	-.058935
12	27.500000	.371096	-.060594
13	30.000000	.379331	-.062064
14	32.500000	.385672	-.062916
15	35.000000	.390262	-.063235
16	37.500000	.392843	-.062708
17	40.000000	.394291	-.062174
18	42.500000	.393252	-.060245
19	45.000000	.390251	-.057423
20	50.000000	.379145	-.049804
21	55.000000	.362050	-.040297
22	60.000000	.339659	-.029577
23	65.000000	.312506	-.018255
24	70.000000	.280968	-.006863
25	75.000000	.245498	.003793
26	80.000000	.206653	.012786
27	85.000000	.164613	.018700
28	90.000000	.119021	.021060
29	95.000000	.067574	.017566
30	100.000000	.010000	-.010000

I= 15.00 S(INCH)= 21.961526

CHORD= 5.149850Y/B/2= .776000

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.038585	.038585
2	2.500000	.122350	-.017005
3	5.000000	.162600	-.029283
4	7.500000	.195071	-.036158
5	10.000000	.222039	-.041531
6	12.500000	.245126	-.046356
7	15.000000	.264372	-.049460
8	17.500000	.281169	-.051821
9	20.000000	.296853	-.054779
10	22.500000	.309715	-.056543
11	25.000000	.320975	-.058157
12	27.500000	.330288	-.059144
13	30.000000	.338205	-.059982
14	32.500000	.344391	-.060285
15	35.000000	.348977	-.060127
16	37.500000	.351730	-.059228
17	40.000000	.353440	-.058342
18	42.500000	.352886	-.056218
19	45.000000	.350544	-.053307
20	50.000000	.341195	-.045765
21	55.000000	.326364	-.036598
22	60.000000	.306673	-.026419
23	65.000000	.282601	-.015781
24	70.000000	.254485	-.005170
25	75.000000	.222723	.004679
26	80.000000	.187812	.012923
27	85.000000	.149891	.018261
28	90.000000	.108620	.020249
29	95.000000	.061848	.016735
30	100.000000	.010000	-.010000

I= 16.00 S(INCH)= 23.529398

CHORD= 4.591040Y/B/2= .831400

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.023149	.023149
2	2.500000	.098591	-.025642
3	5.000000	.135238	-.035824
4	7.500000	.164914	-.041224
5	10.000000	.189626	-.045343
6	12.500000	.210831	-.049022
7	15.000000	.228580	-.051198
8	17.500000	.244123	-.052733
9	20.000000	.258650	-.054826
10	22.500000	.270638	-.055877
11	25.000000	.281176	-.056816
12	27.500000	.289960	-.057215
13	30.000000	.297479	-.057500
14	32.500000	.303436	-.057328
15	35.000000	.307949	-.056763
16	37.500000	.310809	-.055556
17	40.000000	.312722	-.054377
18	42.500000	.312599	-.052114
19	45.000000	.310862	-.049168
20	50.000000	.303176	-.041795
21	55.000000	.290527	-.033050
22	60.000000	.273467	-.023481
23	65.000000	.252420	-.013585
24	70.000000	.227681	-.003800
25	75.000000	.199597	.005213
26	80.000000	.168605	.012694
27	85.000000	.134811	.017464
28	90.000000	.097901	.019118
29	95.000000	.055893	.015676
30	100.000000	.010000	-.010000

I= 17.00 S(INCH)= 25.097270

CHORD= 4.032220Y/B/2= .886800

I	PCTX	ZUP(IN)	ZLO(IN)
1	0.000000	.013899	.013899
2	2.500000	.080797	-.028315
3	5.000000	.113618	-.036622
4	7.500000	.140291	-.040756
5	10.000000	.162559	-.043811
6	12.500000	.181707	-.046517
7	15.000000	.197796	-.047927
8	17.500000	.211927	-.048797
9	20.000000	.225143	-.050177
10	22.500000	.236108	-.050664
11	25.000000	.245780	-.051072
12	27.500000	.253891	-.051026
13	30.000000	.260871	-.050900
14	32.500000	.266460	-.050392
15	35.000000	.270758	-.049562
16	37.500000	.273584	-.048188
17	40.000000	.275555	-.046861
18	42.500000	.275715	-.044605
19	45.000000	.274434	-.041772
20	50.000000	.268101	-.034880
21	55.000000	.257307	-.026884
22	60.000000	.242535	-.018269
23	65.000000	.224153	-.009474
24	70.000000	.202422	-.000883
25	75.000000	.177648	.006923
26	80.000000	.150216	.013282
27	85.000000	.120218	.017155
28	90.000000	.087383	.018190
29	95.000000	.049940	.014618
30	100.000000	.010000	-.010000

I= 18.00 S(INCH)= 26.665141

CHORD= 3.473410Y/B/2= .942200

I	PCTX	ZUP(IN)	ZLO(IN)
1	0.000000	.022580	.022580
2	2.500000	.080541	-.013450
3	5.000000	.109147	-.020273
4	7.500000	.132434	-.023522
5	10.000000	.151886	-.025883
6	12.500000	.168607	-.027988
7	15.000000	.182650	-.029019
8	17.500000	.194957	-.029633
9	20.000000	.206422	-.030743
10	22.500000	.215884	-.031145
11	25.000000	.224166	-.031546
12	27.500000	.231032	-.031627
13	30.000000	.236852	-.031712
14	32.500000	.241400	-.031540
15	35.000000	.244765	-.031162
16	37.500000	.246793	-.030385
17	40.000000	.248022	-.029712
18	42.500000	.247631	-.028297
19	45.000000	.245948	-.026437
20	50.000000	.239205	-.021787
21	55.000000	.228506	-.016300
22	60.000000	.214335	-.010325
23	65.000000	.197082	-.004168
24	70.000000	.177042	.001912
25	75.000000	.154548	.007484
26	80.000000	.129994	.012037
27	85.000000	.103511	.014731
28	90.000000	.074902	.015299
29	95.000000	.042669	.012242
30	100.000000	.010000	-.010000

I= 19.00 S(INCH)= .491893

CHORD= 2.461800Y/R/2= .973700

I	PCTX	ZUP(IN)	ZLO(IN)
1	0.000000	-.031850	-.031850
2	2.500000	.014890	-.051726
3	5.000000	.040762	-.050964
4	7.500000	.062146	-.048389
5	10.000000	.079614	-.046381
6	12.500000	.094184	-.045154
7	15.000000	.106296	-.043726
8	17.500000	.116772	-.042408
9	20.000000	.126269	-.041822
10	22.500000	.134015	-.041068
11	25.000000	.140670	-.040568
12	27.500000	.146129	-.040032
13	30.000000	.150697	-.039649
14	32.500000	.154250	-.039199
15	35.000000	.156884	-.038682
16	37.500000	.158522	-.037930
17	40.000000	.159571	-.037275
18	42.500000	.159472	-.036094
19	45.000000	.158474	-.034580
20	50.000000	.154195	-.030785
21	55.000000	.147319	-.026188
22	60.000000	.138233	-.020996
23	65.000000	.127227	-.015410
24	70.000000	.114498	-.009626
25	75.000000	.100252	-.003981
26	80.000000	.084717	.001114
27	85.000000	.067909	.004985
28	90.000000	.049601	.007357
29	95.000000	.028627	.007061
30	100.000000	.010000	-.010000

I= 20.00 S(INCH)= 1.662281

CHORD= 1.488240Y/B/2= .982700

I	PCTX	ZUP(IN)	ZLO(IN)
1	0.000000	-.058118	-.058118
2	2.500000	-.030079	-.070351
3	5.000000	-.014629	-.070081
4	7.500000	-.001587	-.068409
5	10.000000	.009596	-.066573
6	12.500000	.019431	-.064804
7	15.000000	.028010	-.062684
8	17.500000	.035763	-.060466
9	20.000000	.043077	-.058540
10	22.500000	.049464	-.056380
11	25.000000	.055287	-.054277
12	27.500000	.060456	-.052084
13	30.000000	.065135	-.049935
14	32.500000	.069231	-.047715
15	35.000000	.072784	-.045442
16	37.500000	.075731	-.043031
17	40.000000	.078301	-.040699
18	42.500000	.080143	-.038083
19	45.000000	.081395	-.035312
20	50.000000	.082337	-.029489
21	55.000000	.081409	-.023483
22	60.000000	.078787	-.017472
23	65.000000	.074604	-.011625
24	70.000000	.068944	-.006093
25	75.000000	.061901	-.001111
26	80.000000	.053597	.003056
27	85.000000	.043998	.005959
28	90.000000	.032962	.007423
29	95.000000	.023073	.003073
30	100.000000	.010000	-.010000

I= 21.00 S(INCH)= 3.131768

CHORD= .969010Y/B/2= .994000

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	-.048322	-.048322
2	2.500000	-.030443	-.056664
3	5.000000	-.020756	-.056862
4	7.500000	-.012596	-.056105
5	10.000000	-.005577	-.055171
6	12.500000	.000625	-.054221
7	15.000000	.006049	-.053003
8	17.500000	.010968	-.051688
9	20.000000	.015636	-.050528
10	22.500000	.019733	-.049183
11	25.000000	.023493	-.047846
12	27.500000	.026856	-.046420
13	30.000000	.029928	-.044996
14	32.500000	.032647	-.043498
15	35.000000	.035040	-.041938
16	37.500000	.037065	-.040262
17	40.000000	.038870	-.038612
18	42.500000	.040228	-.036750
19	45.000000	.041228	-.034762
20	50.000000	.042289	-.030522
21	55.000000	.042238	-.026058
22	60.000000	.041191	-.021485
23	65.000000	.039235	-.016909
24	70.000000	.036429	-.012428
25	75.000000	.032838	-.008190
26	80.000000	.028545	-.004363
27	85.000000	.023545	-.001223
28	90.000000	.019442	-.000558
29	95.000000	.016416	-.003584
30	100.000000	.010000	-.010000

## INTERP ZS ON WING (INCH)

CHORD= 15.742600Y/B/2= 0.000000

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.995245	.995245
2	2.500000	1.202815	.776821
3	5.000000	1.277488	.690918
4	7.500000	1.329803	.622960
5	10.000000	1.367710	.562004
6	12.500000	1.395796	.504764
7	15.000000	1.413495	.454141
8	17.500000	1.424868	.406951
9	20.000000	1.434055	.359150
10	22.500000	1.435831	.316217
11	25.000000	1.433866	.274895
12	27.500000	1.427067	.236611
13	30.000000	1.417113	.199895
14	32.500000	1.402988	.165935
15	35.000000	1.385094	.134502
16	37.500000	1.362719	.106459
17	40.000000	1.338290	.079512
18	42.500000	1.308086	.057494
19	45.000000	1.273572	.039037
20	50.000000	1.193835	.010936
21	55.000000	1.102205	-.007333
22	60.000000	1.000790	-.017442
23	65.000000	.891310	-.020817
24	70.000000	.775107	-.018635
25	75.000000	.653882	-.012660
26	80.000000	.529630	-.004989
27	85.000000	.404069	.001688
28	90.000000	.277081	.006938
29	95.000000	.146534	.008629
30	100.000000	.010000	-.010000

## INTERP ZS ON WING (INCH)

CHORD= 9.063300Y/8/2= .387968

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.256268	.256268
2	2.500000	.393188	.147935
3	5.000000	.453564	.115866
4	7.500000	.500689	.093747
5	10.000000	.538868	.075008
6	12.500000	.570817	.057834
7	15.000000	.596369	.044051
8	17.500000	.617893	.031860
9	20.000000	.637745	.018903
10	22.500000	.652902	.008320
11	25.000000	.665480	-.001760
12	27.500000	.674850	-.010516
13	30.000000	.681970	-.018805
14	32.500000	.686243	-.025951
15	35.000000	.687894	-.032094
16	37.500000	.686506	-.036745
17	40.000000	.683467	-.041234
18	42.500000	.676626	-.043362
19	45.000000	.666818	-.043926
20	50.000000	.639545	-.041471
21	55.000000	.603378	-.035404
22	60.000000	.559457	-.026758
23	65.000000	.508692	-.016436
24	70.000000	.451770	-.005202
25	75.000000	.389545	.005805
26	80.000000	.323060	.015270
27	85.000000	.252969	.021311
28	90.000000	.179027	.023501
29	95.000000	.098788	.019393
30	100.000000	.010000	-.010000

INTERP ZS ON WING (INCH)

CHORD= 3.194000Y/B/2= .969917

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	.026923	.026923
2	2.500000	.080415	-.006014
3	5.000000	.106913	-.012096
4	7.500000	.128507	-.014904
5	10.000000	.146550	-.016919
6	12.500000	.162058	-.018722
7	15.000000	.175078	-.019565
8	17.500000	.186473	-.020051
9	20.000000	.197061	-.021025
10	22.500000	.205772	-.021385
11	25.000000	.213359	-.021784
12	27.500000	.219603	-.021928
13	30.000000	.224842	-.022118
14	32.500000	.228869	-.022115
15	35.000000	.231768	-.021964
16	37.500000	.233397	-.021484
17	40.000000	.234253	-.021139
18	42.500000	.233587	-.020144
19	45.000000	.231703	-.018771
20	50.000000	.224755	-.015242
21	55.000000	.214103	-.011010
22	60.000000	.200232	-.006356
23	65.000000	.183542	-.001518
24	70.000000	.164348	.003306
25	75.000000	.142994	.007760
26	80.000000	.119879	.011411
27	85.000000	.095154	.013516
28	90.000000	.068660	.013851
29	95.000000	.039033	.011053
30	100.000000	.010000	-.010000

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## INTERP ZS ON WINGLET (INCH)

CHORD= 3.194000Y/B/2= .969917

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	-.020809	-.020809
2	2.500000	.038160	-.048269
3	5.000000	.070060	-.048948
4	7.500000	.096184	-.047227
5	10.000000	.117308	-.046161
6	12.500000	.134743	-.046037
7	15.000000	.149040	-.045602
8	17.500000	.161262	-.045262
9	20.000000	.172261	-.045825
10	22.500000	.181038	-.046119
11	25.000000	.188445	-.046697
12	27.500000	.194350	-.047180
13	30.000000	.199146	-.047814
14	32.500000	.202673	-.048311
15	35.000000	.205060	-.048671
16	37.500000	.206207	-.048675
17	40.000000	.206642	-.048750
18	42.500000	.205643	-.048088
19	45.000000	.203535	-.046938
20	50.000000	.196531	-.043466
21	55.000000	.186404	-.038709
22	60.000000	.173664	-.032924
23	65.000000	.158701	-.026359
24	70.000000	.141787	-.019255
25	75.000000	.123208	-.012026
26	80.000000	.103281	-.005188
27	85.000000	.082087	.000448
28	90.000000	.059366	.004557
29	95.000000	.033839	.005859
30	100.000000	.010000	-.010000

## INTERP ZS ON WINGLET (INCH)

CHORD= 1.730000Y/8/2= .977439

I	PCTX	ZUP (IN)	ZLO (IN)
1	0.000000	-.042763	-.042763
2	2.500000	-.008221	-.055035
3	5.000000	.011652	-.052808
4	7.500000	.028320	-.049357
5	10.000000	.042149	-.046393
6	12.500000	.053865	-.044053
7	15.000000	.063798	-.041628
8	17.500000	.072535	-.039327
9	20.000000	.080532	-.037592
10	22.500000	.087249	-.035789
11	25.000000	.093149	-.034214
12	27.500000	.098160	-.032662
13	30.000000	.102496	-.031267
14	32.500000	.106068	-.029875
15	35.000000	.108943	-.028488
16	37.500000	.111066	-.026988
17	40.000000	.112721	-.025610
18	42.500000	.113513	-.023918
19	45.000000	.113617	-.022049
20	50.000000	.112044	-.017948
21	55.000000	.108402	-.013529
22	60.000000	.102951	-.008946
23	65.000000	.095882	-.004355
24	70.000000	.087320	.000094
25	75.000000	.077389	.004141
26	80.000000	.066230	.007479
27	85.000000	.053792	.009573
28	90.000000	.039880	.010193
29	95.000000	.025862	.005862
30	100.000000	.010000	-.010000

## INTERP ZS ON WINGLET (INCH)

CHORD= .691600Y/B/2= 1.000000

I	PCTX	ZUP (IN)	ZLC (IN)
1	0.000000	-.043121	-.043121
2	2.500000	-.030016	-.050016
3	5.000000	-.024042	-.049811
4	7.500000	-.018481	-.049534
5	10.000000	-.013677	-.049073
6	12.500000	-.009409	-.048554
7	15.000000	-.005664	-.047810
8	17.500000	-.002252	-.046971
9	20.000000	.001007	-.046215
10	22.500000	.003885	-.045301
11	25.000000	.006548	-.044367
12	27.500000	.008951	-.043348
13	30.000000	.011168	-.042307
14	32.500000	.013155	-.041191
15	35.000000	.014931	-.040010
16	37.500000	.016466	-.038724
17	40.000000	.017865	-.037435
18	42.500000	.018966	-.035974
19	45.000000	.019833	-.034402
20	50.000000	.020960	-.031006
21	55.000000	.021379	-.027365
22	60.000000	.021173	-.023560
23	65.000000	.020406	-.019665
24	70.000000	.019121	-.015749
25	75.000000	.017370	-.011913
26	80.000000	.015213	-.008273
27	85.000000	.013825	-.006175
28	90.000000	.013734	-.006266
29	95.000000	.012881	-.007119
30	100.000000	.010000	-.010000

I. Link (0) - (System Control)

Item (1) -- Alphanumeric Identification  
(2) cards, (72 columns each)

Item (2) -- Next Link Number  
(Col. 1-5, Right Justified)

II. Link (1) - (Planform and Airfoil Sections)

Item (1) -- (1) card, (Col. 1-10, Right-Justified)  
KASE (= 0, New Case)  
(≠ 0, Link 1 Def. on File 1)

Item (2) -- (1) card, (4 fields of 10 col. each)  
Leading and Trailing Edge Data

(a) - (Col. 1-10, Right-Justified)  
= 1 (Straight Line(s) on leading edge)  
= 2 (Cubic curve on leading edge)

(b) - (Col. 11-20, Right-Justified)  
(No. of points on leading edge)

(c) - (Col. 21-30, Right-Justified)  
Same as (a) above for T.E.

(d) - (Col. 31-40, Right-Justified)  
Same as (b) above for T.E.

Item (3) -- See form for L.E. and T.E. data

Item (4) -- (1) card, (9 data fields)  
Airfoil Definition Data (21 Limit)

(a) - (Col. 1-5, Right-Justified)  
= 1 (No airfoil fit)  
= 2 (Fit straight lines)  
= 3 (Fit cubics)

(b) - (Col. 6-10, R-J)  
No. of given airfoils. (Max. 21)

(c) - (Col. 11-15, R-J)  
No. of points per airfoil. (Max. 30)

- (d) - (Col. 16-20, R-J)  
No. of camber line points
- (e) - (Col. 21-50, Left-Justified with decimal)  
L.E. Radius
- (f) - (Col. 31-40, L-J w D)  
T.E. Radius
- (g) - (Col. 41-50, L-J w D)  
L.E. Thickness
- (h) - (Col. 51-60, L-J w D)  
T.E. Thickness
- (i) - (Col. 61-70, L-J w D) (FAC = 1.0)

Item (5) - See form for airfoil WB lines.  
YDEM for WB (lines)

Item (6) -- (1) card, (Max. of 20, one Col. fields)  
A one in the (ith) column will apply a cubic fit to all  
surface lines between the (ith) and (i + 1st) airfoils.  
A zero will cause a straight line fit.

Item (7) -- (1) card, (Max. of 31, one Col. fields)  
A one in the (ith) column will cause the (ith) airfoil  
to be read from cards. A zero will make the (ith)  
airfoil identical with the (i - 1st) airfoil.

Item (8) -- See form for airfoil ordinates percent-of-chord  
locations.

Item (9) -- See form for airfoil ordinates. (order: percent, upper, lower)

CONTROL RETURNS TO LINK (0) FOR ITEM (2).

### III. Link (3) - (Spanwise Percent Line Arrays)

Item (1) -- (1) card, (3 fields of 10 Col. each)

- (a) - (Col. 1-10, R-J)  
(No. of percent line values in this set - Max. 31)
- (b) - (Col. 11-20, R-J)  
= 1 (Read another set of line values)  
= 0 (This is the last set of lines)

(c) - (Col. 21-30, R-J)  
= 0 (In all cases)

Item (2) -- See form for percent line values.

CONTROL RETURNS TO LINK (0) FOR ITEM (2).

IV. Link (5) - (Cutter Motion and Surface Parameters)

Item (1) -- (1) card, (7 fields of 10 Col. each)

(a) - (Col. 1-10 R-J)  
= 0 (Output both surfaces)  
= 1 (Output upper surface only)  
= 2 (Output lower surface only)

(b) - (Col. 11-20, R-J)  
= 1 (MDI)

(c) - (Col. 21-30, R-J)  
= 0 (Do not invert lower surf. Z)  
= 1 (Do invert lower surf. Z)

(d) - (Col. 31-40, R-J)  
= 0 (This is last case)  
≠ 0 (Another case follows)

(e) - (Col. 41-50, R-J)  
= 0 (Output cutter center)  
= 1 (Output surf. points and normals)

(f) - (Col. 51-60, R-J)  
= 0 (No plot output)  
≠ 0 (Generate plot tape)

(g) - (Col. 61-70, R-J)  
(Line print increment)

Item (2) -- (2) cards, (8 fields of 10 Col. each)

(a) - (Col. 1-10, L-J w decimal)  
YS = (Outboard WBL for line cuts)

(b) - (Col. 11-20, L-J w dec.)  
YE = (Inboard WBL for line cuts)

- (c) - (Col. 21-30, L-J w dec.)  
DY = (Point increment for line cuts)
- (d) - (Col. 31-40, L-J w dec.)  
PS = (First cut percent line)
- (e) - (Col. 41-50, L-J w dec.)  
PE = (Last cut percent line)
- (f) - (Col. 51-60, L-J e dec.)  
a = (Rotation angle, usually 0)
- (g) - (Col. 61-70, L-J w dec.)  
R = (Cutter radius)
- (h) - (Col. 1-10. L-J w dec.)  
PM = (1.0, Not used currently)

Item (3) -- (1) card, (1 field of 10 Col.)  
(a) - (Col. 1-10, R-J)  
NB = (No. of Butt Blocks.)

IF NB  $\neq$  0 Include ITEM (3.1)

Item (3.1) -- (1) card, (3  $\leq$  N  $\leq$  7 (10) Col. fields)

- (a) - (Col. 1-10, L-J w dec.)  
YB = (Y line at butt blocks)
- (b) - (Cols. 11-20, 21-30, ....61-70)  
 $X_{N,M}$  = (Butt block  $\times$  locations)  
(1  $\leq$  N  $\leq$  3; M = 1, 2)

CONTROL RETURNS TO LINK (0) FOR ITEM (2).

#### V. Link (6) - (Postprocessor Control Commands)

Items (1-N) -- (One statement per card.)

The input for Link (6) must be selected from the list that follows:

<u>STATEMENT</u>	<u>FUNCTION</u>
(1) PARTNO - 66 Characters -	Part I.D.
(2) MACHIN/"Name", N, Mode	Postprocessor Selection
(3) CLEARP/XYPLAN, Z	Clearance Plane
YZPLAN, X	Clearance Plane
ZXPLAN, Y	Clearnace Plane
(4) TRANS /"X", "Y", "Z"	Coordinate Translation
(5) FROM /"X", "Y", "Z"	Set Point
(6) GO TO /"X", "Y", "Z"	Go to point
(7) GODLTA/"X", "Y", "Z"	End-of-line retract
(8) COOLNT/FLOOD	Coolant Control
MIST	Coolant Control
OFF	Coolant Control
(9) SPINDL/ON, CLW	Spindle Control
ON, CCLW	Spindle Control
OFF	Spindle Control
(10) TMARK /N	Manual Rewind Stop
N, AUTO	Auto Rewind Stop
(11) MCHTOL/e	Corner Tolerance
(12) INTOL/e	Surface Tolerance
(13) OUTTOL/e	Surface Tolerance
(14) REWIND/N	Automatic Rewind
(15) RETRCT	Move to CLEARP
(16) OPSTOP	Optional Stop Code
(17) STOP	Stop Code
(18) END	Process Points
(19) FINI	Program End

CONTROL RETURNS TO LINK (0) FOR ITEM (2).

WING KUHLMAN UPPER 1.0 MILL 6/4/79 JMK 50-99 PERCENT

c

1

4

1

3

1

0.0	0.0	8.5902	10.979849	21.4754	27.449572	
15.7426	0.0	17.6535	10.979849	24.6694	27.449572	
3 21 30	00.0	0.0	0.0	0.0	0.0	1.0
0.0	.786766	2.354638	3.922510	5.490381	7.058253	8.628955
10.196827	10.979849	11.374146	12.551465	14.122167	15.690039	17.25791
18.825782	20.393654	21.961526	23.529398	25.09727	26.665141	27.449572
00000000000000000000						
11111111111111111111						
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.995245	1.202815	1.277488	1.329803	1.367710	1.395796	1.413495
1.424868	1.434055	1.435831	1.433866	1.427067	1.417113	1.402988
1.385094	1.362719	1.338290	1.308086	1.273572	1.193835	1.102205
1.000790	.891310	.775107	.653882	.529630	.404069	.277081
.146534	.010000					
.995245	.776821	.690918	.622960	.562004	.504764	.454141
.406951	.359150	.316217	.274895	.236611	.199895	.165935
.134502	.106459	.079512	.057494	.039037	.010936	-.007333
-.017442	-.020817	-.018635	-.012660	-.004989	.001688	.006938
.008629	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.851330	1.056410	1.132631	1.187220	1.227910	1.259126	1.280283
1.295299	1.308178	1.313844	1.315845	1.313112	1.307265	1.297313
1.283640	1.265551	1.245394	1.219557	1.189457	1.118607	1.035952
.943213	.842337	.734507	.621346	.504767	.386381	.266029
.141446	.010000					
.851330	.643350	.563872	.501839	.446668	.395150	.350058
.308289	.265911	.228226	.192065	.158803	.127006	.097821
.071020	.047436	.024837	.006937	-.007593	-.028375	-.039997
-.044101	-.042094	-.035134	-.024958	-.013619	-.003782	.004088
.007728	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.564534	.764523	.843919	.903030	.649259	.986706	1.014749

Input Deck for Numerically Controlled (NC) Machining of Wing

ORIGINAL PAGE IS  
OF POOR QUALITY

1.037020	1.057253	1.070669	1.080571	1.085937	1.098273	1.086636
1.081373	1.071824	1.060180	1.043046	1.021743	.968609	.903546
.828402	.744680	.653542	.556460	.455181	.351105	.243985
.131297	.010000					
.564536	.377400	.310736	.260520	.216884	.176772	.142710
.111748	.080180	.052956	.027083	.003830	-.018161	-.037828
-.055397	-.070098	-.084031	-.093725	-.100431	-.106629	-.105009
-.097156	-.084430	-.067958	-.049417	-.030780	-.014653	-.001571
.005943	-.010000					
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17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.443564	.633525	.711442	.770064	.816571	.854802	.884207
.908170	.430201	.945807	.958074	.966064	.971162	.972491
.470372	.964187	.955974	.942572	.925202	.880400	.824135
.758110	.683704	.761475	.514265	.422167	.325917	.228223
.123530	.010000					
.443664	.272514	.213802	.179384	.133016	.099858	.070298
.044587	.018261	-.004164	-.025182	-.043908	-.061517	-.077016
-.040620	-.101614	-.111960	-.119421	-.122153	-.123162	-.117189
-.105750	-.090137	-.071430	-.051224	-.031342	-.014460	-.000954
.006522	-.010000					
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17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.368965	.548121	.622578	.679399	.724820	.762431	.791767
.815995	.838346	.854674	.867846	.876980	.883378	.886220
.885804	.881557	.875374	.864309	.849504	.810377	.760360
.701026	.633640	.559168	.478834	.394095	.306043	.214376
.116554	.010000					
.368965	.212523	.160480	.122550	.090085	.060478	.035989
.014082	-.008462	-.027357	-.045189	-.060859	-.075545	-.088330
-.099411	-.108123	-.116290	-.120906	-.123060	-.121509	-.113733
-.101135	-.084932	-.066141	-.046267	-.027077	-.010952	.001557
.007913	-.010000					
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35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.316432	.483867	.554648	.609044	.652741	.689084	.717696
.741517	.763530	.779909	.793310	.802921	.809947	.813632
.814255	.811283	.806470	.797096	.784215	.749500	.704509
.650687	.589195	.520913	.446955	.368651	.286967	.201597
.110036	.010000					

.316432	.174082	.128091	.095024	.066827	.041122	.020048
.001283	-.018147	-.034280	-.049499	-.062784	-.075220	-.085959
-.095183	-.102275	-.108920	-.112341	-.113545	-.110710	-.102353
-.089776	-.074108	-.056300	-.037758	-.020126	-.005647	.005147
.009750	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.278829	.434163	.500886	.552476	.594067	.628757	.656257
.679282	.700565	.716602	.729836	.739527	.746782	.750910
.752167	.750069	.746221	.738131	.726767	.695652	.654876
.605767	.549368	.486498	.418159	.345564	.269558	.199844
.103972	-.010000					
.278829	.150190	.109872	.081287	.056974	.034785	.016740
.000727	-.015979	-.029745	-.042747	-.054045	-.064630	-.073724
-.081492	-.087368	-.092895	-.095528	-.096188	-.092883	-.084755
-.073003	-.058666	-.042620	-.026165	-.010819	.001326	.009764
.012043	-.010000					
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35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.262052	.405002	.467384	.515886	.555088	.587837	.613931
.635856	.656093	.671458	.684178	.693585	.700687	.704857
.706329	.704663	.701321	.694038	.683692	.655123	.617434
.571826	.519262	.460469	.396358	.328029	.256228	.180691
.099089	-.010000					
.262052	.146842	.111914	.087528	.066817	.047858	.032547
.018982	.004683	-.007046	-.018177	-.027851	-.036967	-.044818
-.051550	-.056650	-.061519	-.063841	-.064456	-.061733	-.054964
-.045238	-.033501	-.020551	-.007577	-.004041	.012379	.016980
.015516	-.010000					
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35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.256268	.393188	.453564	.500689	.538868	.570817	.596369
.617893	.637745	.652902	.665480	.674850	.681970	.686243
.687894	.686506	.683467	.676626	.666818	.639545	.603378
.559457	.508692	.451770	.389545	.323060	.252969	.179027
.098788	-.010000					
.256268	.147935	.115866	.093747	.075008	.057834	.044051
.031860	.018903	.008320	-.001760	-.010516	-.018805	-.025951
-.032094	-.036745	-.041234	-.043362	-.043926	-.041471	-.035404
-.026758	-.018436	-.005702	-.005805	-.015270	.021311	.022501

.019393	-.010000						
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17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000	
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000	
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000	
95.000000	100.000000						
.253355	.388587	.448461	.495273	.533250	.565066	.590561	
.612069	.631907	.647100	.659732	.669183	.676396	.680785	
.682569	.681338	.678460	.671815	.662227	.635443	.599810	
.556449	.506255	.449901	.388224	.322249	.252601	.179044	
.099073	.010000						
.253355	.147138	.116000	.094642	.076584	.060039	.046809	
.035124	.022663	.012515	.002840	-.005554	-.013510	-.020364	
-.026254	-.030696	-.035002	-.037007	-.037494	-.035011	-.029064	
-.020673	-.010729	.000016	.010435	.019233	.024536	.025930	
.020909	-.010000						
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000	
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000	
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000	
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000	
95.000000	100.000000						
.193940	.323953	.382153	.427888	.465175	.496577	.521960	
.543554	.563570	.579172	.592351	.602517	.610569	.615952	
.618873	.618943	.617465	.612420	.604592	.581749	.550553	
.512063	.467116	.416332	.360470	.300453	.236758	.168994	
.094360	.010000						
.193940	.093868	.065340	.046114	.030004	.015321	.003802	
-.006234	-.016999	-.025544	-.033622	-.040462	-.046864	-.052195	
-.056586	-.059577	-.062415	-.063039	-.062195	-.057149	-.048727	
-.037895	-.025534	-.012377	.000463	.011699	.019428	.023087	
.019876	-.010000						
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000	
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000	
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000	
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000	
95.000000	100.000000						
.151121	.273935	.329651	.373674	.409726	.440219	.465051	
.486319	.506085	.521704	.535038	.545540	.554051	.560051	
.563737	.564745	.564291	.560491	.554075	.534483	.507018	
.472667	.432167	.386102	.335140	.280105	.221383	.158563	
.088912	.010000						
.151121	.058972	.033660	.016991	.003156	-.009408	-.019053	
-.027337	-.036327	-.043269	-.049795	-.055181	-.060175	-.064184	
-.067330	-.069182	-.070906	-.070576	-.068889	-.062424	-.052871	
-.041157	-.028105	-.014431	-.001206	.010329	.018336	.022245	
.019323	-.010000						
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35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000	

60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.121660	.237017	.289993	.332045	.366599	.395911	.419918
.440575	.459801	.475136	.488318	.498838	.507480	.513762
.517868	.519459	.519667	.516739	.511355	.494228	.469677
.438607	.401718	.359520	.312626	.261790	.207340	.148875
.083752	.010000					
.121660	.037176	.014823	.000452	-.011372	-.022087	-.030132
-.036948	-.044456	-.050094	-.055376	-.059626	-.063538	-.066561
-.068807	-.069874	-.070848	-.069936	-.067786	-.060691	-.050827
-.039064	-.026176	-.012838	-.000061	.010991	.018576	.022146
.019059	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.097412	.205119	.255160	.295052	.327926	.355883	.378889
.398763	.417277	.432159	.445018	.455388	.463994	.470391
.474750	.476758	.477463	.475243	.470729	.455746	.433801
.405726	.372165	.333583	.290538	.243717	.193396	.139186
.078542	.010000					
.097412	.020399	.000812	-.011449	-.021444	-.030486	-.037106
-.042626	-.048823	-.053327	-.057534	-.060817	-.063815	-.066020
-.067532	-.067981	-.068368	-.067038	-.064590	-.057182	-.047316
-.035799	-.023351	-.010599	.001512	.011896	.018916	.022046
.018743	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.076455	.176343	.223281	.260851	.291892	.318349	.340217
.359174	.376845	.391149	.403563	.413662	.422115	.428513
.433013	.435331	.436427	.434814	.431070	.418044	.398530
.373291	.342916	.307826	.268525	.225635	.179383	.129392
.073232	.010000					
.076455	.006745	-.010245	-.020559	-.028877	-.036390	-.041723
-.046081	-.051098	-.054594	-.057849	-.060284	-.062486	-.063986
-.064875	-.064814	-.064721	-.063075	-.060426	-.052895	-.043202
-.032090	-.020222	-.008180	.003160	.012792	.019186	.021842
.018320	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.055906	.147816	.191494	.226594	.255672	.280511	.301132
.310070	.335807	.346446	.361337	.371096	.379331	.385572

.390262	.392843	.394291	.393252	.390251	.379145	.362050
.339659	.312506	.280968	.245498	.206653	.164613	.119021
.067574	.010000					
.055906	-.006660	-.021211	-.029725	-.036498	-.042599	-.046754
-.050052	-.053981	-.056555	-.058935	-.060594	-.062064	-.062916
-.063235	-.062708	-.062174	-.060245	-.057423	-.049804	-.040297
-.029577	-.018255	-.006863	.003793	.012786	.018700	.021060
.017566	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.038585	.122350	.162600	.195071	.222039	.245126	.264372
.281169	.296853	.309715	.320975	.330288	.338205	.344391
.348977	.351730	.353440	.352886	.350544	.341195	.326364
.306673	.282601	.254485	.222723	.187812	.149891	.108620
.061848	-.010000					
.038585	-.017005	-.029283	-.036158	-.041531	-.046356	-.049460
-.051821	-.054779	-.056543	-.058157	-.059144	-.059982	-.060285
-.060127	-.059228	-.058342	-.056218	-.053307	-.045765	-.036598
-.026419	-.015781	-.005170	.004679	.012923	.018261	.020249
.016735	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.023149	.098591	.135238	.164914	.189626	.210831	.228580
.244123	.258650	.270638	.281176	.289960	.297479	.303436
.307949	.310809	.312722	.312599	.310862	.303176	.290527
.273467	.252420	.227681	.199597	.168605	.134811	.097901
.055893	.010000					
.023149	-.025642	-.035824	-.041224	-.045343	-.049022	-.051198
-.052733	-.054826	-.055877	-.056816	-.057215	-.057500	-.057328
-.056763	-.055556	-.054377	-.052114	-.049168	-.041795	-.033050
-.023481	-.013585	-.003800	.005213	.012694	.017464	.019118
.015676	-.010000					
0.000000	2.500000	5.000000	7.500000	10.000000	12.500000	15.000000
17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
.013899	.080797	.113618	.140291	.162559	.181707	.197796
.211927	.225143	.236108	.245780	.253891	.260871	.266460
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 -.018269 -.009474 -.000883 .006923 .013282 .017155 .018190  
 .014618 -.010000  
 0.000000 2.500000 5.000000 7.500000 10.000000 12.500000 15.000000  
 17.500000 20.000000 22.500000 25.000000 27.500000 30.000000 32.500000  
 35.000000 37.500000 40.000000 42.500000 45.000000 50.000000 55.000000  
 60.000000 65.000000 70.000000 75.000000 80.000000 85.000000 90.000000  
 95.000000 100.000000  
 .022580 .080541 .109147 .132434 .151886 .168607 .182650  
 .194957 .206422 .215884 .224166 .231032 .236852 .241400  
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 .214335 .197082 .177042 .154548 .129994 .103511 .074902  
 .042669 .010000  
 .022580 -.013450 -.020273 -.023522 -.025883 -.027988 -.029019  
 -.029633 -.030743 -.031145 -.031546 -.031627 -.031712 -.031540  
 -.031162 -.030385 -.029712 -.028297 -.026437 -.021787 -.016300  
 -.010325 -.004168 .001912 .007484 .012037 .014731 .015299  
 .012242 -.010000  
 0.000000 2.500000 5.000000 7.500000 10.000000 12.500000 15.000000  
 17.500000 20.000000 22.500000 25.000000 27.500000 30.000000 32.500000  
 35.000000 37.500000 40.000000 42.500000 45.000000 50.000000 55.000000  
 60.000000 65.000000 70.000000 75.000000 80.000000 85.000000 90.000000  
 95.000000 100.000000  
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 .186473 .197061 .205772 .213359 .219603 .224842 .228869  
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 .011053 -.010000

3

	26	1	0			
0.0	4.0	8.0	12.0	16.0	20.0	24.0
28.0	32.0	36.0	40.0	44.0	48.0	52.0
56.0	60.0	64.0	68.0	72.0	76.0	80.0
84.0	88.0	92.0	96.0	100.0		
	25	1	0			
0.5	4.5	8.5	12.5	16.5	20.5	24.5
28.5	32.5	36.5	40.5	44.5	48.5	52.5
56.5	60.5	64.5	68.5	72.5	76.5	80.5
84.5	88.5	92.5	96.5			
	25	1	0			
1.0	5.0	9.0	13.0	17.0	21.0	25.0
29.0	33.0	37.0	41.0	45.0	49.0	53.0
57.0	61.0	65.0	69.0	73.0	77.0	81.0

85.0	89.0	93.0	97.0				
25	1	0					
1.5	5.5	9.5	13.5	17.5	21.5	25.5	
29.5	33.5	37.5	41.5	45.5	49.5	53.5	
57.5	61.5	65.5	69.5	73.5	77.5	81.5	
85.5	89.5	93.5	97.5				
25	1	0					
2.0	6.0	10.0	14.0	18.0	22.0	26.0	
30.0	34.0	38.0	42.0	46.0	50.0	54.0	
58.0	62.0	66.0	70.0	74.0	78.0	82.0	
86.0	90.0	94.0	98.0				
25	1	0					
2.5	6.5	10.5	14.5	18.5	22.5	26.5	
30.5	34.5	38.5	42.5	46.5	50.5	54.5	
58.5	62.5	66.5	70.5	74.5	78.5	82.5	
86.5	90.5	94.5	98.5				
25	1	0					
3.0	7.0	11.0	15.0	19.0	23.0	27.0	
31.0	35.0	39.0	43.0	47.0	51.0	55.0	
59.0	63.0	67.0	71.0	75.0	79.0	83.0	
87.0	91.0	95.0	99.0				
25	0	0					
3.5	7.5	11.5	15.5	19.5	23.5	27.5	
31.5	35.5	39.5	43.5	47.5	51.5	55.5	
59.5	63.5	67.5	71.5	75.5	79.5	83.5	
87.5	91.5	95.5	99.5				
5							
1	1	1	0	0	0	0	10
27.449572	0.0	1.646972	50.0	99.0	0.0	0.0	
1.0							
0							

6  
 PARTNO      WING KÜHLMAN UPPER 1.0 MILL 6/4/79 JMK 50-99 PERCENT  
 MACHIN/SUNTRN.3.,LINEAR  
 CLEARP/XYPLAN.3.0  
 FFDPAT/50.0  
 COOLNT/MIST  
 SPINDL/ON,CLW  
 FRON/-1.0,-1.0,2.0,60.0  
 GOTO/7.0,3.0,2.0,60.0  
 COOLTA/0.0,0.0,1,20.0  
 OPSTOP  
 CUTPTS  
 RFTPCT  
 GOTO/-1.0,-1.0,2.0,60.0  
 COOLNT/OFF  
 SPINDL/OFF  
 STOP  
 END

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PARTNO TX 23-WING  
MACHIN/SUNTRN  
PTONLY/2  
FINI

## WINGLET KUHLMAN 1/4 MILL 6/4/79 JMK

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0.0	0.0	0.9051	0.489151	1.8098	0.978070	
2.2931	1.661108	3.3311	3.12814	3.8856	3.912094	
3.912094	0.0	3.36690	0.489151	3.53980	0.978070	
3.78134	1.661108	4.30011	3.12814	4.57720	3.912094	
3	6	30	00.0	0.0	0.0	1.0
0.0	0.489151	0.978070	1.661108	3.12814	3.912094	
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111111						
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17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
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.161262	.172261	.181038	.188445	.194350	.199146	.202673
.205060	.206207	.206642	.205643	.203535	.196531	.186404
.173664	.158701	.141787	.123208	.103281	.082087	.059366
.033839	.010000					
-.020809	-.048269	-.048948	-.047227	-.046161	-.046037	-.045602
-.045262	-.045825	-.046119	-.046697	-.047180	-.047814	-.048311
-.048671	-.048675	-.048750	-.048088	-.046938	-.043466	-.038709
-.032924	-.026359	-.019255	-.012026	-.005188	.000448	.004557
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35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
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.138233	.127227	.114498	.100252	.084717	.067909	.049601
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-.020996	-.015410	-.009626	-.003981	.001114	.004985	.007357
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35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
-.042768	-.008221	.011652	.028320	.042149	.053865	.063798

Input Deck for Numerically Controlled (NC) Machining of Winglet

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.108943	.111066	.112721	.113513	.113617	.112044	.108402
.102951	.095882	.087320	.077389	.066230	.053792	.039880
.025862	.010000					
-.042763	-.055035	-.052808	-.049357	-.046393	-.044053	-.041628
-.039327	-.037592	-.035789	-.034214	-.032662	-.031267	-.029875
-.028488	-.026988	-.025610	-.023918	-.022049	-.017948	-.013529
-.008946	-.004355	.000094	.004141	.007479	.009573	.010193
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17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
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.035763	.043077	.049464	.055287	.060456	.065135	.069231
.072784	.075731	.078301	.080143	.081395	.082337	.081409
.078787	.074604	.068944	.061901	.053597	.043998	.032962
.023073	.010000					
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-.060466	-.058540	-.056380	-.054277	-.052084	-.049935	-.047715
-.045442	-.043031	-.040699	-.038083	-.035312	-.029489	-.023483
-.017472	-.011625	-.006093	-.001111	.003056	.005959	.007423
.003073	-.010000					
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17.500000	20.000000	22.500000	25.000000	27.500000	30.000000	32.500000
35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
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.010968	.015636	.019733	.023493	.026856	.029928	.032647
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.041191	.039235	.036429	.032838	.028545	.023545	.019442
.016416	.010000					
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-.051688	-.050528	-.049183	-.047846	-.046420	-.044996	-.043498
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35.000000	37.500000	40.000000	42.500000	45.000000	50.000000	55.000000
60.000000	65.000000	70.000000	75.000000	80.000000	85.000000	90.000000
95.000000	100.000000					
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-.002252	.001007	.003885	.006548	.008951	.011168	.013155
.014931	.016466	.017865	.018966	.019833	.020960	.021379
.021173	.020406	.019121	.017370	.015213	.013825	.013734
.012881	.010000					

-.043121 -.050016 -.049811 -.049534 -.049073 -.048554 -.047810  
 -.046971 -.046215 -.045301 -.044367 -.043348 -.042307 -.041191  
 -.040010 -.038724 -.037435 -.035974 -.034402 -.031006 -.027365  
 -.023560 -.019665 -.015749 -.011913 -.008273 -.006175 -.006266  
 -.007119 -.010000

3

26	1	0				
0.0	4.0	8.0	12.0	16.0	20.0	24.0
28.0	32.0	36.0	40.0	44.0	48.0	52.0
56.0	60.0	64.0	68.0	72.0	76.0	80.0
84.0	88.0	92.0	96.0	100.0		
25	1	0				
1.0	5.0	9.0	13.0	17.0	21.0	25.0
29.0	33.0	37.0	41.0	45.0	49.0	53.0
57.0	61.0	65.0	69.0	73.0	77.0	81.0
85.0	89.0	93.0	97.0			
25	1	0				
2.0	6.0	10.0	14.0	18.0	22.0	26.0
30.0	34.0	38.0	42.0	46.0	50.0	54.0
58.0	62.0	66.0	70.0	74.0	78.0	82.0
86.0	90.0	94.0	98.0			
25	0	0				
3.0	7.0	11.0	15.0	19.0	23.0	27.0
31.0	35.0	39.0	43.0	47.0	51.0	55.0
59.0	63.0	67.0	71.0	75.0	79.0	83.0
87.0	91.0	95.0	99.0			

5

4.0000	1	1	1			
1.0	0.0	1.511	1.0	99.0	0.0	.1255

0

6

PARTNO WINGLET KUHLMAN 1/4 MILL 6/4/79 JMK  
 MACHIN/SUNTPN.3.,LINEAR  
 CLEAPP/XYPLAN.3.0  
 FEDPAT/60.0  
 COOLNT/MIST  
 SPINDL/ON.CLW  
 FROM/-1.0,-1.0,2.0,60.00  
 GOTO/0.0,2.0,1.0,60.0  
 GDLTA/0.0,0.0,,1.20.0  
 OPSTOP  
 CUTPTS  
 PETRCT  
 GOTO/-1.0,-1.0,2.0,60.0  
 COOLNT/OFF  
 SPINDL/OFF  
 STOP  
 END

FINI

0

R  
PARTNO

TX 23.WING  
MACHIN/SUNTRN  
PTONLY/2  
FINI

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7. Author(s)  John M. Kuhlman		8. Performing Organization Report No.	
9. Performing Organization Name and Address  Old Dominion University Research Foundation P. O. Box 6369 Norfolk, Virginia 23508		10. Work Unit No.	11. Contract or Grant No. NSG-1357
12. Sponsoring Agency Name and Address  National Aeronautics and Space Administration Washington, DC 20546		13. Type of Report and Period Covered  Contractor Report	14. Sponsoring Agency Code
15. Supplementary Notes  Langley Technical Monitors: John E. Lamar and John B. Peterson, Jr.			
16. Abstract  The aerodynamic design of a wind-tunnel model of a wing representative of that of a subsonic jet transport aircraft, fitted with winglets, has been performed using two recently developed optimal wing-design computer programs. Both potential flow codes use a vortex lattice representation of the near-field of the aerodynamic surfaces for determination of the required mean camber surfaces for minimum induced drag, and both codes use far-field induced drag minimization procedures to obtain the required spanloads. One code uses a discrete vortex wake model for this far-field drag computation, while the second uses a 2-D advanced panel wake model. Wing camber shapes for the two codes are very similar, but the resulting winglet camber shapes differ widely. Design techniques and considerations for these two wind-tunnel models are detailed herein, including a description of the necessary modifications of the design geometry to format it for use by a numerically controlled (NC) machine for the actual model construction.			
17. Key Words (Suggested by Author(s))  Subsonic Aerodynamics Wing Design Winglets		18. Distribution Statement  Unclassified - Unlimited Subject Category 02	
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